# INSTRUCTION MANUAL MODEL F210A



DATA ROYAL CORPORATION SAN DIEGO, CALIFORNIA

# INSTRUCTION MANUAL MODEL F210A

BL06-77 RM53



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#### SECTION I

# INTRODUCTION

The Data Royal Model F210A is a high frequency Waveform Generator. The F210A provides continuously variable selection of frequency from .005 Hz to 3MHz by means of 16 possible range switch combinations and a 20:1 vernier control.

The Model F210A provides Square, Sine, Triangle and Ramp outputs of up to 16.25 volts peak-to-peak, selectable by push button function switches on the front panel. In addition, fixed level outputs of all waveforms are simultaneously available on BNC connectors on the rear panel. All rear outputs have  $50\Omega$  output impedances, while both  $50\Omega$  and  $600\Omega$  connectors are provided for the front panel outputs.

A Sync signal output is also provided on a front panel BNC connector. The Sync pulse is a -10 volt pulse of maximum duration of 5 micro-seconds, and is synchronized with the selected frequency.

A Frequency Control Input is provided on the front panel, enabling the F210A to deliver frequency modulated (FM), frequency shift keying (FSK), or "swept" signals. This is accomplished by applying a Sine, Square or Ramp signal, respectively, to the FC Input.

The following F900 Series Accessories can be added:

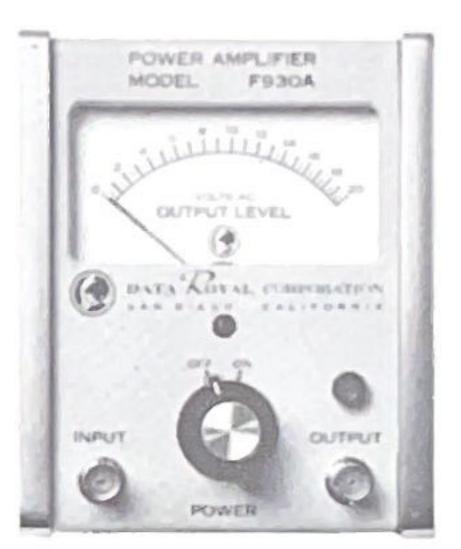
#### MODEL F910A ATTENUATOR/METER

For applications requiring more accurately known sine wave amplitudes than are possible to obtain using either the F200 or F300 Series instruments, Model F910A is provided. Although classified as an accessory, it is in itself a useful laboratory and production test instrument. A wide band AC voltmeter provides an accurate means of determining and monitoring sine wave inputs. In addition, a precision voltage divider enables the known voltage to be attenuated from 0 to -90 dB by push button control in -10 dB steps (10, 20, 30, and 30 dB). A fifth push button (-9 dB) allows the output voltage to be determined in rms or p-p.



#### MODEL F930A POWER AMPLIFIER

Although specifically designed for the F300 Series Sine and Sine/Square Generators, the Model F930A is suitable for use with other sine wave signal sources. For applications which require higher output than 3 V rms, this completely self-contained instrument can provide up to 30 V p-p across 50 ohms. The wide band AC amplifier employed has a frequency response from 10Hz to 100KHz. The same mechanical design concept as employed throughout the F900 Accessory Series enables the Model F930A to be attached to any one of the F300 Sine and Sine/Square Generators to form an integral package to facilitate rack mounting, space reduction and portability.



#### MODEL F940A TONE BURST GATE

The output of a selected number of cycles (1-100) of a specific frequency from any F300 Series Sine or Sine/Square Generator is enabled by the Model F940A tone burst control unit. Frequency capability extends from 10Hz to 10MHz. Thus, the ability of Data Royal instruments to meet ever changing test and measuring applications is greatly increased. The trigger start and stop point is adjustable over 360° in either polarity. Should the last cycle not be complete at the end of the selected tone burst period, a circuit allows the remainder of that cycle to be generated.



## SECTION II

# INSPECTION AND INSTALLATION

Your Data Royal Generator is ready for use immediately upon receipt. Make the following checks, however, to assure that no damage has occured during shipment.

- 1. Inspect the shipping container prior to acceptance from the carrier.

  Note any damage to the shipping container on the carrier's receipt.
- 2. Inspect the instrument for damage. Check for dents, scratches, broken knobs, connectors, etc.

- 3. Remove the top and bottom covers and inspect for broken components or hardware.
- 4. If damage is not apparent until after the instrument has been accepted, file a claim for concealed damage with the carrier within 15 days after receipt. All packaging material must be kept for inspection by the carrier's agent. A copy of the claim must be forwarded to Data Royal Corporation.

#### RACK MOUNTING:

Data Royal Generators are ready for bench operation as shipped from the factory. If specifically ordered, the necessary parts for rack mounting are packaged with the instrument. To convert to rack installation refer to Figure 2-1 and proceed as follows:

- 1. Remove the (4) rubber feet and the instrument bail.
- 2. Remove the Filler Panels from both sides.
- 3. Install the Rack Mounting Brackets using the #10 screws provided. The instrument is now ready to mount in a standard (19 inch) rack.

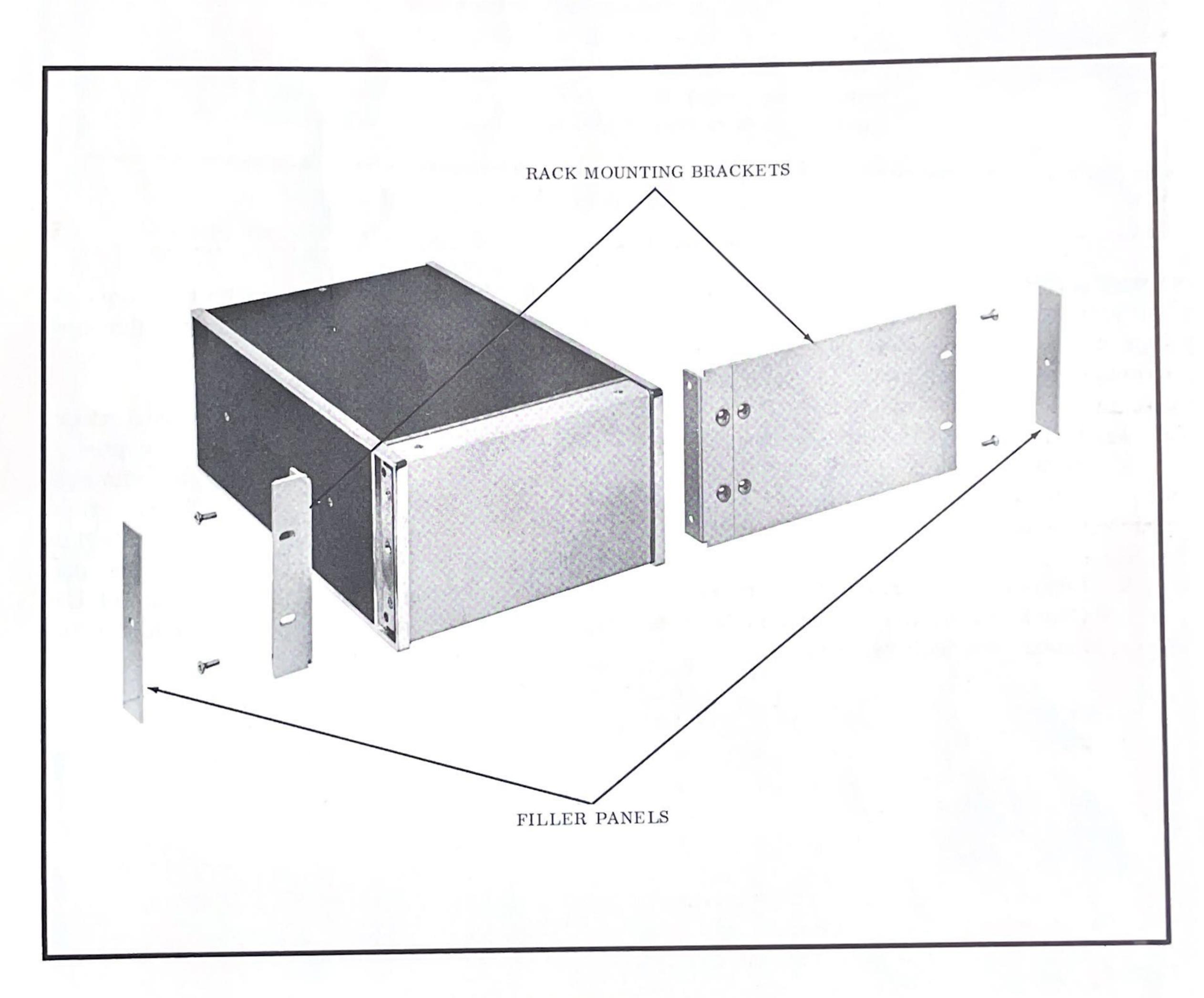
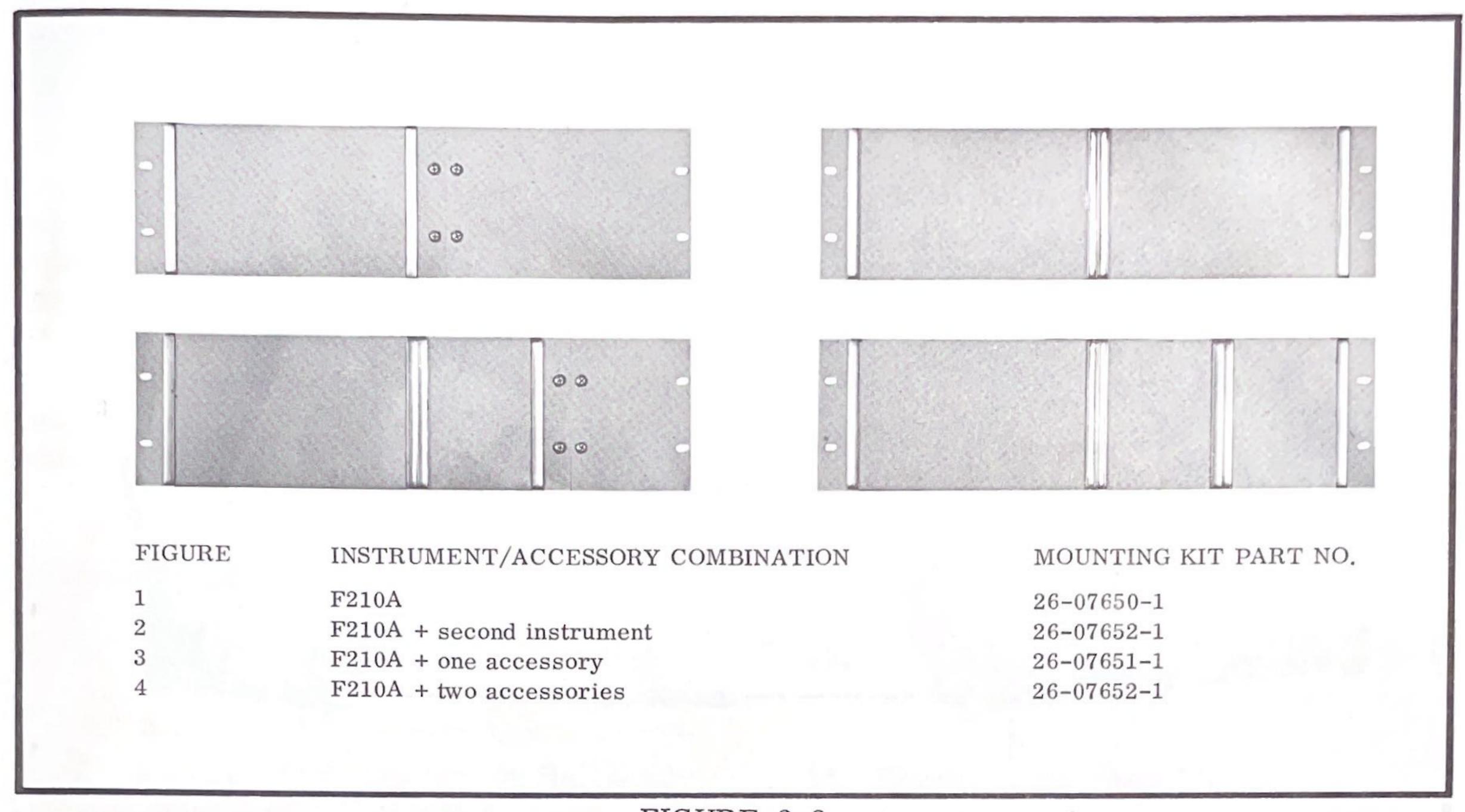


FIGURE 2-1



#### FIGURE 2-2

## COMBINATION WITH ACCESSORIES:

Each Generator can be combined with any other Data Royal 1/2 rack instrument, or with any Data Royal Series 900 Accessory, for ease of handling and conservation of space. With the appropriate Rack Mounting Kit, (4) combinations of instruments can be mounted in a single 5 1/4 inch space. (See Figure 2-2).

To combine two instruments, refer to Figure 2-3 and proceed as follows:

- 1. Remove the top and bottom covers from both instruments.
- 2. Remove the Filler Panels from the sides to be joined.
- 3. Remove the Mounting Clips from both instruments. (Under the top flange of front panel, held in place with #6-32 screw through the flange).

- 4. Remove the Angle mounted on the rear panel.
- 5. Insert the Mounting Clips in the rectangular holes at the top and bottom of the side rail near the front.
- 6. Secure the Mounting Clips with #6-32 screws removed in step 3 and spares provided.
- 7. Mount the Angle on the rear of the adjoining side rails, using the #6-32 screws provided.
- 8. Replace the top and bottom covers.

The procedure for attaching the Mounting Kit remains unchanged.

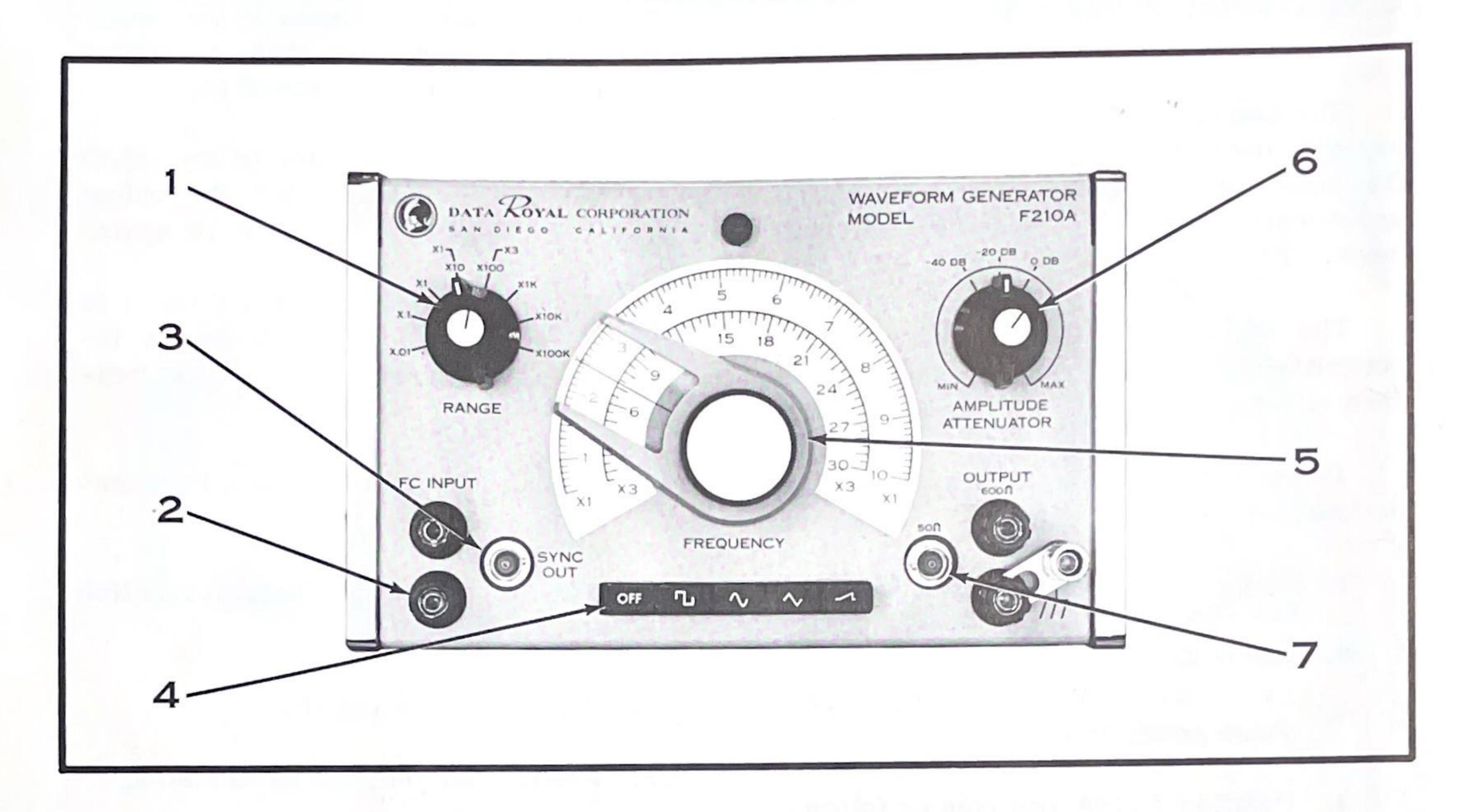


FIGURE 2-4

#### CONTROLS:

- 1. Range and Range Multiplier Switch. Concentric switches, which determine the RC networks for the Integrating Amplifier.
- 2. External Frequency Control Input. Enables the F210A output frequency to be controlled from an outside signal source, thus the F210A can provide Frequency Modulation or Frequency Shift output signals.
- 3. Sync Output. Provides a Sync signal of -10 volt amplitude, at same frequency as the output signal.
- 4. Function Switches and Power OFF. Selects the desired waveform as

- marked on each switch. Power is ON when one of the Function Switches is depressed.
- 5. Frequency Dial and Control. Marked in X1 and X3 ranges to correspond to the Range and Range Multiplier Switches.
- 6. Attenuator and Amplitude Controls. Varies the output signal level in fixed steps of 0dB, -20dB, and -40 dB. Amplitude Control varies the output over a range of >20dB.
- 7. Output Connectors provide  $50 \Omega$  and  $600 \Omega$  outputs, respectively. Output can be floated from chassis and from Earth Ground, if desired.

#### SECTION III

# CALIBRATION AND SPECIFICATION VALIDATION

#### SPECIFICATIONS

OUTPUT WAVE FORMS: Sine, Square, Triangle and Ramp wave forms selectable at the front panel with all wave forms simultaneously available at the rear. All outputs are synchronized.

FREQUENCY RANGES: .005Hz to 3MHz in 16 continuously variable ranges of 1 and 3 combinations with a 20:1 frequency ratio. Vernier control provided by 3:1 dial gear ratio.

#### OUTPUT VOLTAGE:

Front Panel: Continuously variable by fixed output attenuator (0, -20, -40dB) with output amplitude vernier of > -20dB from 0.3-32.5 volts p-p (60dB range) with 50 or 600 ohm output impedance.

Rear Panel: Fixed outputs for each wave form with 50 ohm output impedance are simultaneously available as follows:

Sine	2 volts p-p
Square	5 volts p-p
Triangle	2 volts p-p
Ramp	0 to -1 volt

## OUTPUT IMPEDANCE:

Front Panel: Both 50 ohm (BNC Connector) and 600 ohm (binding posts) output impedances are provided for the selected wave form.

Rear Panel: 50 ohm (BNC Connector) output impedance provided for each wave form.

SYNC OUTPUT: > -10 volts (open circuit) pulse for maximum of  $5\mu$ seconds duration. (Front Panel BNC Connector).

#### FREQUENCY STABILITY:

Short Term Drift:  $< \pm 0.05\%$  of setting for 10 minutes.

Long Term Drift:  $< \pm 0.25\%$  of setting for 24 hours.

#### AMPLITUDE STABILITY:

Short Term:  $\pm 0.05\%$  of maximum output (p-p) for at least 10 minutes.

Long Term:  $\pm 0.25\%$  of maximum output (p-p) for 24 hours.

SYMMETRY (AMPLITUDE): Amplitude of all waveforms is within ± 1% of maximum output (p-p) above ground.

# SYMMETRY (TIME):

>99.5% .005Hz to 100KHz >99.0% 100KHz to 1MHz >95.0% 1MHz to 3MHz

#### SINE WAVE DISTORTION:

<1%, .005Hz to 100KHz <2%, 100KHz to 1MHz <5%, 1MHz to 3MHz

OPERATING TEMPERATURE: 0° C to +50° C

POWER: 115V AC ±10% or 230V AC ±10%. 50 Hz-400Hz; 20 watts.

DIALACCURACY: ±1% of full scale, .005Hz to 100 KHz; ±2% of full scale, 100 KHz to 3MHz.

FREQUENCY RESPONSE: Amplitude change of <. 1dB, .005Hz to 100KHz; <. 5dB 100KHz to 3 MHz.

# SQUARE WAVE RISE AND FALL TIME: < 75 nano-seconds

TILT: <0.5% of p-p amplitude.

OVERSHOOT AND PRESHOOT: <5% of p-p amplitude.

# TRIANGLE WAVE AND RAMP LINEARITY: >99%, .005Hz to 100KHz >95%, 100KHz to 3MHz

DC OFFSET STABILITY: Within ±.1% of maximum p-p amplitude for 7 days; no external adjustment required.

ISOLATION: Signal output and control input terminals are floating and isolated from case and power line ground; grounding strap provided.

#### CALIBRATION PROCEDURE

#### Operational Adjustments.

- 1. 12 Volt Power Supply Adjustment:
  - a. Lift the Generator Board Assembly, exposing the Master Board.
  - b. Connect a Digital Voltmeter to the +12 Volt Test Point (Red).
  - c. Adjust R20 until the reading is / 12.000 Volts.
  - d. Check the voltage at the -12 Volt
    Test Point. Should read 12.000 volts
    ±.2 volts.
  - e. Lower the Generator Board Assembly into place.

- 2. Square Wave Symmetry Adjustment:
  - a. Position the Range Switch to X1K, and the Frequency Dial to 10.
  - b. Connect the Oscilloscope to the  $50\Omega$  output connector on the Front Panel. Terminate the output in a  $50\Omega$  load at the input to the Oscilloscope.
    - c. Select the Square Wave Function.
      Set Output Level to 0dB and the vernier fully clockwise.
    - d. Set Oscilloscope to Trigger. Expand the sweep as far as possible, and adjust the Horizontal Position so the positive going edge of the square wave is lined up with a vertical line on the grid.
    - e. Switch the Oscilloscope to + Trigger and adjust the UPPER DIAL SYM-METRY Potentiometer so the negative going edge of the square wave lines up with the same vertical line on the grid.
    - f. Turn the Frequency Dial to 1.
    - g. Repeat Step d.
    - h. Switch the Oscilloscope to + Trigger and adjust the LOWER DIAL SYM-METRY Potentiometer so the negative going edge of the square wave lines up with the same vertical line on the grid.
    - i. Repeat Steps a. through g. until no further adjustment is required.
  - 3. Frequency Control Amplifier Adjustments:
    - a. Short the F.C. input on the Front Panel.

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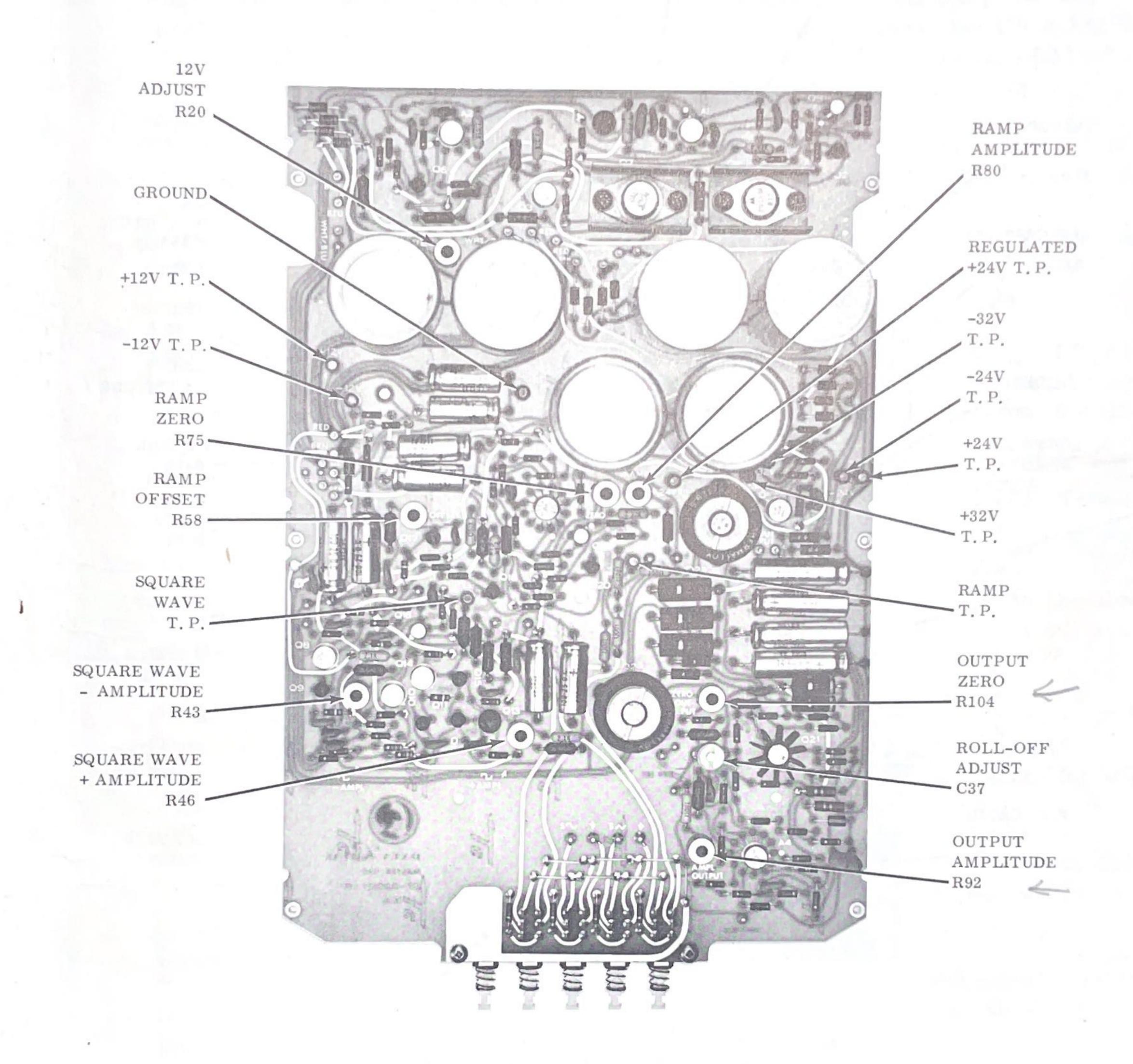


FIGURE 3-1

Master Board - Test Points and Calibration Adjustments

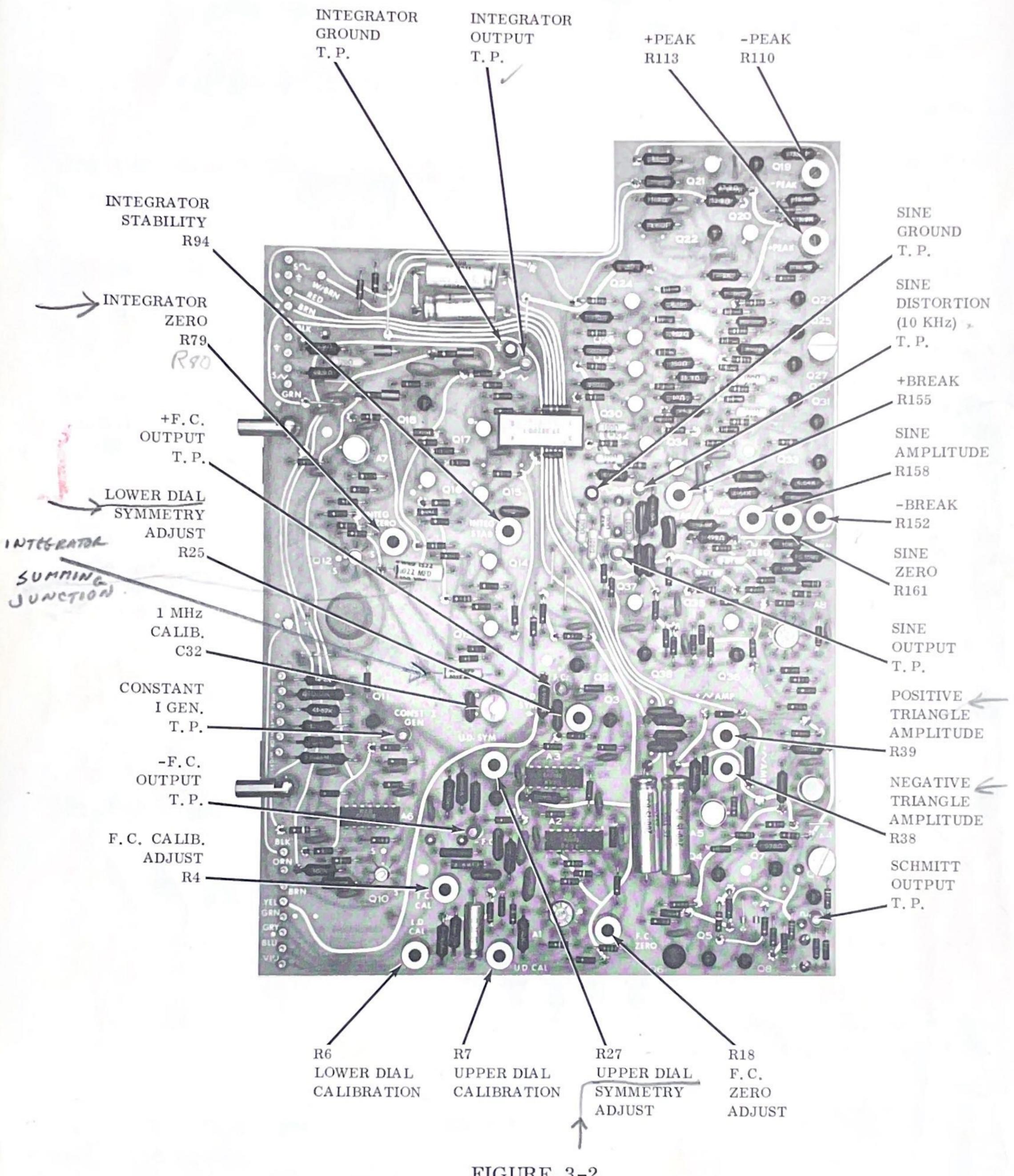


FIGURE 3-2

Generator Board - Test Points and Calibration Adjustments

- b. Connect the Digital Voltmeter to the Summing Junction of the Integrator.
- c. Adjust the INTEGRATOR ZERO
  Potentiometer for 0 volts DC at the
  Summing Junction.
  - d. Disconnect the short from the F.C. input.
- 4. Schmitt Trigger Adjustments:
  - a. Connect the Oscilloscope to the Integrater Output Test Point (Green).
  - b. Adjust the TRIANGLE POSITIVE AMPLITUDE Potentiometer for +1 volt peak amplitude.
  - c. Adjust the TRIANGLE NEGATIVE AMPLITUDE Potentiometer for -1 volt peak amplitude.
- 5. Sine Generator Adjustments:
  - a. Position the Range Switch to X1K, and the Frequency Dial to 10.
  - b. Connect the Oscilloscope to the Sine Distortion Test Point (Green).

    Connect dist Analyzor To output-
  - c. Vary the Frequency Dial slightly for minimum amplitude at the test point.
- d. Adjust the NEGATIVE BREAK Potentiometer for minimum signal.
- e. Adjust the POSITIVE BREAK Potentiometer for minimum signal.
- f. Adjust the NEGATIVE PEAK Potentiometer for minimum signal.
- g. Adjust the POSITIVE PEAK Potentiometer for minimum signal.

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- h. Repeat Steps d. through h. until no further adjustment is required.
- 6. Output Amplifier Adjustments:
  - a. Connect the Oscilloscope to the  $50\Omega$  output connector on the Front Panel. Terminate the output in a  $50\Omega$  load at the input to the Oscilloscope.
  - b. Select the Triangle Function and raise the Generator Board Assembly.
  - c. Make sure the Output Attenuator is at 0dB and the Amplitude Control is fully clockwise.
  - d. Adjust the OUTPUT AMPLIFIER ZERO Potentiometer for equal peak amplitude above and below 0 volts DC.
  - e. Adjust the OUTPUT AMPLITUDE

    Potentiometer for 17 volts peak-topeak amplitude.
    - f. Adjust the sensitivity of the Oscilloscope so the signal displayed is a full grid in amplitude.
    - g. Select the Square Wave Function, and adjust the POSITIVE and NEGATIVE AMPLITUDE Potentiometers for full grid deflection.
    - h. Select the Sine Wave Function, and lower the Generator Board Assembly into place.
    - i. Adjust the SINE ZERO Potentiometer for equal amplitude above and below 0 volts DC.
  - j. Adjust the SINE AMPLITUDE Potentiometer for full grid deflection.
    - k. Select the Ramp Function, and raise the Generator Board Assembly.

- 1. Adjust the RAMP ZERO Potentiometer so the base of the Ramp is at 0 volts DC.
- m. Adjust the RAMP OFFSET Potentiometer so the start of the Ramp is at 0 volts DC.
  - n. Adjust the RAMP AMPLITUDE Potentiometer for full positive deflection.
  - o. Lower the Generator Board Assembly into place.

This completes the Operational Adjustments.

# Frequency Calibration.

- a. Select the Sine Function.
- b. Position the Range Switch to X100, the Range Multiplier to X1, and the Frequency Dial to 0.5.
  - c. Connect the Frequency Counter to the  $50\Omega$  output connector on the Front Panel. Terminate the output in a  $50\Omega$  load at the input to the counter.
  - d. The counter should indicate 50 Hz ±1% of full scale.
- e. Adjust the LOWER DIAL CALIBRA-TION Potentiometer for a reading of 50.00 Hz. (20.00 msec.).
  - f. Position the Frequency Dial to 10.

- g. Adjust the UPPER DIAL CALIBRA-TION Potentiometer for a reading of 1,000 KHz.
- h. Repeat step e to g as required.
  - i. Position the Range Switch to X1K, and raise the Generator Board Assembly
  - j. Adjust the variable capacitor on the Range Board (along the left side rail) for a reading of 10.00 KHz.
  - k. Lower the Generator Board Assembly, and position the Range Switch to X100K.
  - 1. Adjust the variable capacitor in the center of the Generator Board for a reading of 1.000 MHz.
  - m. Check Step i. There is some interaction between these adjustments; if necessary repeat Step i. through k.

# Frequency Control Adjustments:

- a. Position the Range Switch to X1K, and the Range Multiplier to X1.
- b. Adjust the Frequency Dial until the counter indicates exactly 500 Hz.
- c. Short the F.C. Input terminals.
- d. If the frequency changes, as shown on the counter, adjust the F.C.ZERO Potentiometer while alternately opening and shorting the F.C. Input terminals, until the frequency no longer changes.

- e. Apply an exact +4.7500 volts to the F.C Input.
- f. Adjust the F. C. CALIBRATION Potentiometer for a reading of 10.00 KHz.

This completes the Frequency Calibration Procedure.

#### SPECIFICATION VALIDATION:

Prior to performing the specification validation, ensure that the operational and calibration adjustment procedures have been performed completely.

Before rejecting an instrument for inability to meet all specifications, be certain the test equipment specifications are equal to, or better than, those given in the list of required test equipment.

The following test equipment is required to validate the Model F210A specifications.

Electronic Counter, Hewlett-Packard, Model 5246L, or equivalent.

Time Interval Unit, Hewlett-Packard, Model 5262A, or equivalent.

Distortion Analyzer, Hewlett - Packard, Model 333A, or equivalent.

Distortion Meter, Boonton Electronics Corporation, Model 85B, or equivalent.

Oscilloscope, Tektronix, Model 547, or equivalent.

Differential Amplifier Plug-In, Tektronix, Model 1A5, or equivalent.

RMS-VTVM, Hewlett-Packard, Model 410C or equivalent.

Digital Multimeter, Cimron, Model 7650, or equivalent.

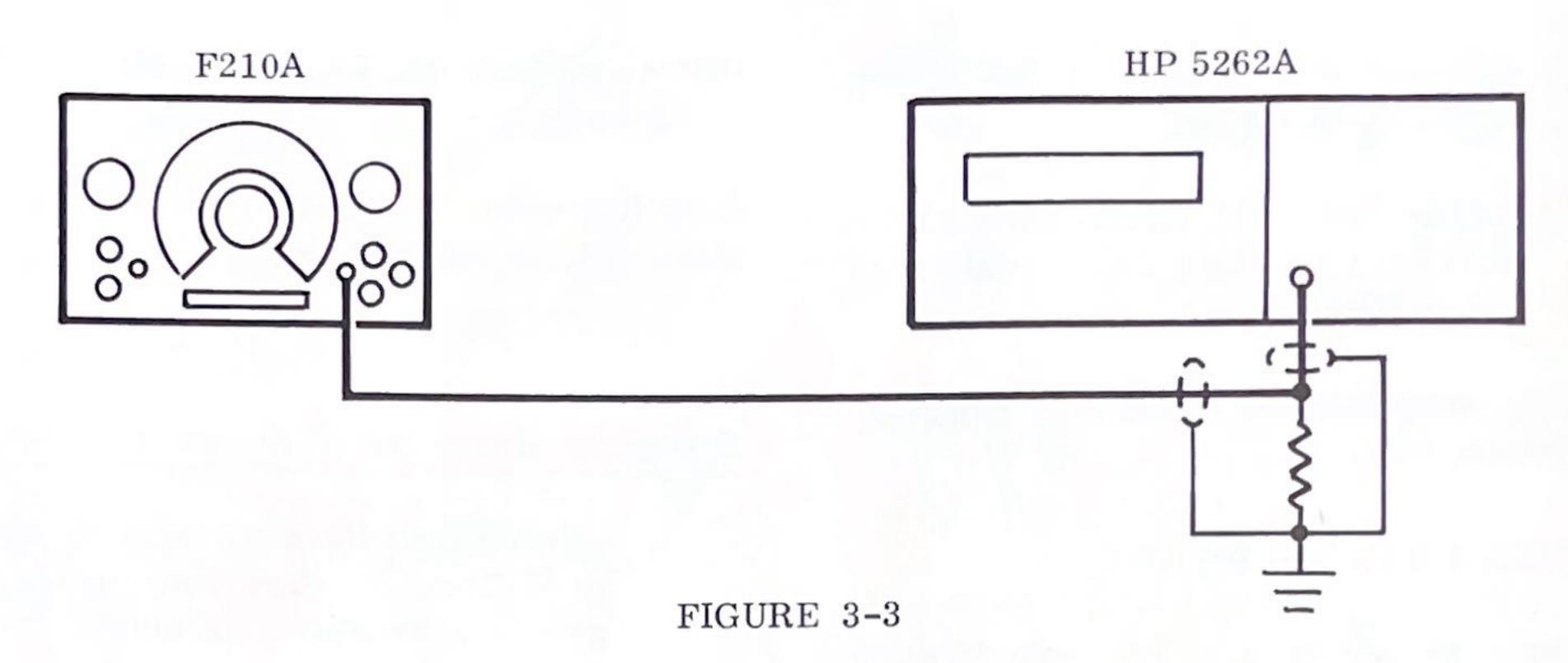
Strip Recorder, Clevite-Brush, Model Mark 220, or equivalent.

# Frequency Range and Calibration Accuracy:

- 1. Interconnect the equipment as shown in Figure 3-3, observing signal and ground connections carefully.
- 2. Position F210A controls as follows:

a	. Function	Sine
b	. Frequency Range	X.01
c	. Range Multiplier	X1
d	. Frequency Dial	1
е	. Attenuator	0dB
f	. Amplitude	Mid-
		range

- 3. Observe that the counter indicates a time interval of 100.0 seconds ±1% of full scale.
- 4. Position the Range Switch to X.1
- 5. Observe that the counter indicates a time interval of 10.00 seconds ±1% of full scale.
- 6. Position the Range Switch to X1.
- Observe that the counter indicates a time interval of 1.000 second ±1% of full scale.
- 8. Position the Range Switch to X10.
- 9. Observe that the counter indicates a time interval of 100.0 msec ±1% of full scale.
- 10. Position the Range Switch to X100.

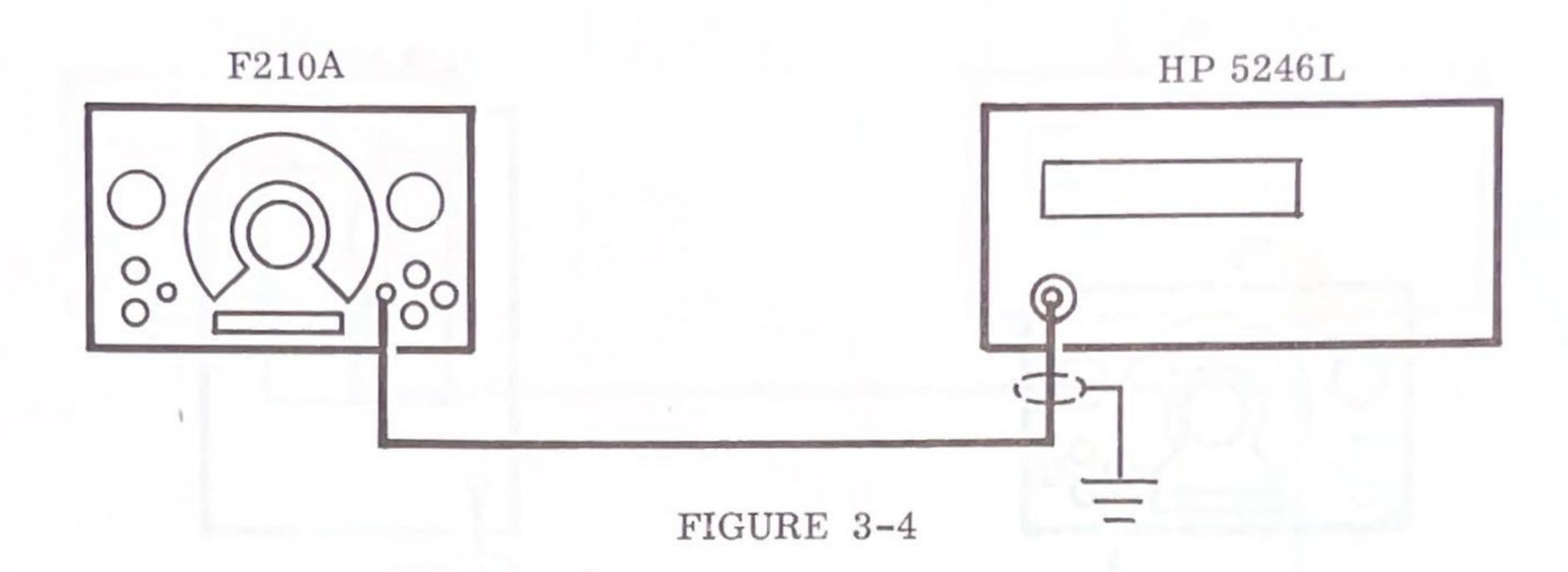


- 11. Observe that the counter indicates a time interval of 10.00 msec ±1% of full scale.
- 12. Position the Frequency Dial to 10.
- 13. Observe that the counter indicates a time interval of 1.000 msec ±1%.
- 14. Position the Range Switch to X10.
- 15. Observe that the counter indicates a time interval of 10.00 msec  $\pm 1\%$ .
- 16. Position the Range Switch to X1.
- 17. Observe that the counter indicates a time interval of 100.0 msec  $\pm 1\%$ .
- 18. Position the Range Switch to X.1
- 19. Observe that the counter indicates a time interval of 1.000 second ±1%.
- 20. Position the Range Switch to X. 01.
- 21. Observe that the counter indicates a time interval of 10.00 seconds ±1%.
- 22. Position the Range Multiplier Switch to X3.
- 23. Observe that the counter indicates a time interval of 3.333 seconds  $\pm 1\%$

of full scale.

- 24. Position the Range Switch to X.1
- 25. Observe that the counter indicates a time interval of 333.3 msec  $\pm 1\%$  of full scale.
- 26. Position the Range Switch to X1.
- 27. Observe that the counter indicates a time interval of 33.33 msec  $\pm 1\%$  of full scale.
- 28. Position the Range Switch to X10.
- 29. Observe that the counter indicates a time interval of 3.333 msec ±1% of full scale.
- 30. Interconnect the equipment as shown in Figure 3-4, observing signal and ground connections carefully.
- 31. Position the Range Switch to X100.
- 32. Position the Range Multiplier Switch to X1.
- 33. Observe that the counter indicates a frequency of 1.000 KHz ±1%.
- 34. Position the Range Switch to X1K.

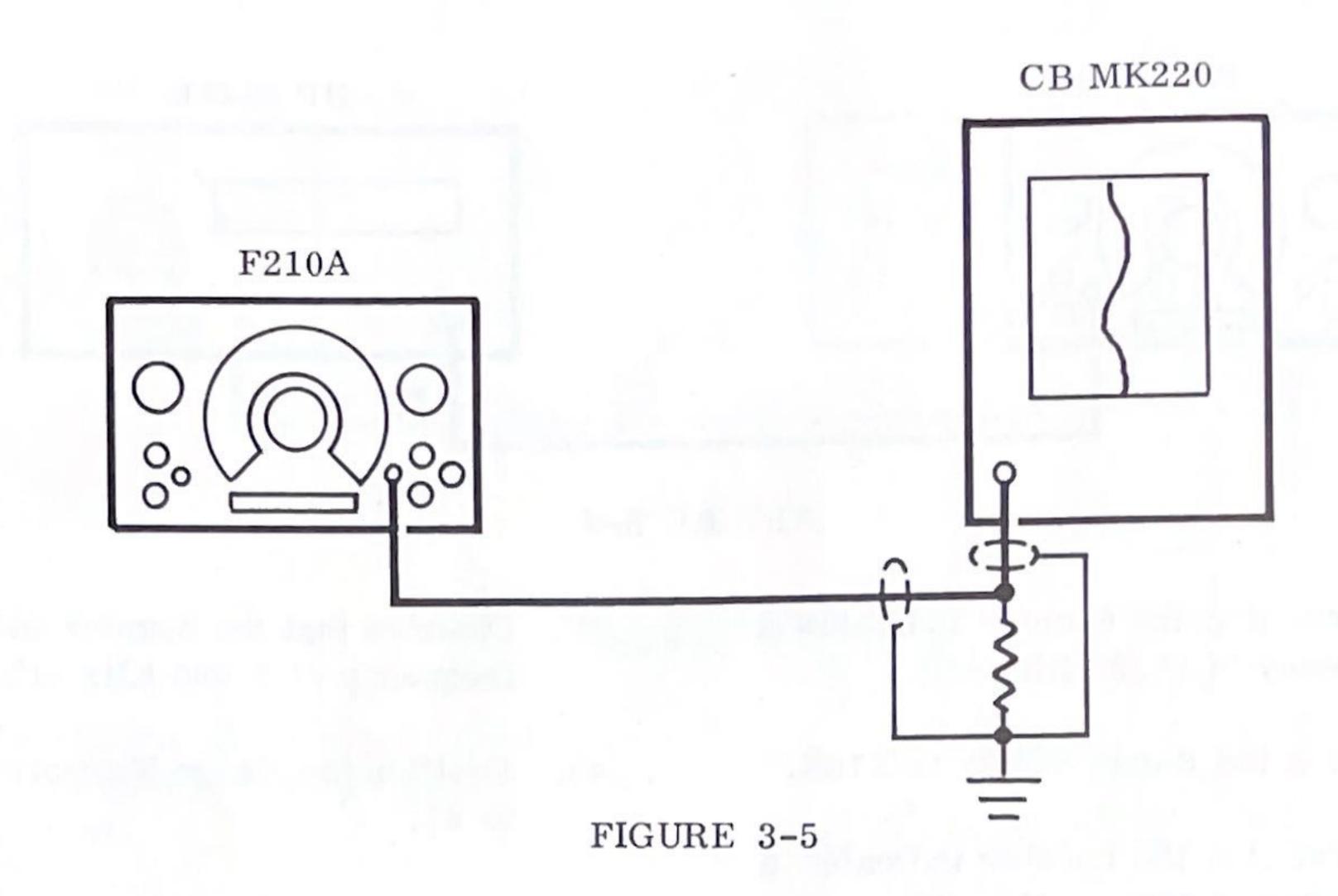




- 35. Observe that the counter indicates a frequency of 10.00 KHz ±1%.
- 36. Position the Range Switch to X10K.
- 37. Observe that the counter indicates a frequency of 100.0 KHz ±1%.
- 38. Position the Range Switch to X100K.
- 39. Observe that the counter indicates a frequency of 1.000 MHz ±2%.
- 40. Position the Range Multiplier Switch to X3.
- 41. Observe that the counter indicates a frequency of 3.000 MHz ±2%.
- 42. Position the Range Switch to X10K.
- 43. Observe that the counter indicates a frequency of 300.0 KHz ±1%.
- 44. Position the Range Switch to X1K.
- 45. Observe that the counter indicates a frequency of 30.00 KHz ±1%.
- 46. Position the Range Switch to X100.

- 47. Observe that the counter indicates a frequency of 3.000 KHz ±1%.
- 48. Position the Range Multiplier Switch to X1.
- 49. Position the Frequency Dial to 1.
- 50. Observe that the counter indicates a frequency of 100.0 Hz ±1% of full scale.
- 51. Position the Range Switch to X1K.
- 52. Observe that the counter indicates a frequency of 1.000 KHz ±1% of full scale.
- 53. Position the Range Switch to X10K.
- 54. Observe that the counter indicates a frequency of 10.00 KHz ±1% of full scale.
- 55. Position the Range Switch to X100K.
- 56. Observe that the counter indicates a frequency of 100.0 KHz ±1% of full scale.



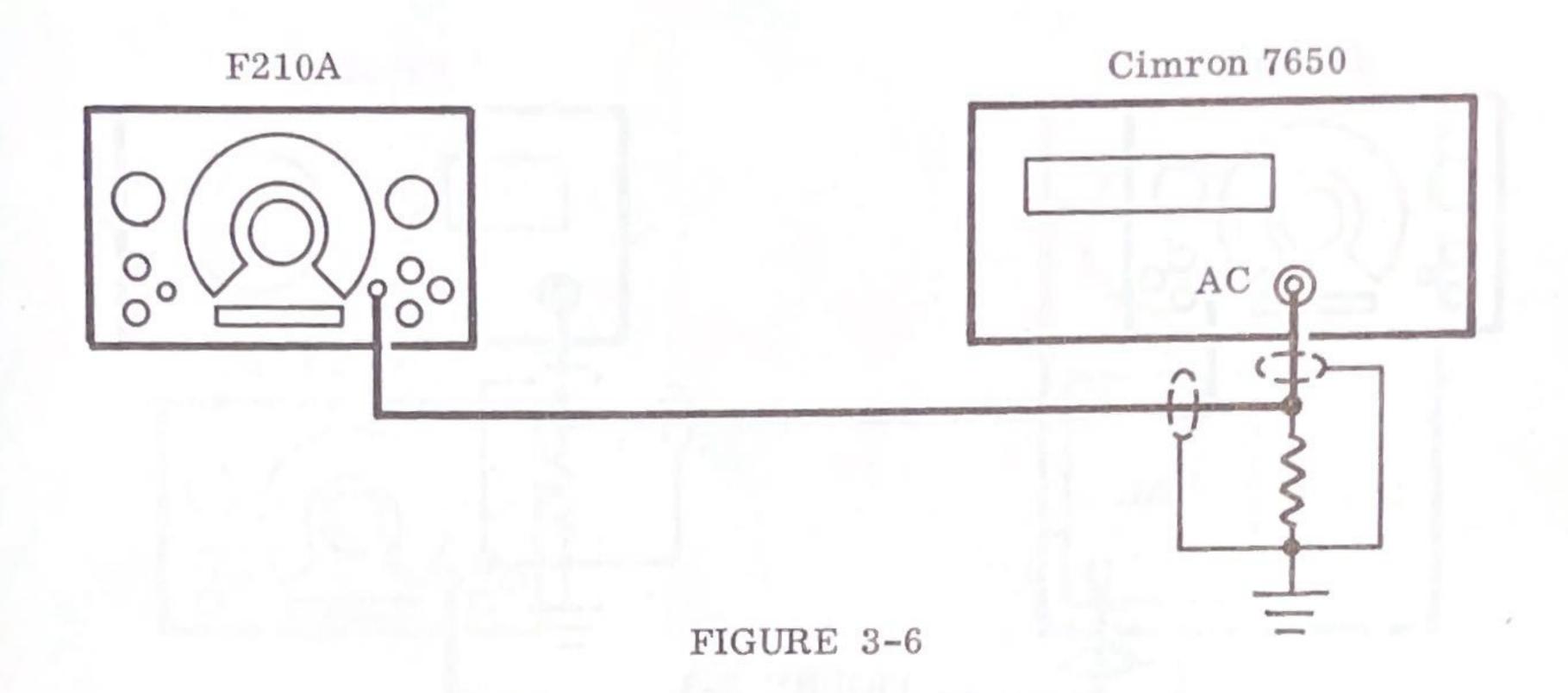


#### Frequency Response:

a.	Function	Sine
b.	Frequency Range	X1
c.	Range Multiplier	X1
d.	Frequency Dial	10
e.	Attenuator	0dB
f.	Amplitude	Mid-
		range

- 2. Interconnect the equipment as shown in Figure 3-5, observing signal and ground connections carefully.
- 3. Adjust the Recorder for 95% deflection of the pen.
- 4. Position the Range Switch to X.1
- Observe that the amplitude is within
   1dB.
- 6. Position the Range Switch to X. 01.
- 7. Observe that the amplitude is within .1dB.

- 8. Position the Frequency Dial to 1.
- 9. Observe that the amplitude is within .1dB.
- 10. Position controls as in Step 1 above.
- 11. Interconnect the equipment as shown in Figure 3-6, observing signal and ground connections carefully.
- 12. Adjust the output of the Model F210A for an indication on the Digital Multimeter of 1,000 volts.
- 13. Position the Range Switch to X10.
- Observe that the amplitude is within
   1dB.
- 15. Position the Range Switch to X100.
- Observe that the amplitude is within
   1dB.
- 17. Position the Range Switch to X1K.
- 18. Observe that the amplitude is within .1dB.



- 19. Interconnect the equipment as shown in Figure 3-7, observing signal and ground connections carefully.
- 20. Adjust the output of the Model F210A for an indication on the Digital Multimeter of 1,000 volts.
- 21. Position the Range Switch to X10K.
- 22. Observe that the amplitude is within .1dB.
- 23. Position the Range Switch to X100K.
- 24. Observe that the amplitude is within .5dB.

- 25. Position the Range Multiplier Switch to X3.
- 26. Observe that the amplitude is within .5dB.

## Distortion (Sine):

a.	Function	Sine
b.	Frequency Range	X1
c.	Range Multiplier	X1
d.	Frequency Dial	5
e.	Attenuator	0dB
f.	Amplitude	Clock-
		wise

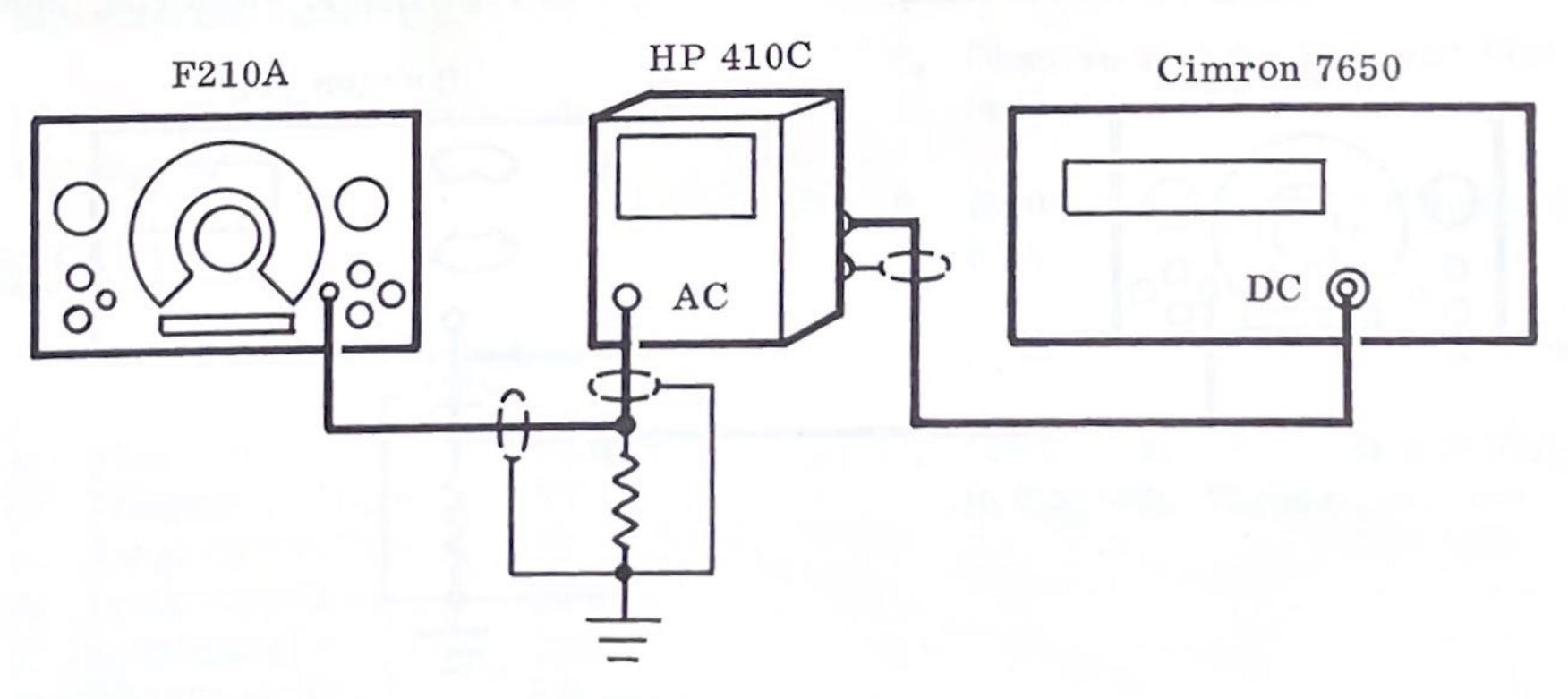


FIGURE 3-7

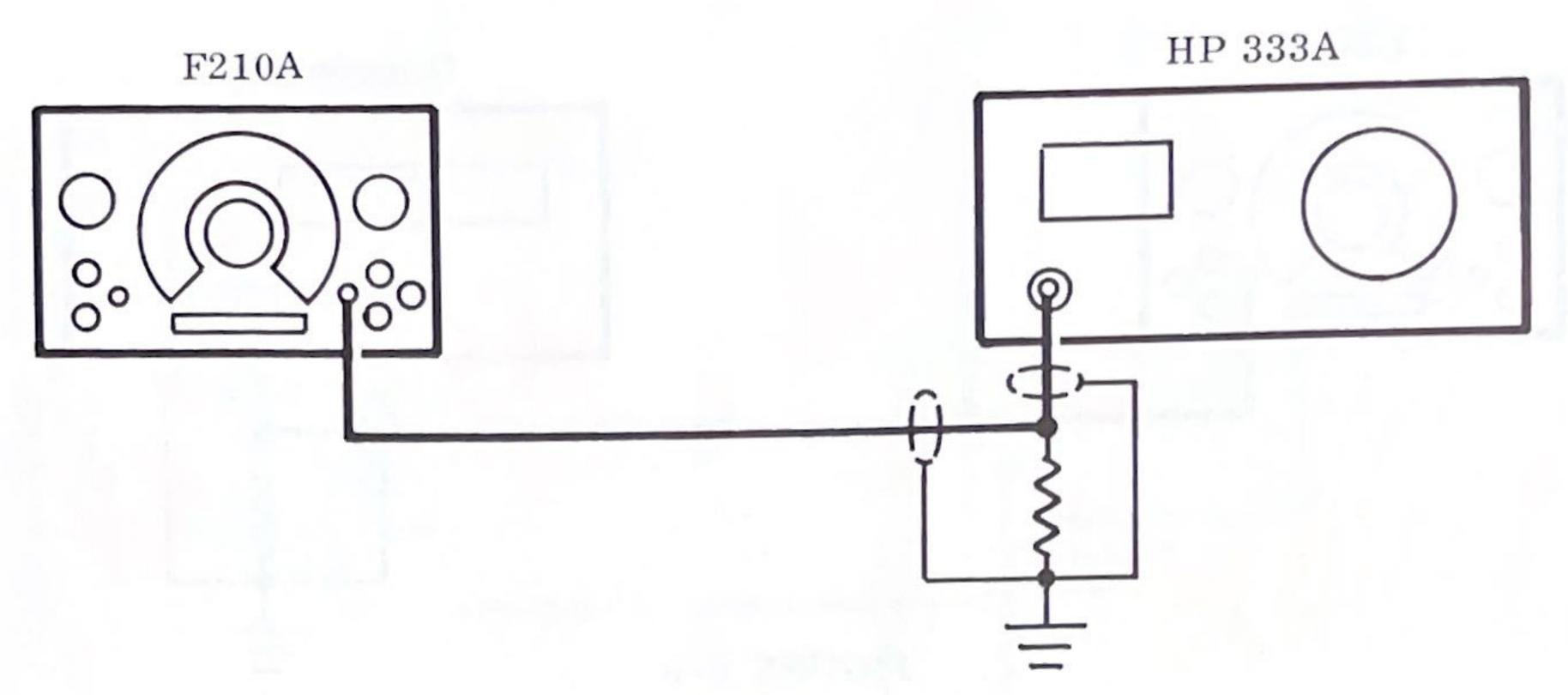


FIGURE 3-8

- 2. Interconnect the equipment as shown in Figure 3-8, observing signal and ground connections carefully.
- 3. Measure the distortion.
- 4. Observe that the distortion does not exceed 1%.
- 5. Position the Range Switch to X10.
- 6. Repeat Steps 3 and 4.
- 7. Position the Range Switch to X100.
- 8. Repeat Steps 3 and 4.
- 9. Position the Range Switch to X1K.

- 10. Repeat Steps 3 and 4.
- 11. Position the Range Switch to X10K.
- 12. Repeat Steps 3 and 4.
- 13. Position the Range Switch to X100K.
- 14. Measure the distortion.
- 15. Observe that the distortion does not exceed 2%.
- 16. Reduce the output amplitude of the F210A.
- 17. Interconnect the equipment as shown in Figure 3-9, observing signal and

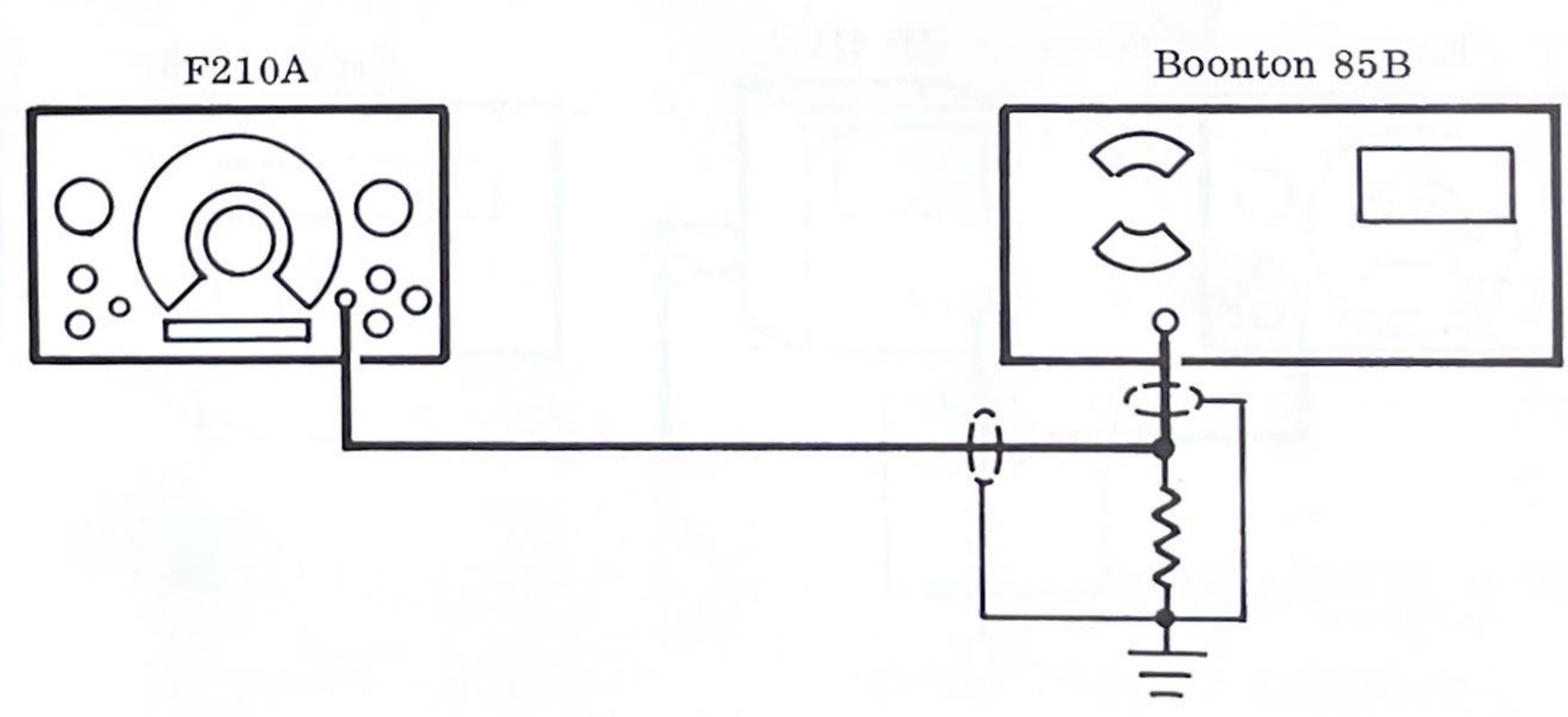


FIGURE 3-9

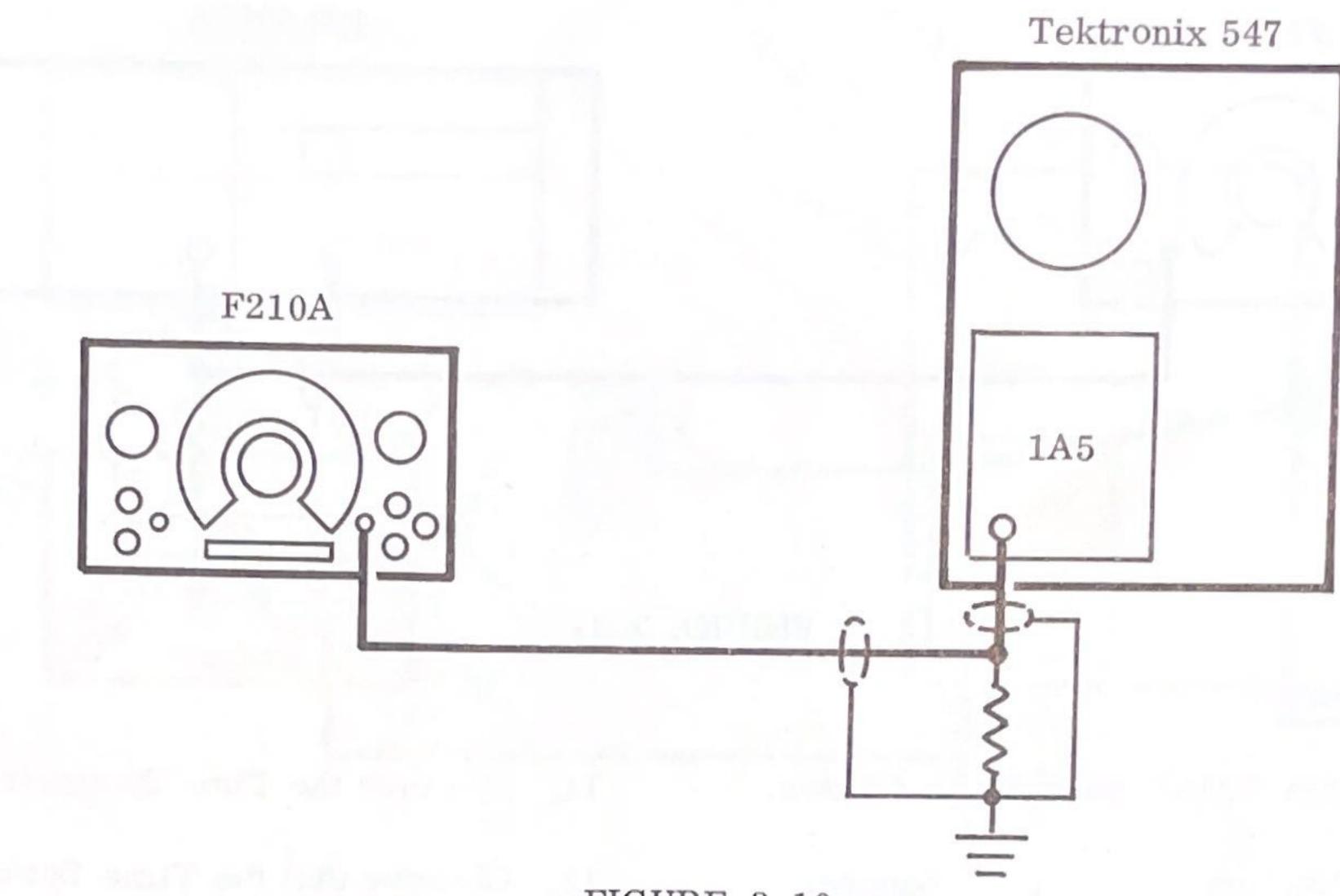


FIGURE 3-10

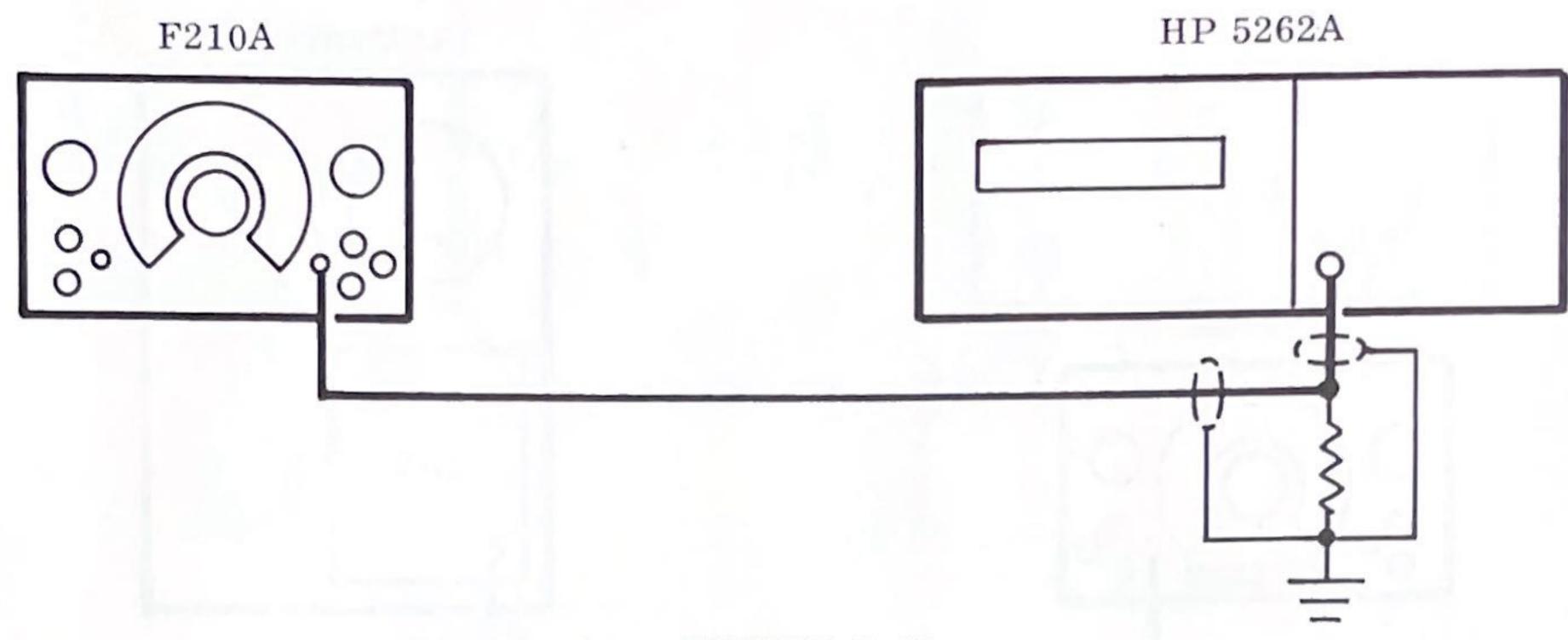
ground connections carefully.

- 18. Position the Frequency Dial to 10.
- 19. Measure the distortion.
- 20. Observe that the distortion does not exceed 5%.
- 21. Position the Range Multiplier Switch to X3.
- 22. Measure the distortion.
- 23. Observe that the distortion does not exceed 5%.

#### Rise and Fall Time:

a.	Function	Square
b.	Frequency Range	X10K
$c_{\bullet}$	Range Multiplier	X1
d.	Frequency Dial	10
e.	Attenuator	0dB
f.	Amplitude	Clock-
		wise

- 2. Interconnect the equipment as shown in Figure 3-10, observing signal and ground connections carefully.
- 3. Measure the Rise and Fall Time.
- 4. Observe that the Rise and Fall Time is less than 75 nsec.
- 5. Position the Range Switch to X100K.
- 6. Measure the Rise and Fall Time.
- 7. Observe that the Rise and Fall Time is less than 75 nsec.
- 8. Position the Range Multiplier Switch to X3.
- 9. Measure the Rise and Fall Time.
- 10. Observe that the Rise and Fall Time is less than 75 nsec.



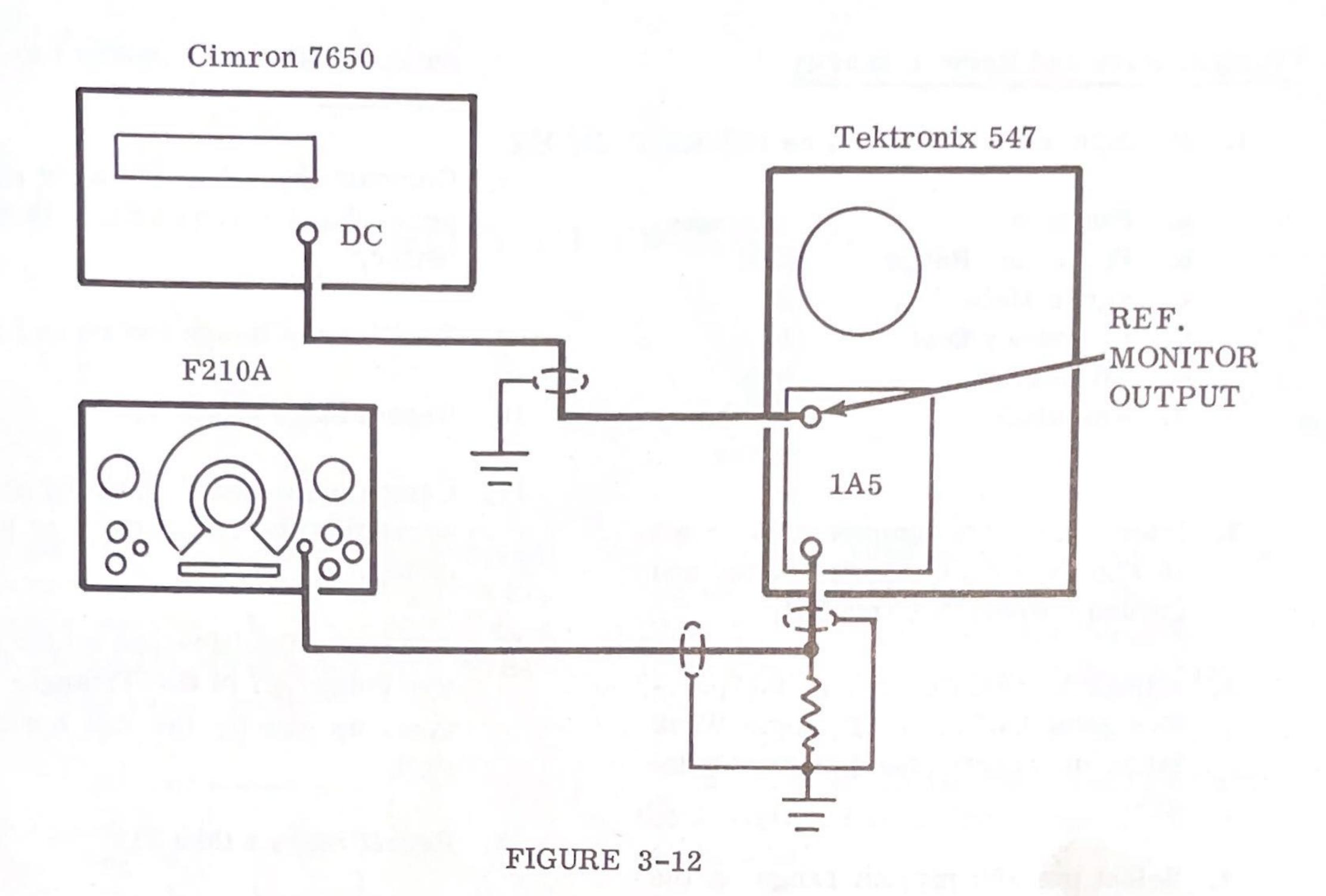
#### FIGURE 3-11

## Time Symmetry:

a.	Function	Square
b.	Frequency Range	X100K
c.	Range Multiplier	X3
d.	Frequency Dial	10
e.	Attenuator	0dB
f.	Amplitude	Clock-
		wise

- 2. Interconnect the equipment as shown in Figure 3-10, observing signal and ground connections carefully.
- 3. Measure the Time Symmetry.
- 4. Observe that the Time Symmetry is 95% or better.
- 5. Position the Range Multiplier Switch to X1.
- 6. Measure the Time Symmetry.
- 7. Observe that the Time Symmetry is 99% or better.
- 8. Position the Range Switch to X10K.
- 9. Repeat Steps 5 and 6.
- 10. Position the Range Switch to X1K.

- 11. Measure the Time Symmetry.
- 12. Observe that the Time Symmetry is 99.5% or better.
- 13. Position the Range Switch to X100.
- 14. Repeat Steps 11 and 12.
- 15. Interconnect the equipment as shown in Figure 3-11, observing signal and ground connections carefully.
- 16. Position the Range Switch to X10.
- 17. Repeat Steps 11 and 12.
- 18. Position the Range Switch to X1.
- 19. Repeat Steps 11 and 12.
- 20. Position the Range Switch to X.1
- 21. Repeat Steps 11 and 12.
- 22. Position the Range Switch to X. 01.
- 23. Repeat Steps 11 and 12.



# Amplitude Symmetry, Overshoot, Preshoot and Tilt:

a.	Function	Triangle
b.	Frequency Range	X1K
c.	Range Multiplier	X1
d.	Frequency Dial	10
e.	Attenuator	0dB
f.	Amplitude	Clock-
		wise

- 2. Interconnect the equipment as shown in Figure 3-10, observing signal and ground connections carefully.
- 3. Select the 100 mv/cm range on the 1A5, and adjust the Reference Supply for 0 indication at the positive peak of the waveform.
- 4. Switch the Reference Supply to -.

- 5. Observe that the negative peak is less than 1% of the peak-to-peak amplitude from the 0 line.
- 6. Select the Sine Function.
- 7. Repeat Steps 3 thru 5.
- 8. Select the Square Function.
- 9. Repeat Steps 3 thru 5.
- 10. Observe that the Overshoot and Preshoot do not exceed 5% of the maximum output of the F210A.
- 11. Observe that the Tilt does not exceed 0.5% of the maximum output of the F210A.

# Triangle Wave and Ramp Linearity:

1. Position F210A controls as follows:

a.	Function	Triangle
b.	Frequency Range	X1K
$c_{\bullet}$	Range Multiplier	X1
d.	Frequency Dial	10
e.	Attenuator	0dB
f.	Amplitude	Clock-
		wise

- 2. Interconnect the equipment as shown in Figure 3-12, observing signal and ground connections carefully.
- Adjust the Oscilloscope so the positive going half of the Triangle Wave takes up exactly the full horizontal grid.
- 4. Select the 100 mv/cm range on the 1A5, and adjust the Reference Supply for 0 indication at the start of the waveform.
- 5. Note and record the reading on the Digital Multimeter.
- 6. Increase the Reference Supply until the waveform intersects the next major vertical mark.
- 7. Repeat Steps 5 and 6 until the desired

- number of check points have been recorded.
- 8. Compute the actual linearity and observe that the linearity is 99% or better.
- 9. Position the Range Switch to X100K.
- 10. Repeat Steps 3 thru 7.
- 11. Compute the actual linearity and observe that the linearity is 95% or better.
- 12. Adjust the Oscilloscope so the negative going half of the Triangle Wave takes up exactly the full horizontal grid.
- 13. Repeat Steps 4 thru 11.
- 14. Select the Ramp Function.
- 15. Position the Range Switch to X1K.
- 16. Adjust the Oscilloscope so the Ramp takes up exactly the full horizontal grid.
- 17. Repeat Steps 4 thru 11.

This completes the Specification Validation.

## SECTION IV

# THEORY OF OPERATION

The generation of a triangular wave form is fundamental to all other wave forms in a waveform generator. It is generated as a function of the characteristics of a circuit referred to as an integrator.

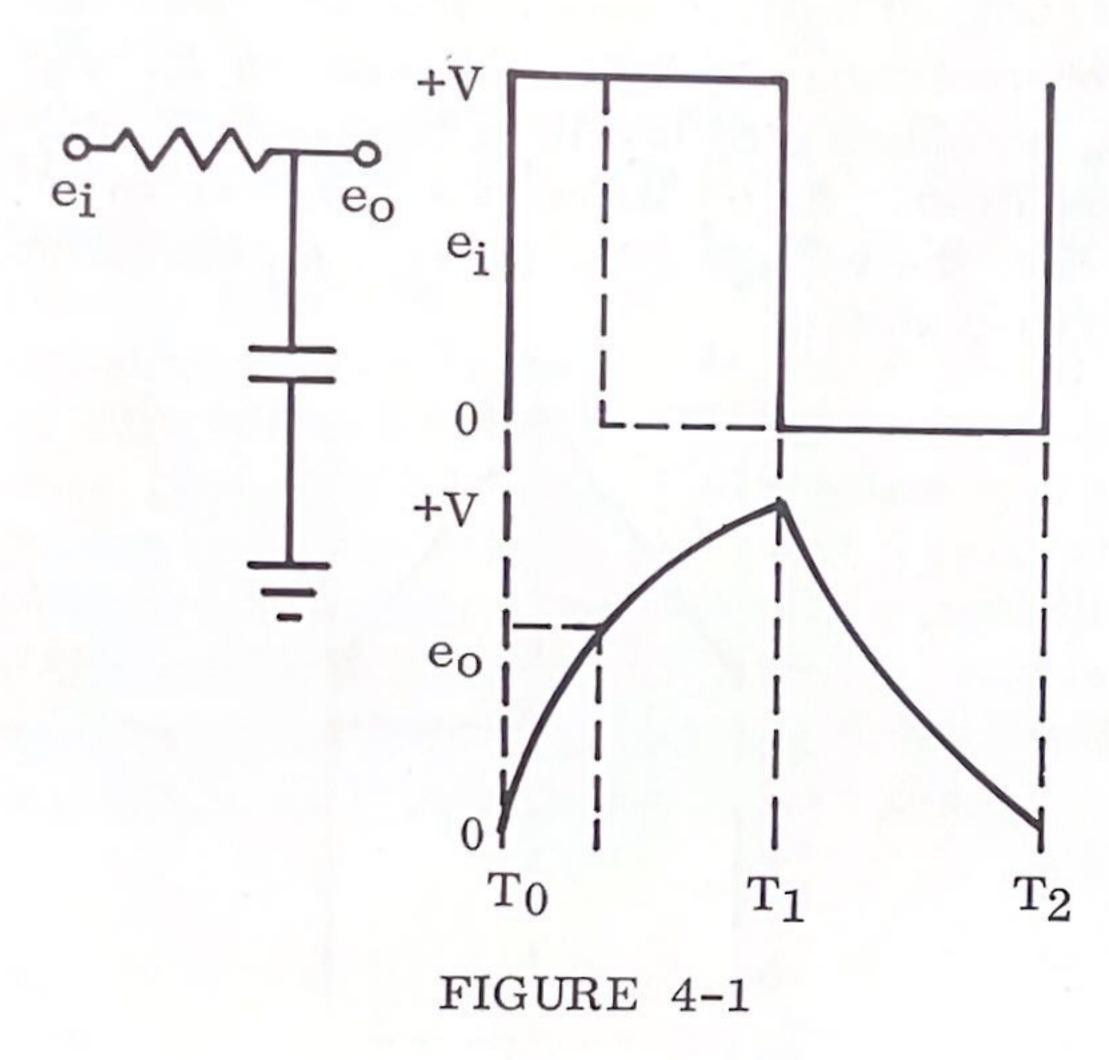
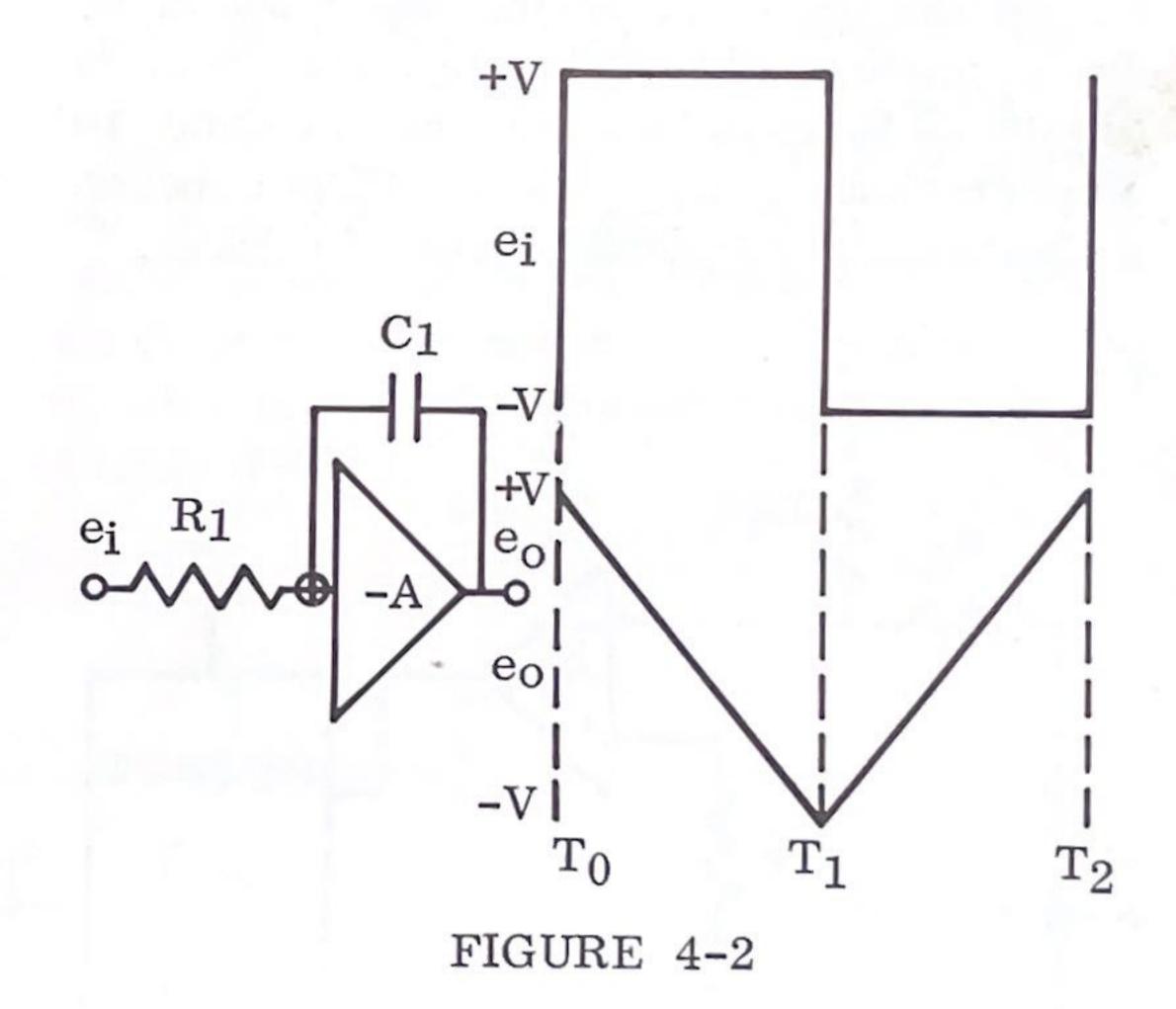


Figure 4-1 depicts a passive integrator. Assuming a step change in voltage to some positive value occurs at time  $T_0$ , the voltage drop across  $C_1$  in the above circuit is equal to zero. As time  $T_1$  approaches, the charge across  $C_1$  increases and the voltage drop across  $R_1$  decreased. In accordance with Ohm's law, the current through  $R_1$  varies in direct proportion to the voltage across  $R_1$ . Therefore, as the charging rate of  $C_1$  decreases, the current through  $R_1$  also decreases. During the first increment of time the charging rate of  $C_1$  is fairly linear.

The quality of integration improves as RC and/or frequency is increased. As illustrated in Figure 4-1, the linearity of  $\rm E_0$  is inversely proportional to the amount of  $\rm E_0$ 

In order to utilize this characteristic, the operational amplifier integrator of Fig. 4-2 is used.



The rate of integration is approximately the same as the initial rate of integration of a passive integrator. However, the addition of an operational amplifier serves to maintain the charge of C<sub>1</sub> at a constant rate. In an operational amplifier the voltage appearing at the summing junction is equal to zero. Therefore, the voltage drop across R<sub>1</sub> is equal to the applied voltage, and the current

through  $R_1$  is constant. Assuming a perfect a mplifier of infinite input resistance is used, the current through  $R_1$  serves as the charging current for  $C_1$ .  $R_1$  is usually a high precision, low temperature coefficient resistor.

For larger capacitor values, the integrating capacitor is usually made of polystyrene or other very low leakage material. Amplifier gain should be high enough to assure that the summing junction is maintained as close to zero as practical; movement around zero results in non-linearities in the output voltage. On the other hand, extremely high gain should be avoided to assure proper stabilization.

Referring to Figure 4-2, it can be seen that the output voltage varies inversely as the integral of the applied voltage, the result of the phase inversion experienced in the amplifier. The triangle wave form is developed by switching the input voltage to an operational integrating amplifier between a positive and negative source of voltage.

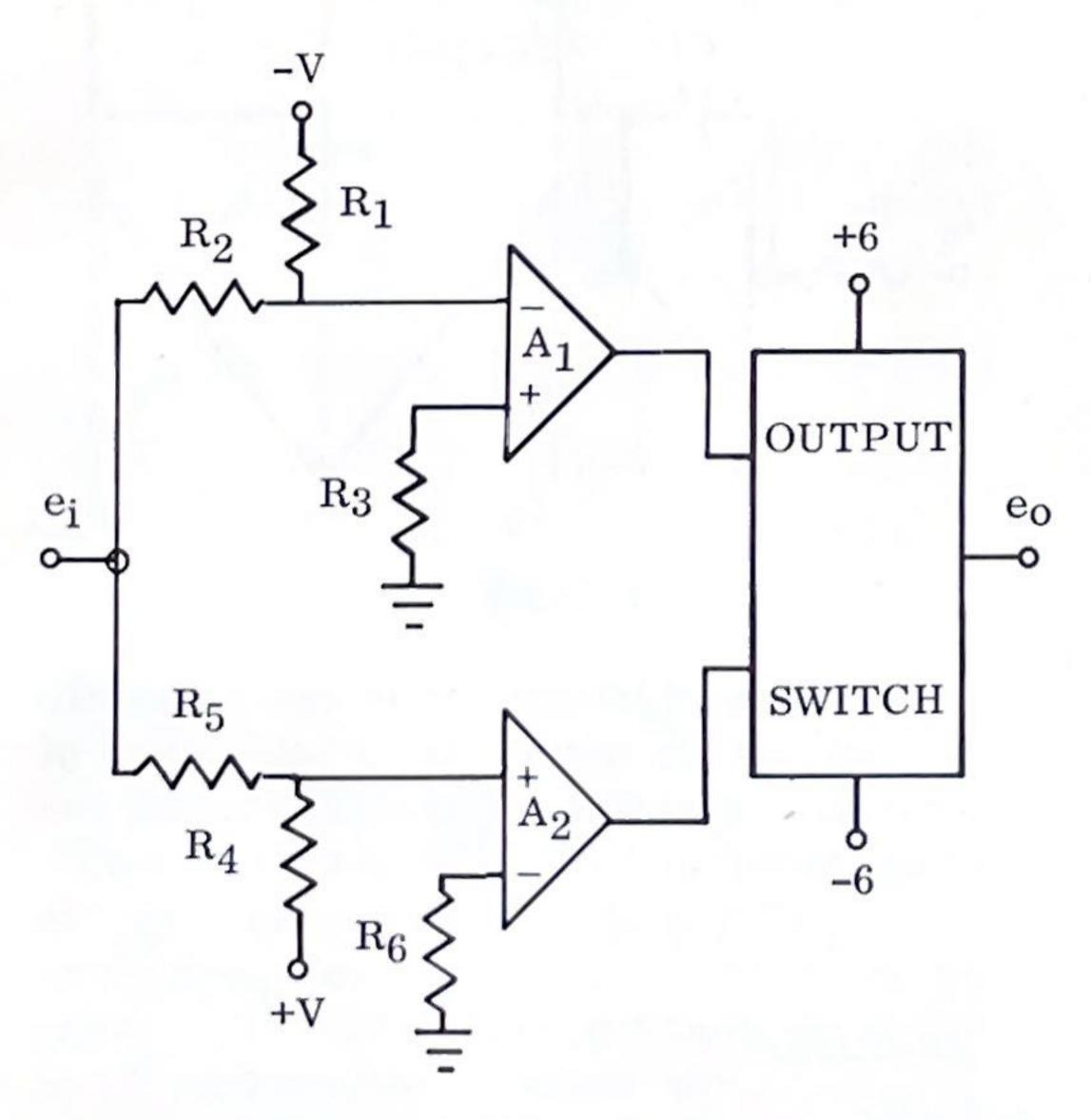


FIGURE 4-3

Square wave generation is accomplished through the use of a level detector in conjunction with the triangle wave form from the integrator. A basic circuit is depicted in Figure 4-3.

In the circuit, A<sub>1</sub> and A<sub>2</sub> represent differential amplifiers having gains in excess of 1000. The typical output voltage swing is usually limited from 0 to +4 volts. With such a relationship, it can be seen that an input voltage change of more than 4mV will cause the output voltage to limit at 0 or +4 volts. It is this feature that is utilized in the level detector. The amplifiers are referenced through resistors R3 and R6 to ground, respectively. In one case the inverting (-) input is used and in the other the non-inverting (+) input. Resistors R<sub>1</sub> and R<sub>4</sub> establish bias levels at the input of each amplifier. As e increases from -1 to +1 volts, the voltage at the input of A2 becomes more positive.

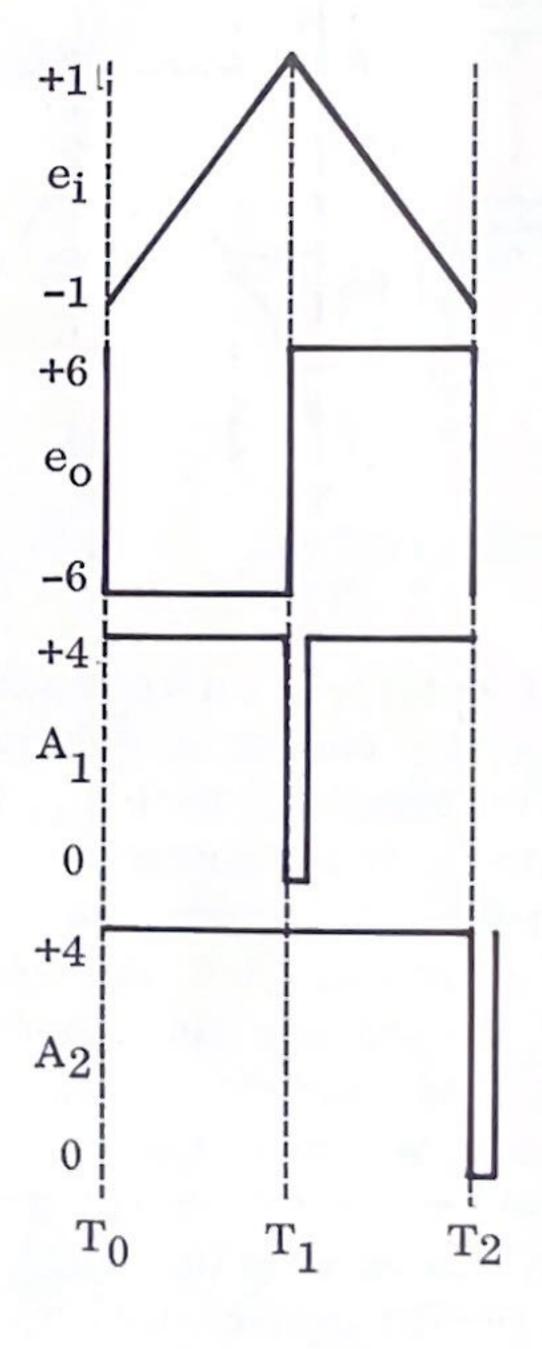


FIGURE 4-4

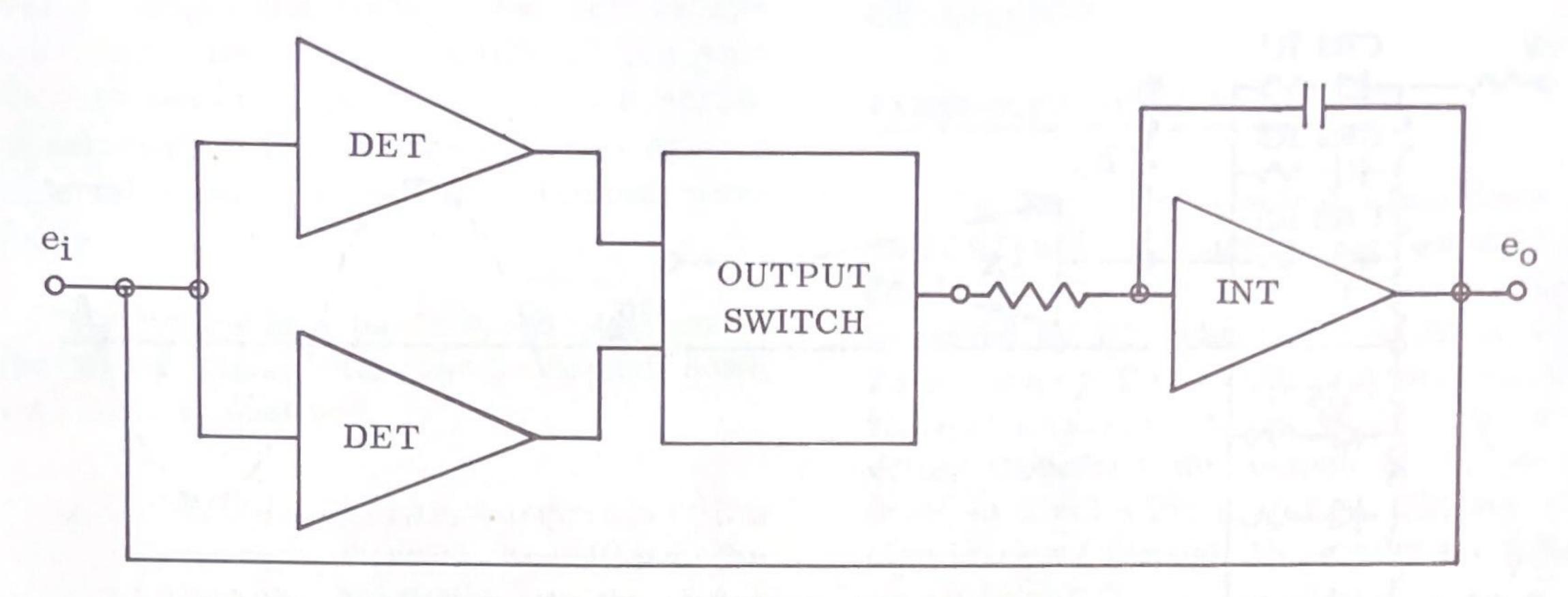


FIGURE 4-5

During the transition from -1 to +1 volts, the outputs of A1 and A2 are held positive. At time T1, ei reaches +1 volt and the voltage appearing at the inverting (-) input of A<sub>1</sub> becomes equal to 0 volts. The output of A<sub>1</sub> drops to 0 volts, where it remains until ei reverses direction and begins to approach -1 volts. At time T2 the procedure is reversed. The output voltage of A2 drops to 0 volts during the period of time ei equals -1 volt. The negative going pulses from the outputs of A 1 and A 2 are in turn used to switch a tunnel diode/transistor combination to produce a 12V p-p square wave with the phase relationship to the input waveform as illustrated in Figure 4-4.

It will be noted that the generation of the triangle wave form is the result of supplying a square wave to the input of the integrating amplifier. Figure 4-5.

Aberrations at the top or bottom of the square wave effect the linearity of the triangle wave form since the rate of integration is dependent upon the amplitude of input signal. To remedy this situation, the square wave is used only to steer the charging current of the integrator to a constant current generator. The manner in which this is accomplished is depicted in Figure 4-6

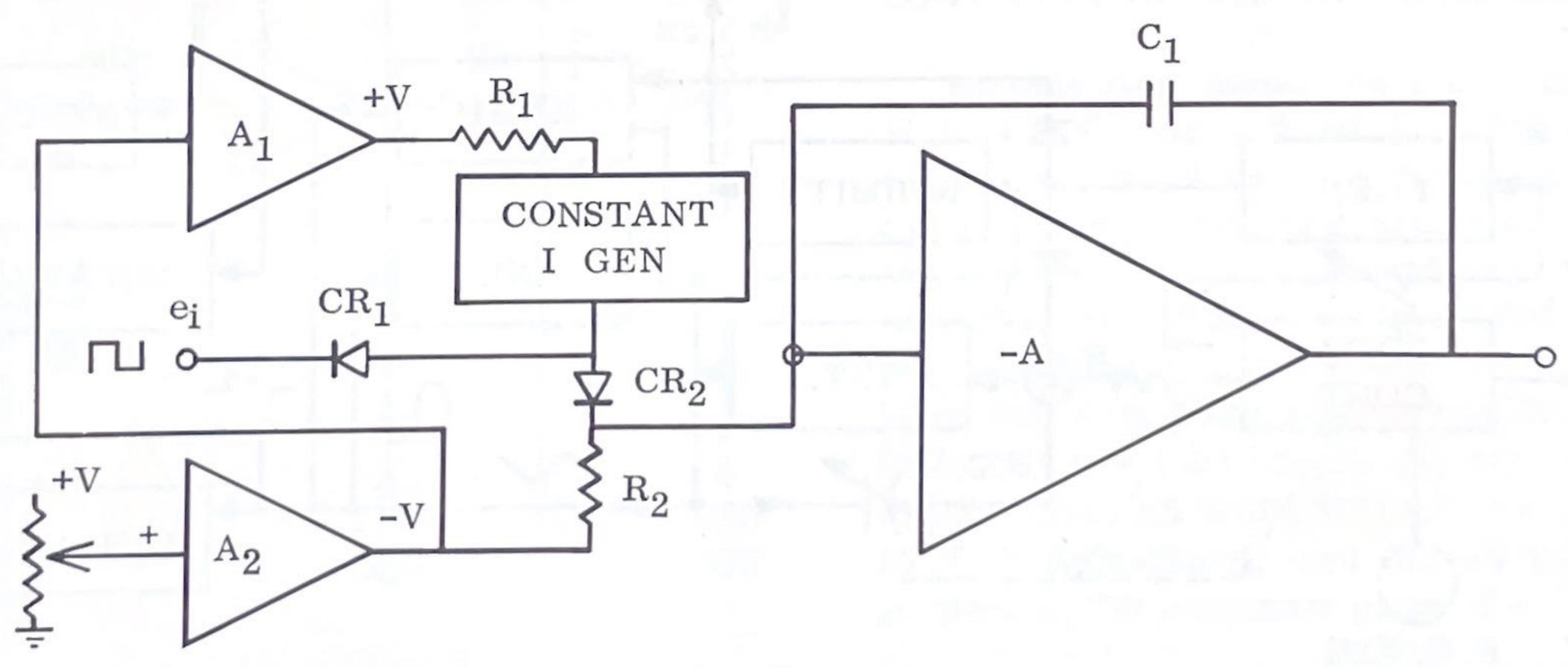


FIGURE 4-6

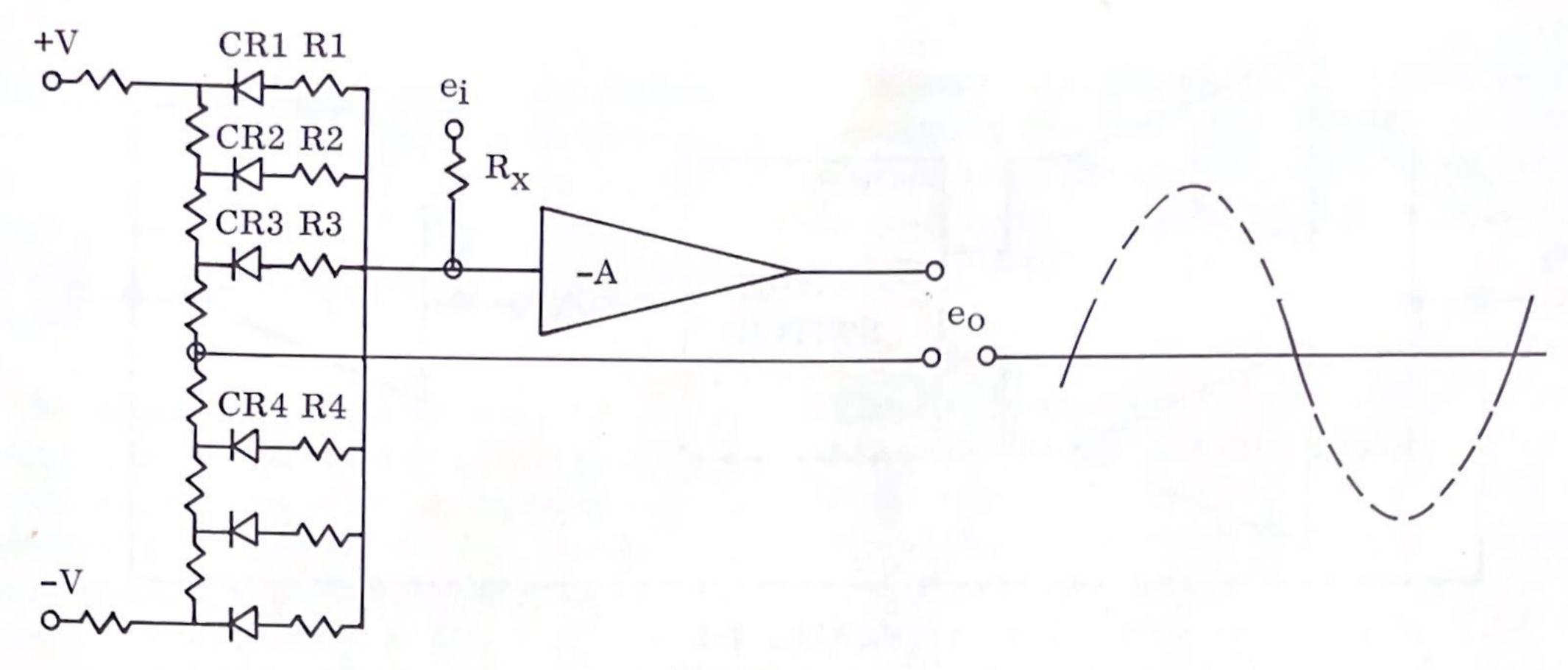


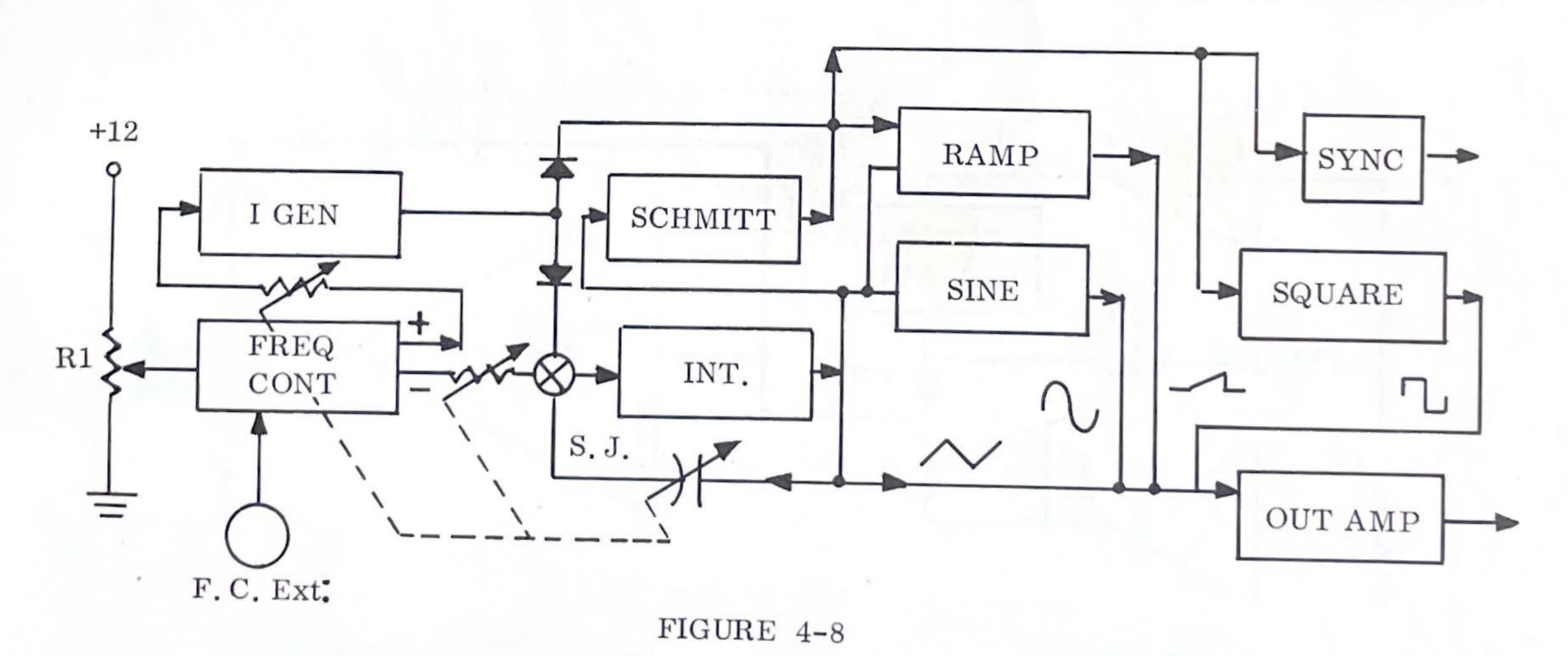
FIGURE 4-7

During the period of time input voltage  $e_i$  is at some positive value, diode  $CR_1$  is reversed biased. Diode  $CR_2$  is forward biased due to the polarity of the voltage appearing at the output of the voltage control amplifiers  $A_1$  and  $A_2$ . The constant current generator maintains the current through  $R_1$  at a value equal to twice the current through  $R_2$ . The additional current is supplied from the integrator, causing  $C_1$  to discharge at a linear rate. During the period of time  $e_i$  is at some negative value, diode  $CR_1$  is forward biased and  $CR_2$  is reversed biased. current through  $R_1$  is supplied from the input.  $C_1$  charges at a rate determined by

the current through R<sub>2</sub>. Variations in the square wave amplitude are thus eliminated as a source of distortion.

The triangular wave form is synthesized into a sine wave by means of the circuit shown in Figure 4-7.

Diodes  $CR_1$   $CR_2$  and  $CR_3$  are biased at different levels as determined by their respective positions along a voltage divider. As the input voltage increases from 0 to some positive value of voltage the diodes  $CR_1$  and  $CR_2$  sequentially conduct. A voltage division occurs between  $R_X$  and the respective resistor associated with each diode



which changes the slope of the voltage applied to the input of an amplifier. The sine wave output is approximated from a series of segments. The number of segments used determines the purity of the resulting wave form.

Figure 4-8 is a basic block diagram of the Model F210A which can be broken down into several sections.

- a. The Generator, comprised of the Frequency Control Amplifiers, the Integrating Amplifier, the Schmitt Trigger, and a Constant Current Generator.
- b. Shaping Amplifiers for the Sine, Square and Ramp Functions.
- c. A separate amplifier provided to deliver a Sync signal.
- d. The Output Amplifier, which is necessary to deliver the required output power, and the proper impedance matching.

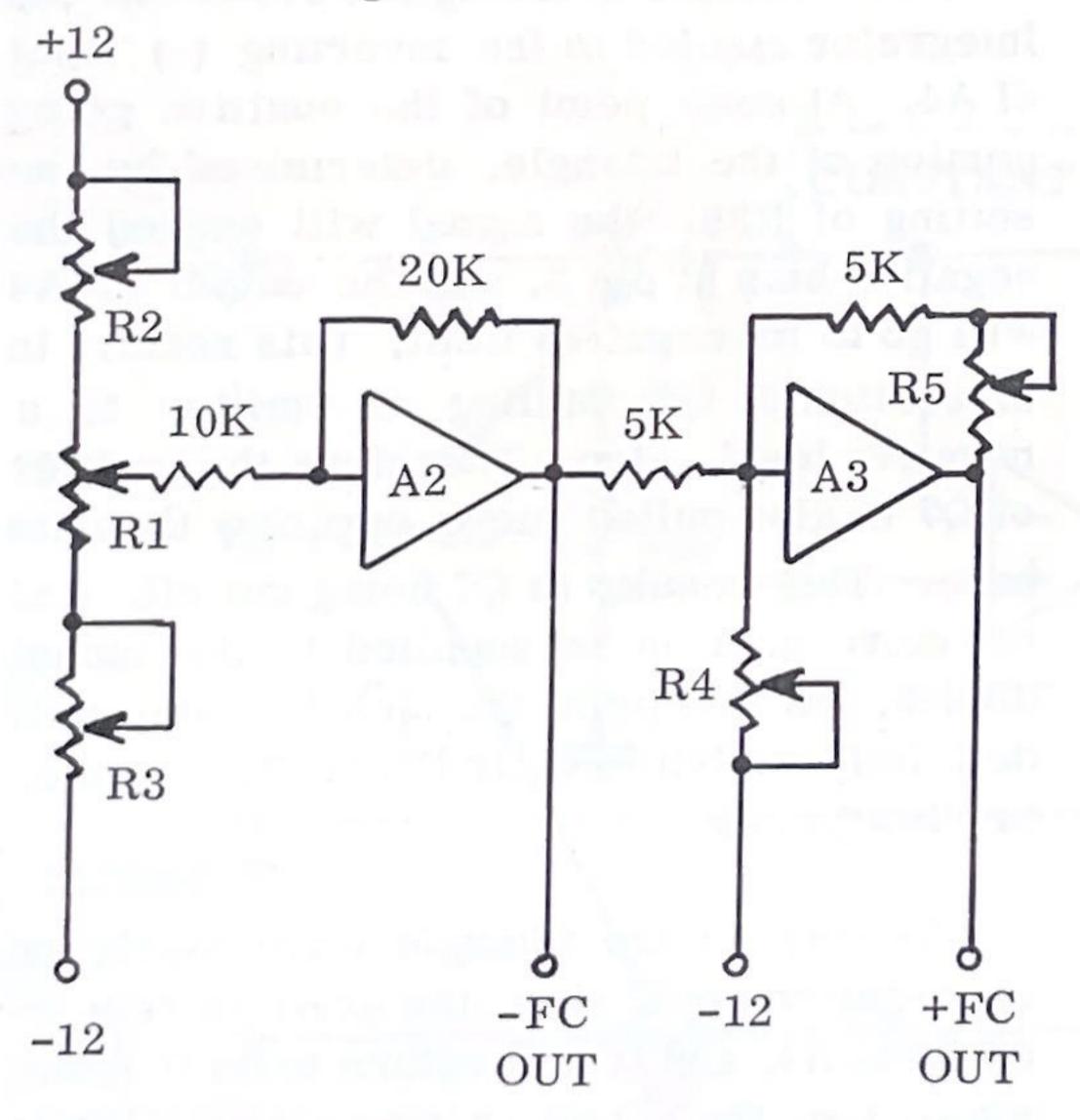


FIGURE 4-9

#### GENERATOR

#### Frequency Control Amplifiers:

The Frequency Control Amplifiers are essentially a pair of inverting DC amplifiers (Figure 4-9). The input signal is varied by R1, which is the Front Panel Frequency Control Potentiometer. This voltage is variable from +0.25 volts to +5 volts, therefore the output of A1 swings from -0.5 volts to -10 volts. The signal is also inverted through A3, giving a + voltage output from A3.

R2 is the UPPER DIAL CALIBRATION Adjustment, and simply determines the maximum positive voltage available at the top of the Frequency Control Potentiometer, and therefore the highest frequency. R3, likewise, determines the minimum voltage available at the bottom of the Frequency Control Potentiometer, and is the LOWER DIAL CALIBRATION Adjustment.

The output from A2 (-F.C.) swings from -0.5 volts to -10 volts, and is applied through a resistor to the Summing Junction of the Integrating Amplifier. The same signal is also applied to the input of A3. The input to A3, however, is offset by approximately -5 volts through R4, which is the LOWER DIAL SYMMETRY Adjustment.

R4 thus determines the minimum point of the + F.C. output from A3. The - F.C. output from A2 delivers a fixed amount of current to the Summing Junction during the half cycle when the integrating capacitor is charging. R4, therefore, is needed to ensure that the same amount of current is taken out of the Summing Junction during the half cycle when the integrating capacitor is discharging. R5 is the UPPER DIAL SYM-METRY Adjustment, and serves the same purpose at the maximum point of + F.C.

Schematic #1 (Section V) is the complete schematic of this circuit. Terminals "E", "G" and "F" are the connections to the Frequency Control Potentiometer. "F" is the arm of the pot. The control voltage is applied through R5 to pin 9 of A1, which is a pair of dual emitter followers, providing isolation between the control voltage source and the Frequency Control Amplifiers. The voltage level from A1 is coupled into the inverting (-) input of A2. The non-inverting (+) input of A2 is referenced back to Ground through R11 and the other half of A1. Pin 6 of A1 might be called the differential input, and its DC level is determined by the FRE-QUENCY CONTROL ZERO Adjustment, R18.

The output from A2 is coupled through CR3, which shifts the DC level of the signal to the proper operating point of Q1. Q1 is an emitter follower supplying the required current for the – F.C. network. The output from Q1 is also taken back through R16 to the input, pin 9 of A1. R16 is equal to R5, therefore the overall gain of A1, A2 and Q1 is unity.

A3 gets its input from Q1, through approximately  $5\mathrm{K}\Omega$ , R22, to the inverting (-) input, and the non-inverting (+) input is referenced back to Ground through R26. The output from A3, through emitter follower Q3 and DC level shift diode CR4 is fed back to the input through approximately  $5\mathrm{K}\Omega$ , R27 and R28. The input resistance equals the feedback resistance, therefore the gain of A3 is unity. This output level is used to drive the +F. C. network. Q2 is the current source for CR4 and Q3.

# Schmitt Trigger:

The Schmitt Trigger is essentially a level detector, with a few refinements to ensure a square wave output, whose rise time is extremely fast, see Figure 4-5. Because

aberrations at the top and/or bottom of the square wave would affect the linearity of the triangle wave form from the Integrator, the chief concern is that the Schmitt Trigger deliver a pulse when its input reaches a pre-determined level, and that the pulse has a fast rise time.

Schematic #2 (Section V) is the complete schematic of the Schmitt Trigger.

Assume a static condition of the circuit, when the outputs of both A4 and A5 are positive. A4 being positive will hold Q4 in its cut-off state, and A5 holds Q5 cut off. Q4 holds the emitter of Q7 at some voltage approaching the + supply. Q5 holds the base of Q7 at some voltage, determined by the voltage division of R49 and R50, but which is negative with respect to the emitter of Q7. A certain amount of current, therefore, is supplied by Q7 to the Tunnel Diodes, CR7 and CR8. Whether the tunnel diodes are in their "high" or "low" mode at this point can not be determined.

Now consider a triangle wave from the Integrator applied to the inverting (-) input of A4. At some point of the positive going portion of the triangle, determined by the setting of R39, the signal will exceed the negative bias at pin 3, and the output of A4 will go to its negative limit. This results in saturation of Q4, pulling its emitter to a negative level, also. Therefore the emitter of Q7 is also pulled more negative than its base. This results in Q7 being cut off, and no more current is supplied to the tunnel diodes. At this point the tunnel diodes will definitely switch to their low voltage state, or "low" mode.

As soon as the triangle wave starts on its negative going side, the drive is removed from A4, and it will return to its original state, i.e. the output is positive. While this will ultimately turn Q7 on again, the

amount of current supplied to the tunnel diodes is not sufficient to switch them to the 'high' mode.

When the triangle wave reaches the negative peak and overcomes the reverse bias on A5, the output of A5 goes negative, pulling the base of Q5 negative, thereby turning Q5 on. This results in the emitter of Q5 going to the same negative level, supplying more base current to Q7. The current through Q7 increases and switches the tunnel diodes to their "high" mode.

Because of the tunnel diode action, Q8 acts effectively as a Flip-Flop. When the tunnel diodes are in their "low" mode, Q8 is cut off, and the output is positive. When the tunnel diodes are in their "high" mode, base current is supplied to Q8, and its output is negative.

The switching time of the tunnel diodes is on the order of nano-seconds, so that the square wave output from the Schmitt Trigger does have the fast rise time which is essential for linear integration.

#### Constant Current Generator:

Figure 4-10 shows the Constant Current Generator and the circuitry associated with the current switching to the Integrator.

A6 is a standard differential amplifier, (See Schematic #3) whose output is 0 volts, as long as both inputs are equal. The non-inverting (-) input side is held constant at +5 volts by a simple voltage divider from the +12 volt supply. Q11 is a P-channel FET, which is biased so that it behaves as a variable resistor.

Assume that the voltage at + F.C. changes in a negative direction for some reason, This will result in a negative going signal at the inverting (-) input to A6, and the output of A6 will go in a positive direction. This decreases the conduction of Q11, effectively raising the resistance of Q11. The voltage division between R1 and Q11 is changed, raising the voltage at the inverting (-) input to A6.

The square wave output from the Schmitt

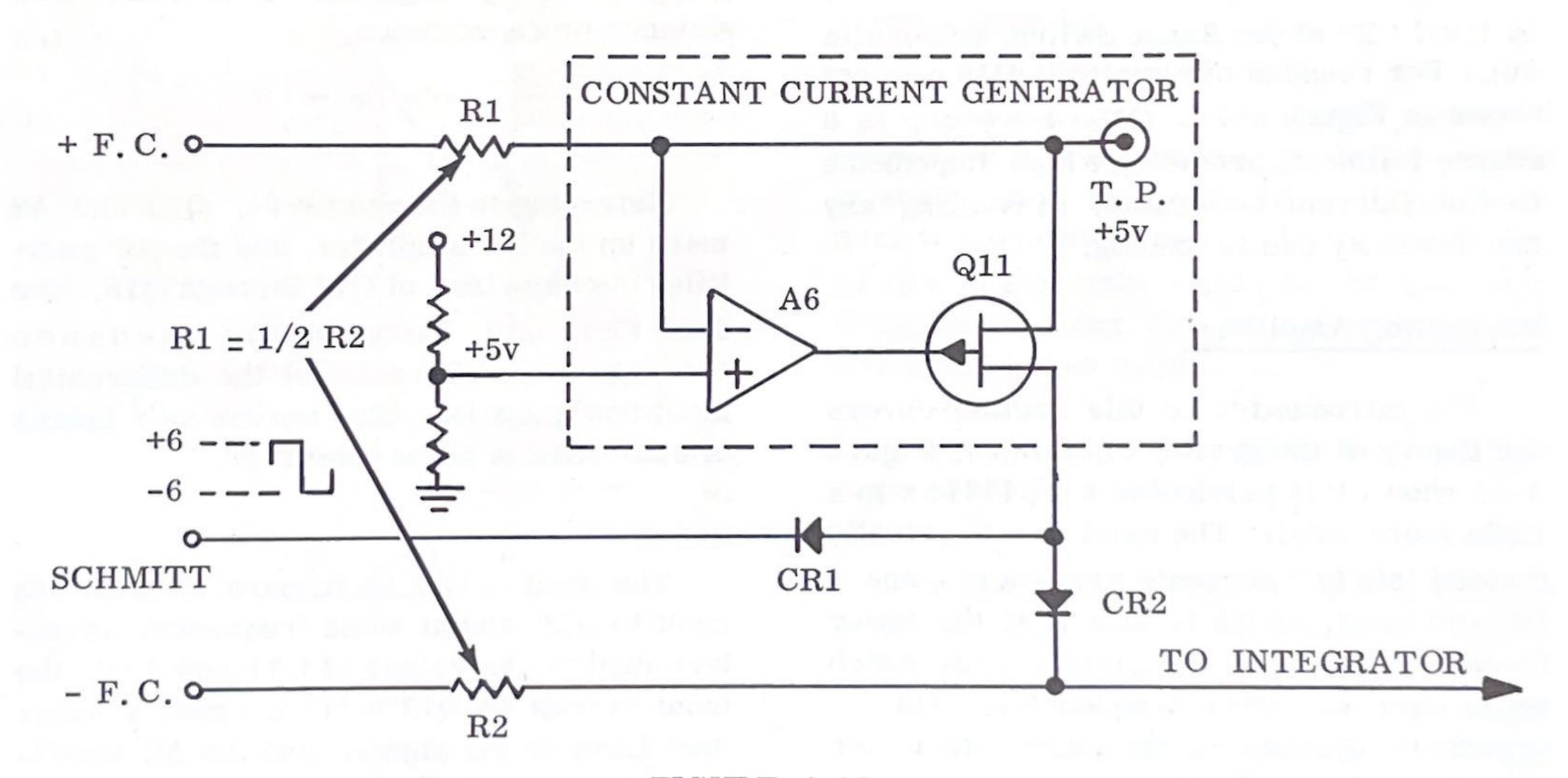


FIGURE 4-10

Trigger is fed into the cathode of CR1, thus when the input is at +6 volts CR1 is backbiased. R1 is 1/2 the resistance of R2, as noted in Figure 4-10. Therefore, regardless of the potential difference between + F.C. and - F.C. the current through R1 is always double the amount of current through R2. When CR1 is reverse biased, the Constant Current Generator maintains the current through R1 at a level equal to twice the current through R2.

The additional current, then, must be supplied from the Integrator, causing the integrating capacitor to discharge at a linear rate.

Similarly, when the input is at -6 volts, CR1 is forward biased, and therefore CR2 is reverse biased. The current through R1 is now supplied from the input, and the integrating capacitor charges at a rate determined by the current through R2.

Referring now to Schematic #3, it will be seen that the resistance between Q11 and + F.C. is a varying value, depending on the range selected. (The resistors are selected by level ''B'' of the Range Switch, Schematic #6). For reasons of simplicity Q10 was not shown in Figure 4-10. Q10, however, is a source follower, providing a high impedance to the Current Generator, preventing any non-linearity due to loading.

#### Integrating Amplifier:

The introduction to this section covers the theory of integrating amplifiers. Figure 4-11 shows this particular amplifier in a little more detail. The amplifier is actually divided into two separate amplifiers, one a DC amplifier, which is active at the lower frequencies, and an AC amplifier, which takes over at higher frequencies. This is necessary because of the bandwidth of the F210A (.005Hz to 3MHz.).

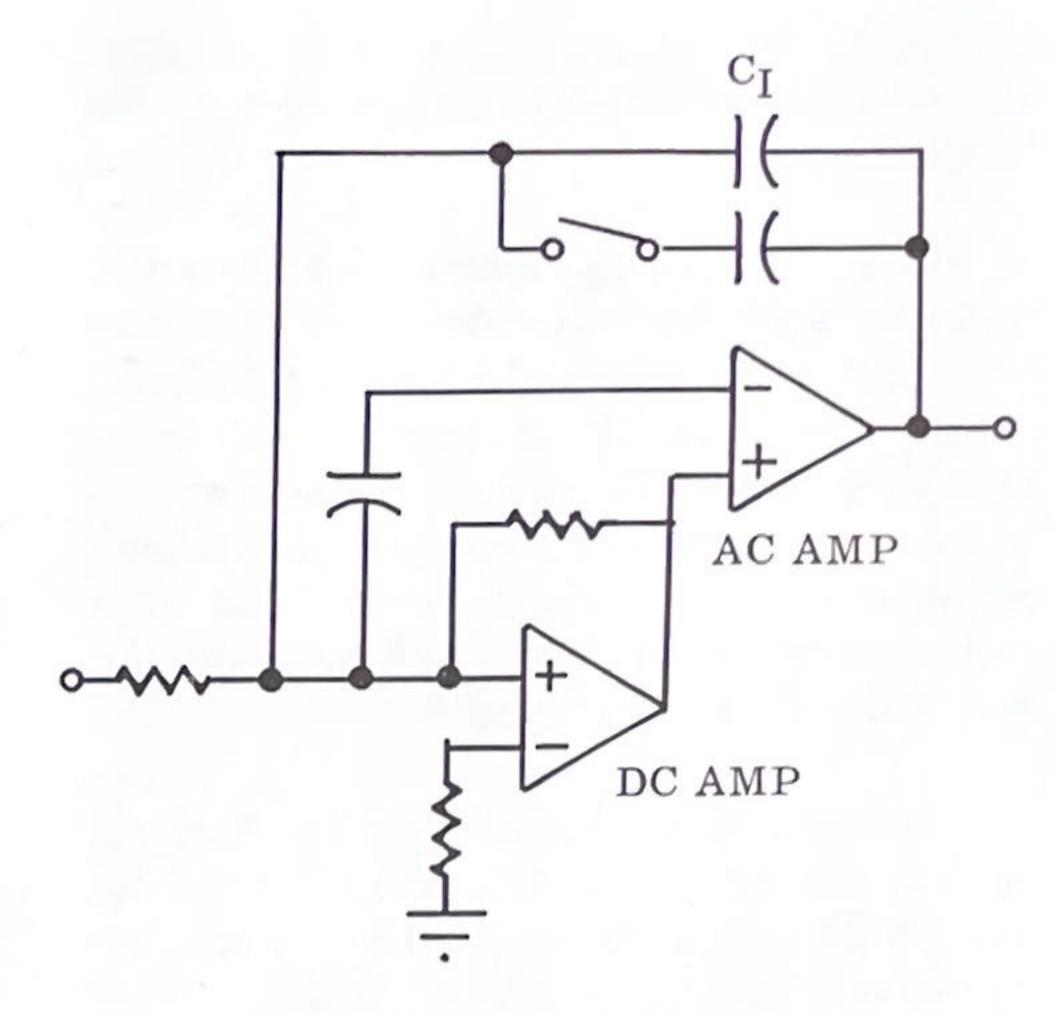
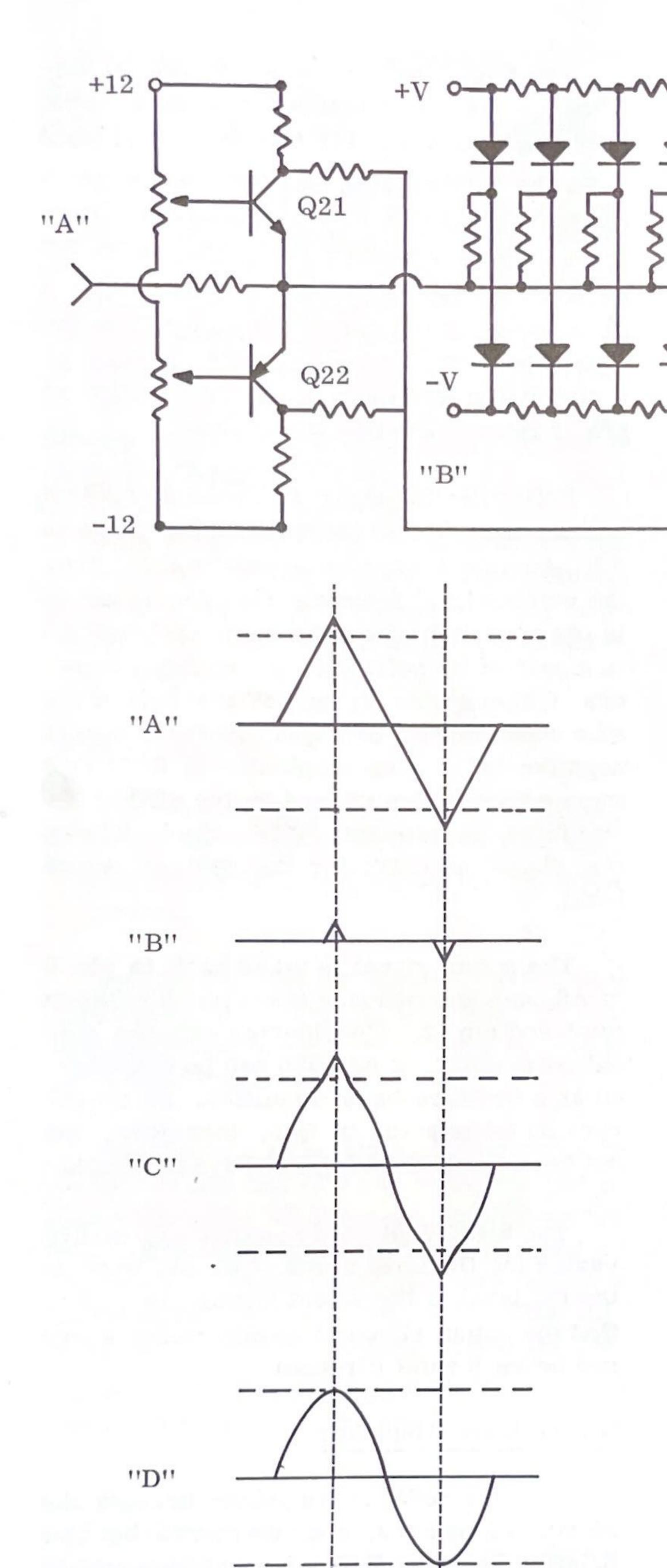


FIGURE 4-11

C1 is the integrating capacitor. The fixed value shown is in the circuit at all times, while the switched value indicates different values being added on various ranges. This is done for reasons of ease of design, as it eliminates the necessity of using extremely large values of either resistance or capacitance.

Referring to Schematic #4, Q12 and A7 make up the DC amplifier, and the AC amplifier is comprised of Q13 through Q18. The dual-FET, Q12, serves as an impedance converter, and because of the differential input configuration, also serves as a means of stabilization of the amplifier.

The input to Q12 is in parallel with the input to Q13, and at some frequency, as determined by the values of C34 and R86, the input circuit to Q13 will present a lower impedance to the signal, and the AC amplifier takes over at this point.



#### SHAPING CIRCUITS

FIGURE 4-12

#### Sine Generator:

As shown in Figure 4-7, the Sine Generator is a synthesizing circuit, which has a triangle wave as its input. CR1 through CR<sub>n</sub> are biased at different DC voltages, determined by their relative position along the voltage divider connected between the + and - power supplies.

Diodes CR1.....CR<sub>n</sub> break down and conduct at increasing voltage levels as the triangle input increases from its negative peak to its positive peak. Therefore the slope of the input signal to the amplifier changes, causing the amplifier output to appear as a sine waveform.

Figure 4-12 shows a more detailed diagram of the Sine Generator.

For ease of drawing, the Sine Amplifier is shown as a simple differential amplifier. In theory the input signal to the non-inverting (+) input side is a sine wave. In practice, however, the signal at point "C" contains a certain amount of peaking. There-

fore the input triangle wave is applied to a pair of non-inverting (Common Base) amplifiers, Q21 and Q22. Q21 and Q22 are biased such that only the peaks of the triangle will cause them to conduct. The output signals from Q21 and Q22 are summed at point "B" and fed into the inverting (-) input side of the differential amplifier.

The input signal at point "C" is distorted by the amount of peaking riding on the sine wave, so by applying only the peaks to the inverting input, the net effect will be that of a subtracting circuit. The final output, thus will be a sine wave with little or no distortion remaining.

Schematic #5 is the complete schematic of the Sine Generator. Q19 and Q20 are the supplies for Q21 and Q22, respectively. As described above, R110 is the NEGATIVE PEAK Adjustment, and determines the point at which Q21 starts conducting. Likewise, R113 is the POSITIVE PEAK Adjustment.

Both sides of the synthesizing network are identical in operation, therefore only the positive side will be discussed. The bases of Q24, 26, 28, 30, 32 and 34 are held at some bias potential, determined by the POSITIVE BREAK Adjustment, R155. The arm of R155 is at +0.7 volts, typically, so the base of Q24 will be at approximately +0.35 volts. The emitters of all these transistors are returned to the -12 volt supply, so the transistors are always conducting. When Q24 is conducting, the voltage across the emitter-base junction is 0.7 volts, so the emitter of Q24 is at approximately -0.35 volts. The drop across CR21 is also 0.7 volts, therefore CR21 will start to conduct, when the input exceeds +0.35 volts. Similarly, CR23 conducts when the input level reaches +0.5 volts, and so on down the line, until at +0.7 volts CR31 conducts.

The Sine Amplifier is a differential amplifier. As is connected in a differential pair configuration. Pin 6 is the signal input from the synthesizing network, while pin 9 is equivalent to the inverting input in Figure 4-12. Pin 9 receives the signal from the peak detectors, as discussed above. Pin 9 also accepts a portion of the output from the Sine Amplifier, so one half of A8 serves as a stabilizing device, because the signal at pin 12 is degenerative (See below).

Following the signal from pin 6 of A8, it will be seen that an inversion takes place in A8. Another inversion occurs in Q36, thus the output signal from the Sine Amplifier is in phase with the input to pin 6. Q37 and Q38 is a pair of complimentary emitter followers. Q37 conducts on the positive half of the sine wave signal, and Q38 conducts on the negative half. The amplitude of the sine wave output is determined by the SINE AMPLITUDE Adjustment, R158, which divides the signal at CR31 for the desired output level.

The output signal is taken back to pin 9 of A8, and an inversion takes place between pin 9 and pin 12. Considering only the signal from pin 12 of A8, Q36 can be considered as a common-base amplifier, so no inversion takes place in Q36, therefore, the net result is that of degenerative feedback.

The SINE ZERO Adjustment, R161, varies the DC level at pin 9 of A8, shifting the DC level of the output signal, to ensure that the output signal is symmetrical above and below 0 volts (Ground).

# Square Wave Amplifier:

The Square Wave Amplifier accepts the ±6 volt square wave generated by the Schmitt Trigger. Referring to Schematic #7 the square wave is applied to the bases of Q8 and Q9. Assume a negative going signal

at the base of Q8. Q8 is an emitter follower therefore the base of Q11 will be pulled in a negative direction, and Q11 will saturate.

Q10 is a series regulator, the voltage output of which is determined by the setting of the POSITIVE AMPLITUDE Adjustment, R43. Thus, when Q11 saturates, its collector will rise to the maximum positive voltage available at the emitter. Q11 in turn drives an emitter follower, Q14, which provides the low output impedance and the current to drive the Output Amplifier.

Similarly, when the input square wave goes positive, Q12 saturates at the maximum negative voltage, as determined by the setting of the NEGATIVE AMPLITUDE Adjustment, R46.

#### Ramp Generator:

The square wave signal at the emitters of Q8 and Q9 of the Square Wave Amplifier is also used as a gating signal for the Ramp Generator.

During the time the square wave signal is positive, the bases of Q17 and Q18 are held at approximately +0.7 volts by CR18 and CR19, respectively.

The triangle wave from the Integrator is applied to R58 and R59 and to the emitter of Q17. Because of the bias established by CR18, Q17 will remain cut off, as long as the signal at the emitter is more negative than 0 volts. R58, the RAMP OFFSET Adjustment, varies the voltage at the emitter of Q17 to 0 volts DC, so that the triangle input will be entirely negative.

Keeping in mind the phase relationship of the triangle and square wave (Figure 4-4) the triangle wave changes from its positive peak to its negative peak during the time the square wave is positive. Thus, the signal

at the emitter of Q17 is a negative going ramp, the emitter returning to 0 volts DC instantaneously as the square wave gate signal goes negative. The negative level of the square wave is -6 volts and the triangle wave amplitude is on the order of 2 volts peak-to-peak, so the triangle voltage can never overcome the forward bias of Q17 as established by the negative half of the square wave. Therefore, during the transition of the triangle from its negative peak to its positive peak, the emitter of Q17 is effectively clamped to Ground.

Q18 serves essentially the same purpose as Q17, but provides more positive clamping of the ramp signal. Also, Q18 is not driven as hard as Q17, therefore, any transient pulses from the edges of the square wave are isolated from the Ramp Amplifier.

The Ramp Amplifier is identical in operation to the Sine Amplifier. As in the Sine Amplifier, IC3 is connected in a differential pair configuration with the incoming ramp signal applied to pin 6, and a portion of the output signal applied to the differential side, pin 3. The RAMP ZERO Adjustment, R75, determined the DC level of the output signal by varying the DC level at the differential input, pin 3. A portion of the output signal is taken back to pin 3, through the RAMP AMPLITUDE Adjustment, R80. The output signal from the Ramp Amplifier is a negative going ramp.

#### SYNC GENERATOR

The square wave signal at the emitters of Q8 and Q9 is used as the source signal for the Sync Generator.

The positive going edge of the square wave is differentiated through R52 and C32 and this pulse is applied to the base fo Q16. Q16 provides a -10 volt pulse with a maximum duration of  $5\mu$ seconds, coincident with the leading edge of the square wave output.



#### OUTPUT AMPLIFIER

The Output Amplifier is also very nearly identical to the Sine Amplifier. The difference being that the Output Amplifier is an inverting amplifier, with part of the output signal taken back to the input, rather than to the differential side of an input pair. The OUTPUT ZERO Adjustment, R104, varies the DC level of the low side of the signal received from the Integrator and the Shaping Amplifiers. The low side of these signals is fed into the differential side of the input stage, IC4, in turn enabling the output signal to be varied around 0 volts DC, in order to achieve amplitude symmetry.

#### POWER SUPPLIES

All power supplies are located on the Master Board Assembly.

The +12 volt and -12 volt supplies are regulated supplies, the -12 volt supply slaved to the +12 volt supply. The supplies are identical in operation, therefore only the +12 volt supply will be discussed.

Regulation of the +12 volt supply is accomplished by the passing transistor, Q4. The output voltage is divided down through R19, R20 and R21 to provide a variable control voltage at the inverting (-) input of a differential amplifier, IC1.

The output voltage is also the source for Q24, which is connected as a zener diode. Q24 breaks down at +6.7 volts, and keeps a constant voltage at the non-inverting (+) input of IC1.

A drop in output voltage causes a less positive voltsge at the inverting (-) input of IC1, which results in a more positive voltage at the output, pin 6. This voltage is applied to the gate of FET, Q5, causing it to conduct more, which pulls the base of Q4 more negative. This results in increased conduction through Q4, which in turn raises the output voltage.

The 24 volt regulated supply is a simple series regulator. The collector of Q1 is supplied from the unregulated +32 volt supply. The base of Q1 is held at a constant voltage by CR12, which holds the conduction of Q1 constant, thereby keeping the emitter voltage constant. The current requirement of the +24 volt supply is very slight, as it is used only for bias voltage for current generators in other parts of the unit.

The +24 volt and -24 volt unregulated supplies, and the +32 volt and -32 volt supplies are derived from respective bridge rectifiers with a single section capacitive filter in each case. These supplies are used only to supply the necessary power for the Output Amplifier, and need not be regulated because of the relatively large amount of feedback used in the Output Amplifier.

### SECTION V

# MAINTENANCE

### General:

This section contains information relative to preventive and corrective maintenance. The portion dealing with corrective maintenance contains troubleshooting and corrective procedures.

Parts identification is provided on photographs of each circuit board or sub-assembly. Each photograph is on the page facing the schematic of the assembly in question.

A complete parts list for each assembly is contained on the page(s) immediately preceding each photograph.

The majority of electronic parts used in this instrument are standard, commercial parts, and replacement parts may be obtained locally. Precision components and mechanical parts, however, should be obtained through Data Royal Corporation's representative in your area.

#### Preventive Maintenance:

In general, no preventive maintenance, as such, is required. Occasional cleaning is recommended, and can be accomplished in conjunction with routine calibration.

A calibration cycle of six months is recommended for areas of normal operating conditions.

Re-calibration is necessary because the calibration of any instrument changes with age, use and operating conditions. Also, problems which may not be apparent during

normal use will show up during a calibration check. See Section III for complete calibration tion procedure.

### Corrective Maintenance:

Figure 5-1 is the logical representation of the procedure designed to assist in the location of any problem. This procedure is based on a systematic analysis of the instrument circuits in order to localize the problem.

This procedure should be undertaken only after it has been established that the problem can not be corrected by following the Adjustment and Calibration Procedures, as detailed in Section III. It should also be determined that the problem is not caused by conditions outside the Model F210A.

Table 5-1 contains a list of the normal indications for each of the checks listed in Figure 5-1. The steps outlined in Figure 5-1 are intended only to help localize the problem to an area within the instrument. Therefore, additional measurements will be required to completely isolate the problem within a specific circuit.

Table 5-2 contains a list of typical voltages as measured at a number of active components throughout the instrument.

Component parameters will vary from one instrument to the next, therefore, the voltage levels listed may not exactly equal readings obtained during the troubleshooting procedure.

#### NORMAL INDICATIONS

- 1. All outputs, corresponding to the Function Switch selected.
- 2. All outputs, as marked at each BNC connector.
- 3. -10 volt pulse, 2  $\mu$ seconds wide.
- 4. Varying the Frequency Control should vary the output over a 20:1 frequency span within any given range.
- 5. Applying 1.000 volts should raise the output frequency by 20% of full scale on any range.
- 6. Each consecutive position should change the output frequency by a factor of 10, the Range Multiplier in either X1 or X3.
- 7. Fixed steps of -20dB and -40dB attenuation of the output signal.
- 8. Vernier amplitude control of the output signal.
- 9. Normal signal at the Triangle T.P. is a ±1 volts triangle waveform (2v peak-to-peak), which is the output of the integrating amplifier. As de-

scribed in Section IV, the Integrator, the Schmitt Trigger and the Constant Current Generator constitute a "closed loop". All three circuits, therefore, must work in order to get a triangle output.

ground the Summing Junction (left end of the .0022 capacitor, C34). Now vary the Integrator Zero pot (R79) from CCW to CW. The DC level at the Triangle T. P. should vary from approximately -5 volts to +5 volts.

10. To troubleshoot the Schmitt Trigger ground the Integrator Summing Junction as in 9 above. Vary the Integrator Zero pot as in 9, while monitoring the Schmitt output. (Green T.P. in right corner at the front of the Generator Board. The Schmitt output should swing from -0.6 volts to +0.6 volts.

The Current Generator either works or it doesn't. If it works, the Green T.P. near Q11 will measure approximately +5 volts. The actual voltage is not extremely critical, but whatever it is, it must be stable.

TABLE 5-1

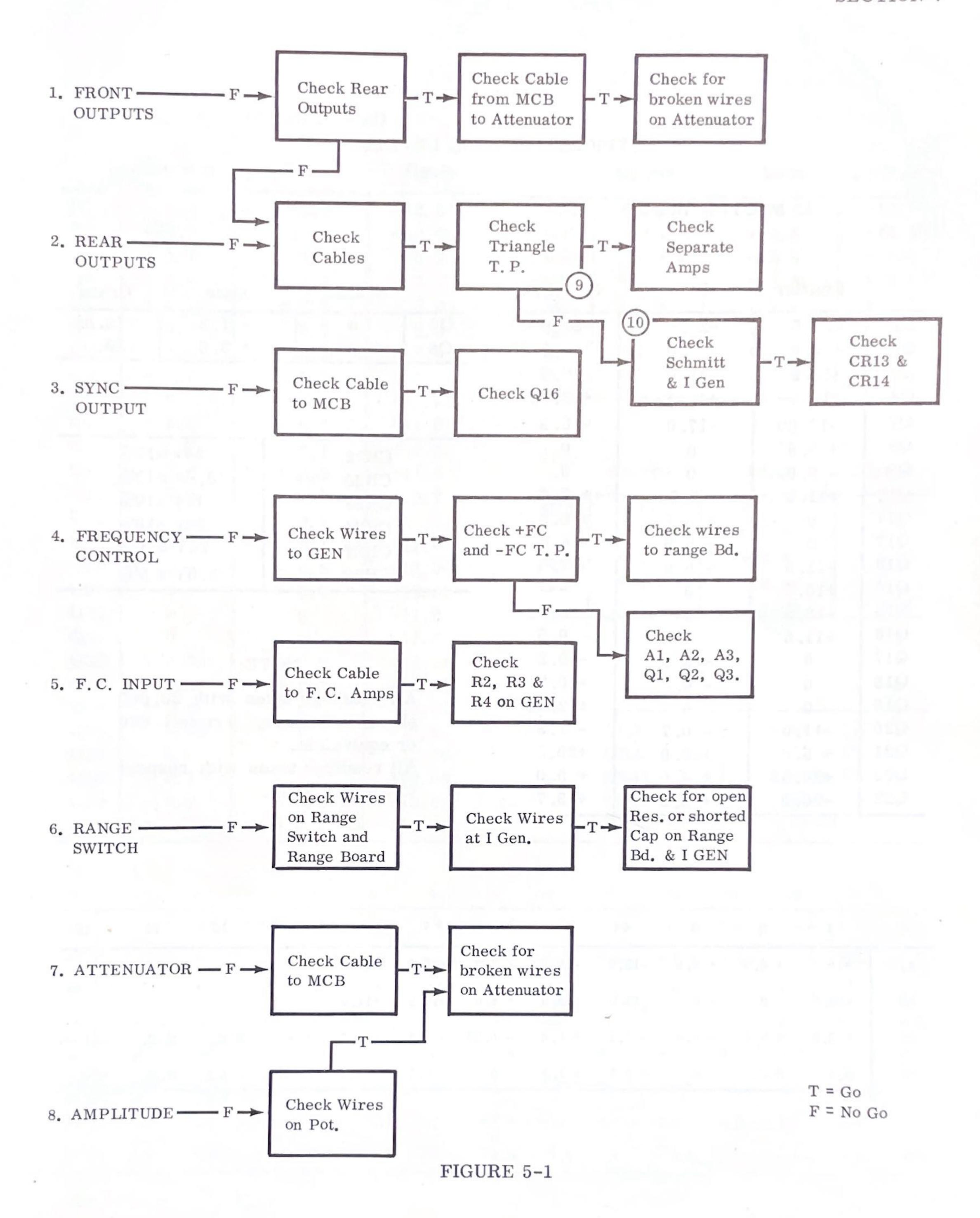


TABLE 5-2 TYPICAL VOLTAGE LEVELS

## 1. MASTER BOARD

-26.0

	Emitter	Base	Collector		Source	Gate	Drain
01	100 -	101 0	+32.0	Q5	0	- 1.2	+12.5
Q1	+23.5	+24.0	200 100	Q6	0	+ 3.8	-13.0
Q2	+17.5	+17.0	+16.5	- 40			
Q3	-17.5	-17.0	-16.5				
Q4	+17.5	+16.5	+12.00				
Q7	-12.00	-17.0	-16.5				~
Q8	+ 8.5	0	0		CR12	I .	±10%
Q9	- 9.0	0	0		CR20	Parallel Manager	±10%
Q10	+11.5	+ 6.7	+ 7.2		CR23		±10%
Q11	0	+ 6.7	+ 6.3		CR24		±10%
Q12	0	- 6.9	- 6.5		CR27	20V	±10%
Q13	-11.5	- 6.9	- 7.4		CR28	3.6V	± 5%
Q14	+10.5	0					
Q15	-10.5	0					
Q16	+11.5	0	- 0.5				
Q17	0	- 0.2	- 0.2		1	OTE:	
Q18	0	- 0.3	- 0.2		All readings	taken with 2	0,000
Q19	0	0	+12.00		ohms/volt me	ter. Triplet	t 630
Q20	-11.0	- 0.7	- 1.3		or equivalent.		
Q21	+ 5.0	+30.0	+29.5		All readings		spect
Q22	+26.5	+ 4.0	+ 5.0		to TP2 (Groun		
Q23	-26.0	+ 4.2	+ 3.7		11 1 (01 04)	/•	

	1	2	3	4	5	6	7	8	9	10	11	12
A1	+10.0	+ 6.9	+ 6.8	-15.5	-15.0	- 1.2	+15.5	+11.5				
A2	+10.0	0	0	-15.5	-15.0	+ 4.0	+15.5	+11.5				
A3	+ 5.5	+ 6.4	- 0.4	- 1.1	+ 6.4	- 0.25	- 1.1	+ 6.7	N.C.	N.C.	N.C.	-12.00
A4	N.C.	N.C.	0	- 0.7	+ 7.3	0	- 0.7	+ 8.5	N.C.	- 4.3	N.C.	N.C.

# 2. GENERATOR BOARD

	Emit	ter	Ε	Base	Col	lector			Emi	itter	I	Base	Coll	lector
Q1	- 5.	0	_	5.9	-1	2.00	_	Q31	- 0	.2	-	0.8	-1	2.00
Q2	+19.	0	+	18.0	+1	0.0		Q32	+ 0	.2	+	0.8	+1	2.00
Q3	+ 1.	7	+	1.0	-1	0.8		Q33	- 0	. 2	-	0.8	-1	200
Q4	+ 4.	0	+	3.8	-	6.0		Q34	+ 0	.2	+	0.8	+1	2.00
Q5	+ 3.	3	+	2.8	-	6.0		Q35	+ 7	. 8	+	8.4	+1	1.6
Q6	- 6.	0	_	6.7	_	9.2		Q36	+ 7	. 5	+	6.8	+	0.7
Q7	+ 4.	0	+	3.3	_	5.6		Q37	0		+	0.7	+1	0.2
Q8	- 6.	0	-	5.6		0		Q38	- 0	. 2	-	0.7	-1	0.2
Q9	0			0	+1	1.6								
Q13	- 1.	0	_	0.1	+1	1.6								
Q14	- 1. (	)	_	0.1	+	8.5								
Q15	+ 7.	8	+	8.5	+1	1.6			Sour	ce	Ga	ate	Dr	ain
Q16	- 5.	5	_	4.7	-	0.7		Q10	+ 6	0 1	+ 4	1 8	+23	7
Q17	0		+	0.7	+1	1.6		OTA	+ 6		+ 5		+23	
Q18	0		_	0.7	-1	1.6		011	+ 5					. 25
Q19	0		-	0.6	-1	2.00		Q11			+ 8	U USA M	0	
Q20	0		+	0.7	+1	2.00		Q12	+ 1 + 1			2.00		. 05
Q21	0			0	+1	1.8			1 1	• T	712	2.00		. 00
Q22	0			0	-1	1.8								
Q23	+ 0.	25	-	0.35	-1	2.00								
Q24	- 0.	3	+	0.35	+1	2.00								
Q25	+ 0.	05	-	0.5	-1	2.00			ana		T	C 0** 1	E 07	
Q26	- 0.	05	+	0.5	+1	2.00			CR3			6. 8v ±		
Q27	- 0.	1	-	0.75		2.00			CR4			8.7v ±		
Q28	+ 0.	1	+	0.75		2.00			CR1			6.8v ±		
Q29	- 0.	2	-	0.8		2.00			CR1			6. 2v ±	CA WOOD AND THE	
Q30	+ 0.	2	+	0.8	+1	2.00	-		CR1	5		0.20	-1070	
					_	c	7	8	9	10	11	12	13	14
	1			_			- 0.7							
A1	- 1.4		- 0.7											
A2 -	+ 0.5	0					N.C.							
А3	+ 0.5	0	0		0		N.C.							
A4	0	0	- 0.3				+ 3.0							
A5	0	+ 0.3	0	- 6.0	N.C.	N.C.	+ 2.8	+11.6	N.C.	N.C.	N.C.	N.C.	N.C.	N.C.
A6	+11.7	+11.2	+ 5.6	+ 5.6	N.C.	0	N.C.	N.C.	+11.7	+18.5	+18.0	+12.0	+23.5	+15.7
A7	+ 7.4	1.0	+ 1.0	-12.0	-11.3	0	+12.0	+ 8.4	N.C.	N.C.	N.C.	N.C.	N.C.	N.C.
A8	- 1.5 -	0.75	- 0.75	- 1.5	+ 6.8	0	- 0.75	+11.8	0	- 4.8	+11.8	+ 8.4	N.C.	N.C.

PARTS LIST

DATA ROYAL A	ASSEMBLY: F210	A GENERATOR	BOARD ASSEMBLY	DATA	ROYAL PART NO	O. 29-02026
SCHEMATIC		DESCRIPTION		MANU	FACTURER	DATA ROYA
DESIGNATION	VALUE	TYPE	RATING	CODE	PART NO.	PART NO.
CADAGEMONA						
CAPACITORS						
C1	100pf	CER DISC	1000V	56289	DD101	21-57007-0
C2	$10\mu f$	ELECT	25V	56289	TE-1204	21-57202-0
C3	68pf	CER DISC	1000V	56289	DD680	21-57013-0
C4	68pf	CER DISC	1000V	56289	DD680	21-57013-0
C5	$.01\mu f$	CER DISC	50V	56289	TG-S10	21-57001-0
C6	$.05\mu f$	CER DISC	50V	56289	TG-S50	21-57003-0
C7	5pf	CER DISC	1000V	56289	DD-050	21-57009-0
C8	. 05µf	CER DISC	50V	56289	TG-S50	21-57003-0
C9	$01\mu f$	CER DISC	50V	56289	TG-S10	21-57001-0
C10	5pf	CER DISC	1000V	56289	DD-050	21-57009-0
C11	68pf	CER DISC	1000V	56289	DD-680	21-57013-0
C12	68pf	CER DISC	1000V	56289	DD-680	21-57013-0
C13	$01\mu f$	CER DISC	50V	56289	TG-S10	21-57001-0
C14	. 01µf	CER DISC	50V	56289	TG-S10	21-57001-0
C15	. 01µf	CER DISC	50V	56289	TG-S10	21-57001-0
C16	75pf	MICA	500V	04062	DM-15-100J	21-57613-0
C17	68pf	CER DISC	1000V	56289	DD-680	21-57013-0
C18	$.01\mu f$	CER DISC	50V	56289	TG-S10	21-57001-0
C19	$.01\mu f$	CER DISC	50V	56289	TG-S10	21-57001-0
C20	. 01µf	CER DISC	50V	56289	TG-S10	21-57001-0
C21	. 01µf	CER DISC	50V	56289	TG-S10	21-57001-0
C22	200μf	ELECT	15V	56289	TE-1164	21-57201-0
C23	. 01µf	CER DISC	50V	56289	TG-S10	21-57001-0
C24	$200\mu f$	ELECT	15V	56289	TE-1164	21-57201-0
C25	$.01\mu f$	CER DISC	50V	56289	TG-S10	21-57001-0
C26	. 01µf	CER DISC	50V	56289	TG-S10	21-57001-0
C27	. 01µf	CER DISC	50V	56289	TG-S10	21-57001-0
C28	68pf	CER DISC	1000V	56289	DD-680	21-57013-0
			1000V	56289	DD-680	21-57013-0
C29	68pf	CER DISC		56289	TG-S10	21-57001-0
C30	. 01µf	CER DISC	50V	30203	10 510	
C31	SELECTED	WAD CED		72982	538-002-89	21-63201-0
C32	2-8pf	VAR CER	500V	04062	DM-15-820F	21-57630-0
C33	82pf	MICA			WMF-1022	21-57412-0
C34	$.0022\mu f$	MYLAR	100V	14655	DD-050	21-57412-0
C35	5pf	CER DISC	1000V	56289	DD-030 DD-101	21-57003-0
C36	100pf	CER DISC	1000V	56289	WMF-1S22	21-57408-0
C37	$.022\mu f$	MYLAR	100V	14655	DM-15-470J	21-57627-0
C38	47pf	MICA	500V	04062	TG-D50	21-57021-0
C39	$.005\mu f$	CER DISC	50V	56289	TG-D50 TG-S50	21-57003-0
C40	$.05\mu f$	CER DISC	50V	56289	TG-S50	21-57003-0
C41	$.05\mu f$	CER DISC	50V	56289	TG-S10	21-57003-0
C42	$.01 \mu f$	CER DISC	50V	56289		21-57001-0
C43	$.01 \mu \mathrm{f}$	CER DISC	50V	56289	TG-S10	21-57001-0
C44	. $01\mu\mathrm{f}$	CER DISC	50V	56289	TG-S10	21-57001-0
C45	$.01\mu \mathrm{f}$	CER DISC	50V	56289	TG-S10	21-01001-0
C46	SELECTED					
C47	SELECTED					0.4
C48	$.01\mu f$	CER DISC	50V	56289	TG-S10	21-57001-0
C49	$.01\mu f$	CER DISC	50V	56289	TG-S10	21-57001-0
C50	560pf	CER DISC	1000V	56289	DD-561	21-57002-0
C51	10pf	CER DISC	1000V	56289	DD-100	21-57004-0
C52	$01\mu f$	CER DISC	50V	56289	TG-S10	21-57001-0

PARTS LIST

DAIN ROIME M	SEMBLY: FZI	OA GENERATOR	BOARD ASSEMBLY	DATA	ROYAL PART NO	. 29-02026
CCHEMATIC		DESCRIPTION		MANU	FACTURER	DATA ROYA
SCHEMATIC DESIGNATION	VALUE	TYPE	RATING	CODE	PART NO.	PART NO.
CAPACITORS (C	ontinued)					
050		ann prac	1.0.0.037	5,000	DD-050	21-57009-0
C53	5pf	CER DISC	1000V	56289	TG-S10	21-57001-0
C54	$01\mu f$	CER DISC	50V	56289	DM-15-501F	21-57611-
C55	500pf	MICA	300V	04062 04062	DM-15-102F	21-57612-
C56	1000pf	MICA	100V	04062	DM-15-501F	21-57611-
C57	500pf	MICA	300V	56289	TE-1211	21-57217-
C58	100μf	ELECT	25V 25V	56289	TE-1211	21-57217-0
C59	$100\mu f$	ELECT		56289	TG-S10	21-57001-0
C60	$01\mu f$	CER DISC	50V	56289	TG-S10	21-57001-0
C61	. $01\mu\mathrm{f}$	CER DISC	50V	30203		
n naramon						
RESISTOR						
R1	$182\Omega$	FILM	1/4W 1%	07115	NA-60-1820F	27-42797-0
R2	5ΚΩ	FILM	1W 1%	04387	RS-1A	27-48007-0
R3	$4.5 \mathrm{K}\Omega$	FILM	1W 1%	04387	RS-1A	27-48006-0
R4	$1 \mathrm{K} \Omega$	VAR	1/2W 10%	01121	SV1021	27-49500-0
R5	$20\mathrm{K}\Omega$	FILM	1/4W 1%	12126	M1/4-20K	27-42927-0
R6	100Ω	VAR	1/2W 10%	01121	SV1011	27-49510-0
R7	$200\Omega$	VAR	1/2W 10%	01121	SV2011	27-49511-0
R8	6.8KΩ	COMP	1/4W 5%	01121	CB6825	27-39284-0
R9	$100 \mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB1045	27-39294-0
R10	$22\mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB2235	27-39288-0
R11	$22\mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB2235	27-39288-0
R12	$100 \mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB1045	27-39294-0
R13	$10 \mathrm{K}\Omega$	COMP	1/4W 1%	12126	M1/4-10K	27-42912-0
R14	$220\Omega$	COMP	1/4W 5%	01121	CB2215	27-39265-0
R15	$220\Omega$	COMP	1/4W 5%	01121	CB2215	27-39265-0
R16	$20\mathrm{K}\Omega$	FILM	1/4W 1%	12126	M1/4-20K	27-42927-0
R17	$33\mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB3335	27-39311-0
R18	$10 \mathrm{K}\Omega$	VAR	1/2W 10%	01121	SV1031	27-49513-0
R19	$1 \mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB1025	27-39273-0
R20	$100\Omega$	COMP	1/4W 5%	01121	CB1015	27-39261-0
R21	$100\Omega$	COMP	1/4W 5%	01121	CB1015	27-39261-0
R22	4.99K $\Omega$	FILM	1/4W 1%	12126	M1/4-4.99K	27-42887-0 27-42884-0
R23	4.64 $K\Omega$	FILM	1/4W 1%	12126	M1/4-4.64K	27-42900-0
R24	7.15K $\Omega$	FILM	1/4W 1%	12126	M1/4-7.15K	27-42500-0
R25	$500\Omega$	VAR	1/2W 10%	01121	SV5011	27-49512-0
R26	$2\mathrm{K}\Omega$	FILM	1/4W 1%	12126	M1/4-2K	27-42600-0
R27	$500\Omega$	VAR	1/2W 10%	01121	SV5011 M1/4-4.75K	27-49512-0
R28	4.75K $\Omega$	FILM	1/4W 1%	12126	CB2215	27-39265-0
R29	$220\Omega$	COMP	1/4W 5%	01121 $01121$	CB2215	27-39265-0
R30	$220\Omega$	COMP	1/4W 5%	01121	CB2215 CB3315	27-39267-0
R31	$330\Omega$	COMP	1/4W 5%	01121	CB3313 CB1835	27-39201-0
R32	18ΚΩ	COMP	1/4W 5%	01121	CB1633	27-39283-0
R33	5. 6ΚΩ	COMP	1/4W 5%	01121	CB7515	27-39203-0
R34	$750\Omega$	COMP	1/4W 5%		M1/4-1K	27-42846-0
R35	1ΚΩ	FILM	1/4W 1%	12126		Control Control Control
R36	$1 \mathrm{K}\Omega$	FILM	1/4W 1%	12126	M1/4-1K M1/4-11 5K	27-42846-0
R37	11.5KΩ	FILM	1/4W 5%	12126	M1/4-11.5K	27-42914-0
R38	$1 \mathrm{K} \Omega$	VAR	1/2W 10%	01121	SV1021	27-49500-0
R39	$1 \mathrm{K} \Omega$	VAR	1/2W 10%	01121	SV1021	27-49500-0
R40	11.5K $\Omega$	FILM	1/4W 1%	12126	M1/4-11.5K	27-42914-0

PARTS LIST

DATA ROYAL AS	SSEMBLY: F210	OA GENERATOR	BOARD ASSEMBLY	DATA	ROYAL PART NO.	29-02026
SCHEMATIC		DESCRIPTION		MANU	FACTURER	DATA ROYA
DESIGNATION	VALUE	TYPE	RATING	CODE	PART NO.	PART NO.
RESISTORS (Con	tinued)					
R41	$10\Omega$	COMP	1/4W 5%	01121	CB1005	27-39250-0
R42	560Ω	COMP	1/4W 5%	01121	CB5615	27-39270-0
R43	$340\Omega$	FILM	1/4W 1%	12126	M1/4-340	27-42807-
R44	82ΚΩ	COMP	1/4W 5%	01121	CB8235	27-39293-
R45	$560\Omega$	COMP	1/4W 5%	01121	CB5615	27-39270-
R46	$340\Omega$	FILM	1/4W 1%	12126	M1/4-340	27-42807-
R47	82ΚΩ	COMP	1/4W 5%	01121	CB8235	27-39293-
R48	22ΚΩ	COMP	1/4W 5%	01121	CB2235	27-39288-
R49	3. 9ΚΩ	COMP	1/4W 5%	01121	CB3925	27-39281-
R50	1. 5ΚΩ	COMP	1/4W 5%	01121	CB1525	27-34275-0
R51	$976\Omega$	FILM	1/4W 1%	12126	M1/4-976	27-42845-
R52	1ΚΩ	COMP	1/4W 5%	01121	CB1025	27-39273-
R53	$1 \mathrm{K} \Omega$	COMP	1/4W 5%	01121	CB1025	27-39273-
R54	1. 2ΚΩ	COMP	1/4W 5%	01121	CB1225	27-39274-
R55	$470\Omega$	COMP	1/4W 5%	01121	CB4715	27-39269-
R56	82Ω	COMP	1/4W 5%	01121	CB8205	27-39260-
R57	$330\Omega$	COMP	1/4W 5%	01121	CB3315	27-39267-0
R58	100ΚΩ	FILM	1/4W 1%	12126	M1/4-100K	27-42958-
R59	71.5ΚΩ	FILM	1/4W 1%	12126	M1/4-71.5K	27-42956-
R60	22ΚΩ	COMP	1/4W 5%	01121	CB2235	27-39288-
R61	22ΚΩ	COMP	1/4W 5%	01121	CB2235	27-39288-
R62	3.3ΚΩ	COMP	1/4W 5%	01121	CB2233	27-39280-
R63	3. 9ΚΩ	COMP	1/4W 5%	01121	CB3925	27-39281-0
R64	$220\Omega$	COMP	1/4W 5%	01121	CB2215	27-39265-0
R65	$220\Omega$	COMP	1/4W 5%	01121	CB2215	27-39265-0
R66	2.2ΚΩ	COMP	1/4W 5%	01121	CB2225	27-39278-0
R67	22ΚΩ	COMP	1/4W 5%	01121	CB2225	27-39288-
R68	$220\Omega$	COMP	1/4W 5%	01121	CB2215	27-39265-
R69	12.5ΚΩ	FILM	1/4W 1%	12126	M1/4-12.5K	27-46502-
R70	4. 167ΚΩ	FILM	1/4W 1%	12126	M1/4-4.167K	27-46500-0
R71	125ΚΩ	FILM	1/4W 1%	12126	M1/4-125K	27-46507-0
R72	41.67K $\Omega$	FILM	1/4W 1%	12126	M1/4-41.67K	27-46505-
R73	$1.25 M\Omega$	FILM	1/4W 1%	12126	M1/4-1.25M	27-46511-
R74	416.7ΚΩ	FILM	1/4W 1%	12126	M1/4-416.7K	27-46509-
R75	$22\mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB2235	27-39288-
R76	$22\mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB2235	27-39288-
R77	$1 \mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB1025	27-39273-
R78	$100\Omega$	COMP	1/4W 5%	01121	CB1015	27-39261-
R79	$22\mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB2235	27-39288-
R80	$10 \mathrm{K}\Omega$	VAR	1/2W 10%	01121	SV1031	27-49513-
R81	$1 \mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB1025	27-39273-
R82	$100 \mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB1045	27-39294-
R83	1.5ΚΩ	COMP	1/4W 5%	01121	CB1525	27-39275-
R84	$10\Omega$	COMP	1/4W 5%	01121	CB1025	27-39250-
R85	$560\Omega$	COMP	1/4W 5%	01121	CB5615	27-39270-
R86	$10 \mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB1035	27-39270-
R87	10ΚΩ	COMP	1/4W 5%	01121	CB1035	27-39286-
R88	$10\Omega$	COMP	1/4W 5%	01121	CB1035	27-39250-
R89	15Ω	COMP	1/4W 5%	01121	CB1005	27-39250-
R90	3.3ΚΩ	COMP	1/4W 5%	01121	CB1303	27-39252-
R91	2.2ΚΩ	COMP	1/4W 5%	01121	CB3323	27-39280-
R92	$15\Omega$	COMP	1/4W 5%	01121	CB2225 CB1505	27-39278-
R93	560Ω	COMP	1/4W 5%	01121	CB1505	27-39252-

PARTS LIST

					O. 29-02026	
SCHEMATIC		DESCRIPTION		MANU	FACTURER	DATA ROYA
DESIGNATION	VALUE	TYPE	RATING	CODE	PART NO.	PART NO.
RESISTORS (Con	ntinued)					
R94	$200\Omega$	VAR	1/2W 10%	01121	SV2011	27-49511-0
R95	$10\Omega$	COMP	1/4W 5%	01121	CB1005	27-39250-0
R96	$470\Omega$	COMP	1/4W 5%	01121	CB4715	27-39269-
R97	$2 \mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB2025	27-39277-
R98	$10\Omega$	COMP	1/4W 5%	01121	CB1005	27-39250-
R99	$2\mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB2025	27-39277-
R100	$1.5\Omega$	COMP	1/2W 5%	01121	EB15G5	27-39508-
R101	$100\Omega$	COMP	1/4W 5%	01121	CB1015	27-39261-
R102	$12\Omega$	COMP	1/4W 5%	01121	CB1205	27-39251-0
R103	$12\Omega$	COMP	1/4W 5%	01121	CB1205	27-39251-0
R104	$100\Omega$	COMP	1/4W 5%	01121	CB1015	27-39261-0
R105	$560\Omega$	COMP	1/4W 5%	01121	CB5615	27-39270-0
R106	$49.9\Omega$	FILM	1/4W 1%	12126	M1/4-49.9	27-42764-0
R107	$100\Omega$	FILM	1/4W 1%	12126	M1/4-100	27-42784-0
R108	$49.9\Omega$	FILM	1/4W 1%	12126	M1/4-49.9	27-42764-6
R109	15.4K $\Omega$	FILM	1/4W 1%	12126	M1/4-15.4K	27-42922-0
R110	$1 \mathrm{K} \Omega$	VAR	1/2W 10%	01121	SV1025	27-49500-0
R111	13.3K $\Omega$	FILM	1/4W 1%	12126	M1/4-13.3K	27-42918-0
R112	13.3ΚΩ	FILM	1/4W 1%	12126	M1/4-13.3K	27-42918-0
R113	$1 \mathrm{K} \Omega$	VAR	1/2W 10%	01121	SV1021	27-49500-0
R114	15.4K $\Omega$	FILM	1/4W 1%	12126	M1/4-15.4K	27-42922-0
R115	5.6ΚΩ	COMP	1/4W 5%	01121	CB5625	27-39283-0
R116	$182\Omega$	FILM	1/4W 1%	12126	M1/4-182	27-42797-0
R117	$5.6 \mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB5625	27-39283-0
R118	$33.2\Omega$	FILM	1/4W 1%	12126	M1/4-33.2	27-42758-0
R119	$33.2\Omega$	FILM	1/4W 1%	12126	M1/4-33.2	27-42758-0
R120	$182\Omega$	FILM	1/4W 1%	12126	M1/4-182	27-42797-0
R121	$1.65 \mathrm{K}\Omega$	FILM	1/4W 1%	07115	VA60-1651F	27-42857-0
R122	$2\mathrm{K}\Omega$	FILM	1/4W 1%	12126	M1/4-2K	27-42860-0
R123	$2\mathrm{K}\Omega$	FILM	1/4W 1%	12126	M1/4-2K	27-42860-0
R124	$1.65 \mathrm{K}\Omega$	FILM	1/4W 1%	07115	NA60-1651F	27-42857-0
R125	$12 \mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB1235	27-39287-0
R126	$1 \mathrm{K}\Omega$	FILM	1/4W 1%	12126	M1/4-1K	27-42846-0
R127	$2.15 \mathrm{K}\Omega$	FILM	1/4W 1%	12126	M1/4-2.15K	27-42862-0
R128	$1 \mathrm{K}\Omega$	FILM	1/4W 1%	12626	M1/4-1K	27-42846-0
R129	$12 \mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB1235	27-39287-0
R130	$12 \mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB1235	27-39287-0
R131	$604\Omega$	FILM	1/4W 1%	12126	M1/4-604	27-42827-0
R132	$562\Omega$	FILM	1/4W 1%	12126	M1/4-562	27-42974-0
R133	$604\Omega$	FILM	1/4W 1%	12126	M1/4-604	27-42827-0
R134	$12\mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB1235	27-39287-0
R135	$12 \mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB1235	27-39287-0
R136	$200\Omega$	FILM	1/4W 1%	12126	M1/4-200	27-42798-0
R137	$150\Omega$	FILM	1/4W 1%	12126	M1/4-150	27-42793-0
R138	$200\Omega$	FILM	1/4W 1%	12126	M1/4-200	27-42798-0
R139	$12\mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB1235	27-39287-0
R140	$12\mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB1235	27-39287-0
R141	$100\Omega$	FILM	1/4W 1%	12126	M1/4-100	27-42784-
R142	$38.3\Omega$	FILM	1/4W 1%	12126	M1/4-38.3	27-42759-
R143	$100\Omega$	FILM	1/4W 1%	12126	M1/4-100	27-42784-
R144	$12 \mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB1235	27-39287-
R145	$6.8 \mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB6825	27-39284-
R146	$24.9\Omega$	FILM	1/4W 1%	12126	M1/4-24.9	27-42755-

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PARTS LIST

DATA ROYAL A	SSEMBLY: F2	10A GENERATOR	R BOARD ASSEMBLY	DATA	ROYAL PART NO.	29-02026	
SCHEMATIC		DESCRIPTION		MANU	FACTURER	DATA ROYA	
DESIGNATION	VALUE	TYPE	RATING	CODE	PART NO.	PART NO.	
RESISTORS (Con	itinued)						
						07 40750 0	
R147	$10\Omega$	FILM	1/4W 1%	12126	M1/4-10	27-42750-0	
R148	6.8K $\Omega$	COMP	1/4W 5%	01121	CB6825	27-39284-0	
R149	$6.8 \mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB6825	27-39284-0	
R150	$6.8 \mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB6825	27-39284-0	
R151	$6.49 \mathrm{K}\Omega$	FILM	1/4W 1%	12126	M1/4-6.49K	27-42896-0	
R152	$1 \mathrm{K}\Omega$	VAR	1/2W 10%	01121	SV1021	27-49500-0	
R153	4. $64 \mathrm{K}\Omega$	FILM	1/4W 1%	12126	M1/4-4.64K	27-42884-0	
R154	4.64 $K\Omega$	FILM	1/4W 1%	12126	M1/4-4.64K	27-42884-0	
R155	$1 \mathrm{K}\Omega$	VAR	1/2W 10%	01121	SV1021	27-49500-0	
R156	$6.49 \mathrm{K}\Omega$	FILM	1/4W 1%	12126	M1/4-6.49K	27-42896-0	
R157	$1 \mathrm{K}\Omega$	FILM	1/4W 1%	12126	M1/4-1K	27-42846-0	
R158	$5\mathrm{K}\Omega$	VAR	1/2W 10%	01121	SV5021	27-49506-0	
R159	$2.1 \mathrm{K}\Omega$	FILM	1/4W 1%	12126	M1/4-2.1K	27-42861-0	
R160	$10 \mathrm{K}\Omega$	FILM	1/4W 1%	12126	M1/4-10K	27-42912-	
R161	$10 \mathrm{K}\Omega$	VAR	1/2W 10%	01121	SV1031	27-49513-	
R162	$10 \mathrm{K}\Omega$	FILM	1/4W 1%	12126	M1/4-10K	27-42912-	
R163	$10\Omega$	COMP	1/4W 5%	01121	CB1005	27-39250-	
R164	$10\Omega$	COMP	1/4W 5%	01121	CB1005	27-39250-	
R165	1. $5K\Omega$	COMP	1/4W 5%	01121	CB1525	27-39275-	
R166	1.5K $\Omega$	COMP	1/4W 5%	01121	CB1525	27-39275-	
R167	$27\Omega$	COMP	1/4W 5%	01121	CB2705	27-39254-	
R168	$22\mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB2235	27-39288-	
R169	$22\Omega$	COMP	1/4W 5%	01121	CB2205	27-39253-	
R170	$22\Omega$	COMP	1/4W 5%	01121	CB2205	27-39253-	
R171	$2.2K\Omega$	COMP	1/4W 5%	01121	CB2225	27-39278-	
R172	$22K\Omega$	COMP	1/4W 5%	01121	CB2235	27-39288-	
R173	4.7K $\Omega$	COMP	1/4W 5%	01121	CB4725	27-39284-	
R174	$6.8 \mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB6825	27-39284-	
R175	$100 \mathrm{K}\Omega$	FILM	1/4W 1%	12126	M1/4-100K	27-42958-	
R176	$2.1 \mathrm{K}\Omega$	FILM	1/4W 1%	12126	M1/4-2.1K	27-42861-	
R177	$100\Omega$	COMP	1/4W 5%	01121	CB1015	27-39261-	
R178	$10\Omega$	COMP	1/4W 5%	01121	CB1005	27-39250-	
R179	$20\Omega$	COMP	1/4W 5%	01121	CB2005	27-39308-	
R180	$1 \mathrm{K} \Omega$	COMP	1/4W 5%	01121	CB1025	27-39273-	
R181	$220\Omega$	COMP	1/4W 5%	01121	CB2215	27-39265-	
R182	$22\Omega$	COMP	1/4W 5%	01121	CB2205	27-39253-	
R183	$22\Omega$	COMP	1/4W 5%	01121	CB2205	27-39253-	
R184	$220\Omega$	COMP	1/4W 5%	01121	CB2215	27-39265-	
R185	$220\Omega$	COMP	1/4W 5%	01121	CB2215	27-39265	
R186	31.6K $\Omega$	FILM	1/4W 1%	12126	M1/4-31.6K		
R187	31.6K $\Omega$	FILM	1/4W 1%	12126	M1/4-31.6K		
R188	15.8KΩ	FILM	1/4W 1%	12126	M1/4-15.8K	, comment comments	
R189	$2.1 \mathrm{K}\Omega$	FILM	1/4W 1%	12126	M1/4-2.1K	27-42861	
R190	$499\Omega$	FILM	1/4W 1%	12126	M1/4-2.1K $M1/4-499$	Secretary Control of the Control of	
R191	$49.9\Omega$	FILM	1/4W 1%	12126	M1/4-499 $M1/4-49.9$	27-42821	
	$49.9\Omega$	FILM	1/4W 1%	12126		27-42764	
R192	$100\Omega$	FILM	1/4W 1%	12126	M1/4-49.9	27-42764	
R193	$100\Omega$	FILM	1/4W 1%		M1/4-100	27-42784	
R194	1002	LILIMI	1/200 1/0	12126	M1/4-100	27-42784	

# PARTS LIST

		DESCRIPTION			ES A COMPANY TO EST		
SCHEMATIC		DESCRIPTION		MANU	FACTURER	DATA ROYA	
DESIGNATION	VALUE	TYPE	RATING	CODE	PART NO.	PART NO.	
SEMICONDUCTO	D						
BEMICONDUCTO	K						
CR1		DIODE		JEDEC	1N914	27-95001-	
CR2		DIODE		JEDEC	1N914	27-95001-	
CR3		ZENER		JEDEC	1N5235B	27-95258-	
CR4		ZENER		JEDEC	1N5238B	27-95260-	
CR5		DIODE		JEDEC	1N914	27-95001-	
CR6		DIODE		JEDEC	1N914	27-95001-	
CR7		TUNNEL DIC	ODE	JEDEC	1N3719	27-95003-	
CR8		TUNNEL DIC	ODE	JEDEC	1N3719	27-95003-	
CR9		DIODE		JEDEC	1N914	27-95001-	
CR10		DIODE		JEDEC	1N914	27-95001-	
CR11		ZENER		JEDEC	1N5235B	27-95258-	
CR12		MS7000		21845		27-95254-	
CR13		MS7000		21845		27-95254-	
CR14		DIODE		JEDEC	1N914	27-95001-	
CR15		ZENER		JEDEC	1N5242B	27-95258-	
CR16		DIODE		JEDEC	1N914	27-95001-	
CR17		DIODE		JEDEC	1N914	27-95001-	
CR18		DIODE		JEDEC	1N914	27-95001-	
CR19		DIODE		JEDEC	1N914	27-95001-	
CR20		DIODE		JEDEC	1N914	27-95001-	
CR21		DIODE		JEDEC	1N914	27-95001-	
CR22		DIODE		JEDEC	1N914	27-95001-	
CR23		DIODE		JEDEC	1N914	27-95001-	
CR24		DIODE		JEDEC	1N914	27-95001-	
CR25		DIODE		JEDEC	1N914	27-95001-	
CR26		DIODE		JEDEC	1N914	27-95001-	
CR27		DIODE		JEDEC	1N914	27-95001-	
CR28		DIODE		JEDEC	1N914	27-95001-	
CR29		DIODE		JEDEC	1N914	27-95001-	
CR30		DIODE		JEDEC	1N914	27-95001-0	
CR31		DIODE		JEDEC	1N914	27-95001-0	
CR32		DIODE		JEDEC	1N914	27-95001-0	
CR33		DIODE		JEDEC	1N914	27-95001-0	
CR34		DIODE		JEDEC	1N914	27-95001-	
CR35		DIODE		JEDEC	1N914	27-95001-0	
TRANSISTOR							
21				JEDEC	2N4121	29-04506-0	
Q2				JEDEC	2N4121	29-04506-	
23				JEDEC	2N4121	29-04506-	
24				JEDEC	2N3640	29-04504-	
25				JEDEC	2N3640	29-04504-	
26				JEDEC	2N3640	29-04504-	
27				JEDEC	2N4274	29-04508-	
8				JEDEC	2N4274	29-04508-	
9				JEDEC	2N3638	29-04503-	
10				JEDEC	2N3956	29-04514-	
11				JEDEC	2N4360	29-04513-	
12				JEDEC	2N3956	29-04514-	
13				JEDEC	2N5179	29-04512-	
14				JEDEC	2N5179	29-04512-	

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# PARTS LIST

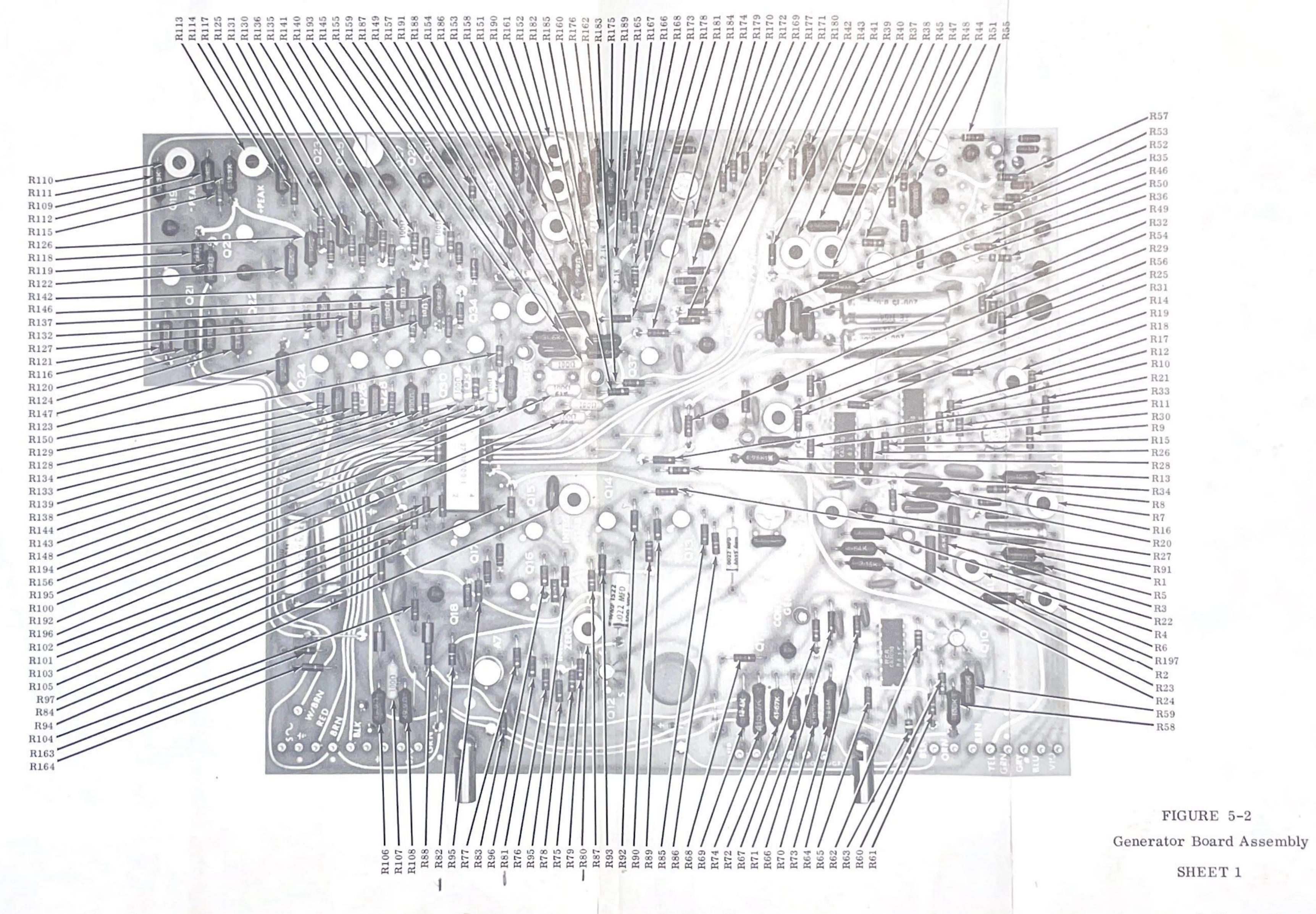
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COHENATIO		DESCRIPTION		MANUI	FACTURER	DATA ROYAL
SCHEMATIC DESIGNATION	VALUE	TYPE	RATING	CODE	PART NO.	PART NO.
TRANSISTORS (C	Continued)					
						00 04519-0
Q15				JEDEC	2N5179	29-04512-0
Q16				JEDEC	2N5179	29-04512-0
Q17				JEDEC	2N5179	29-04512-0
Q18				JEDEC	2N4121	29-04506-0
Q19				JEDEC	2N4121	29-04506-0
Q20				JEDEC	2N5179	29-04512-0
Q21				JEDEC	2N5179	29-04512-0
Q22				JEDEC	2N4121	29-05506-
Q23				JEDEC	2N4121	29-04506-
Q24				JEDEC	2N5179	29-04512-
Q25				JEDEC	2N4121	29-04506-
Q26				JEDEC	2N5179	29-04512-
Q27				JEDEC	2N4121	29-04506-
Q28				JEDEC	2N5179	29-04512-
Q29				JEDEC	2N4121	29-04506-
Q30				JEDEC	2N5179	29-04512-
Q31				JEDEC	2N4121	29-04506-
Q32				JEDEC	2N5179	29-04512-
Q33				JEDEC	2N4121	29-04506-
Q34				JEDEC	2N5179	29-04512-
Q35				JEDEC	2N5179	29-04512-
Q36				JEDEC	2N4121	29-04506-
				JEDEC	2N5179	29-04512-
Q37 Q38				JEDEC	2N4121	29-04506-
DIESCO AEST C	ID CITIE					
INTEGRATED C	IRCUIT					
A1		CA-3018		49671		25-08705-
A2 - 3		CA-3030		49671		25-08706-
A4 - 5		$\mu$ A-710		17227		25-08701-
A6		CA-3030		49671		25-08705-
A7		$\mu A - 709$		17227		25-08700-
A8		CA-3018		49671		25-08705

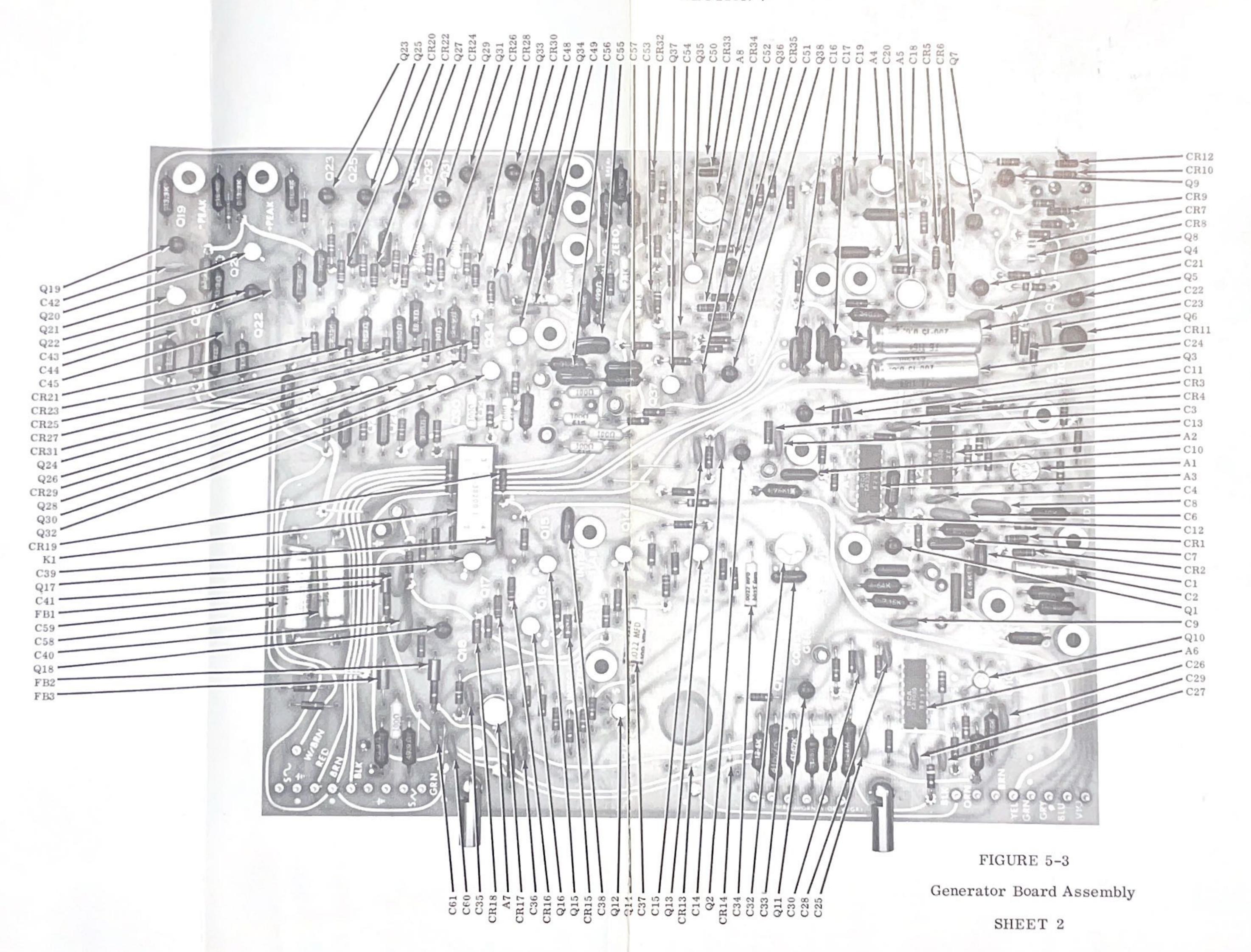
# PARTS LIST

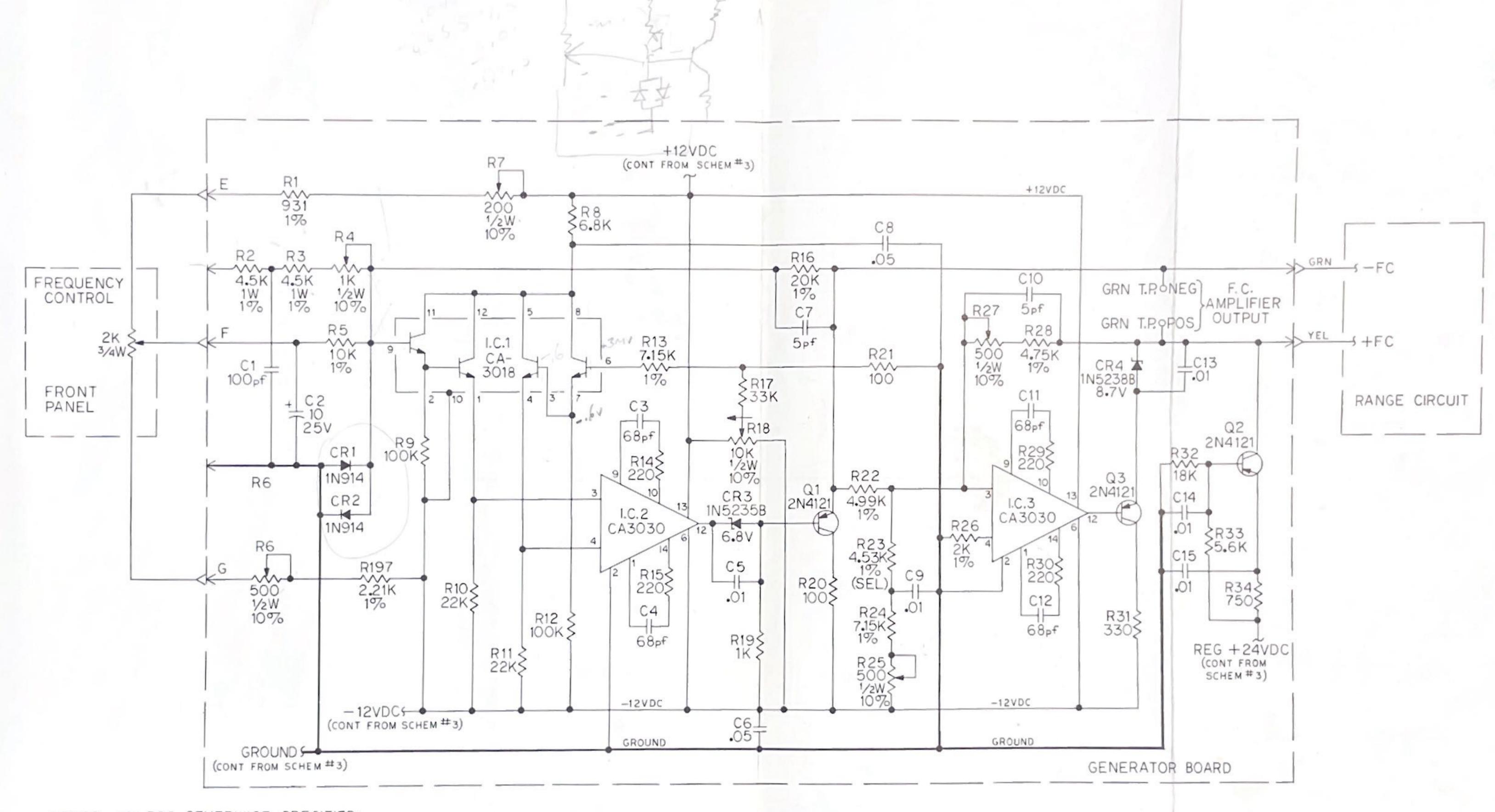
DATA ROYAL AS	SSEMBLY: F21	0A GENERATOR	BOARD ASSEMBLY	DATA	ROYAL PART N	O. 29-02026
SCHEMATIC		DESCRIPTION		MANU	FACTURER	DATA ROYAI
DESIGNATION	VALUE	TYPE	RATING	CODE	PART NO.	PART NO.
TRANSISTORS (C	continued)					46
Q15				JEDEC	2N5179	29-04512-0
Q16				JEDEC	2N5179	29-04512-0
Q17				<b>JEDEC</b>	2N5179	29-04512-0
Q18				JEDEC	2N4121	29-04506-0
Q19				JEDEC	2N4121	29-04506-0
Q20				JEDEC	2N5179	29-04512-0
Q21				JEDEC	2N5179	29-04512-0
Q22				JEDEC	2N4121	29-05506-0
Q23				JEDEC	2N4121	29-04506-0
Q24				JEDEC	2N5179	29-04512-0
Q25				JEDEC	2N4121	29-04506-0
Q26				JEDEC	2N5179	29-04512-0
Q27				JEDEC	2N4121	29-04506-0
Q28				JEDEC	2N5179	29-04512-0
Q29 *				JEDEC	2N4121	29-04506-0
Q30				JEDEC	2N5179	29-04512-0
Q31				JEDEC	2N4121	29-04506-0
Q32				JEDEC	2N5179	29-04512-0
Q33				JEDEC	2N4121	29-04506-0
Q34				JEDEC	2N5179	29-04512-0
Q35				JEDEC	2N5179	29-04512-0
Q36				JEDEC	2N4121	29-04506-0
Q37				JEDEC	2N5179	29-04512-0
Q38				JEDEC	2N4121	29-04506-0
INTEGRATED CD	RCUIT					
		<b>0.1</b> 0.555		40071		25 00705 0
A1		CA-3018		49671		25-08705-0
A2 - 3		CA-3030		49671		25-08706-0
A4 - 5		$\mu$ A-710		17227		25-08701-0
A6		CA-3030		49671		25-08705-0
A7		$\mu A - 709$		17227		25-08700-0
A8		CA-3018		49671		25-08705-0





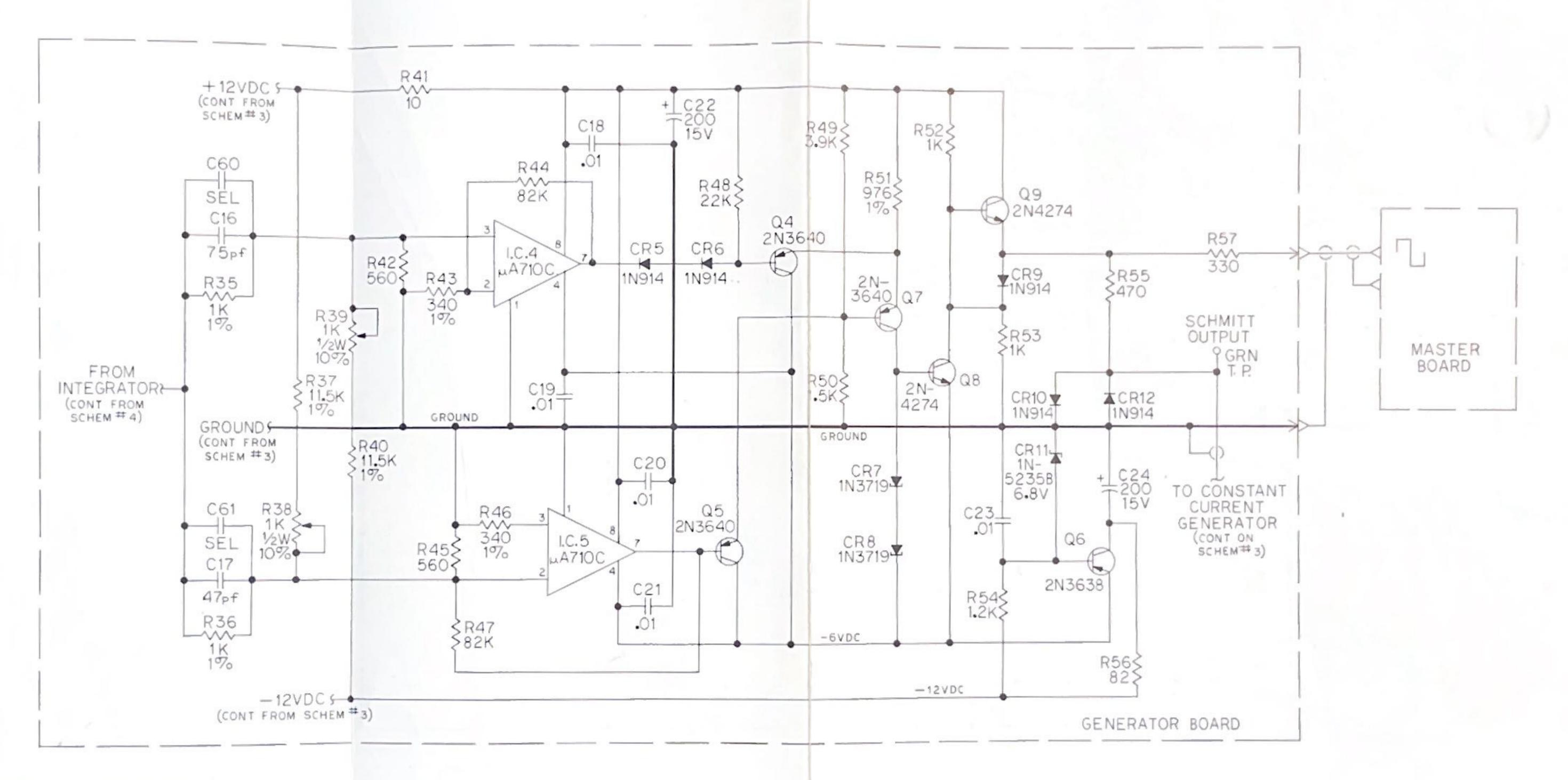






- 1. CAPACITANCE IN MICROFARADS, RESISTANCE IN OHMS.
- 2. RESISTORS ARE 1/4W, 5%.
- 3. VALUE OF SELECTED COMPONENTS IS NOMINAL.

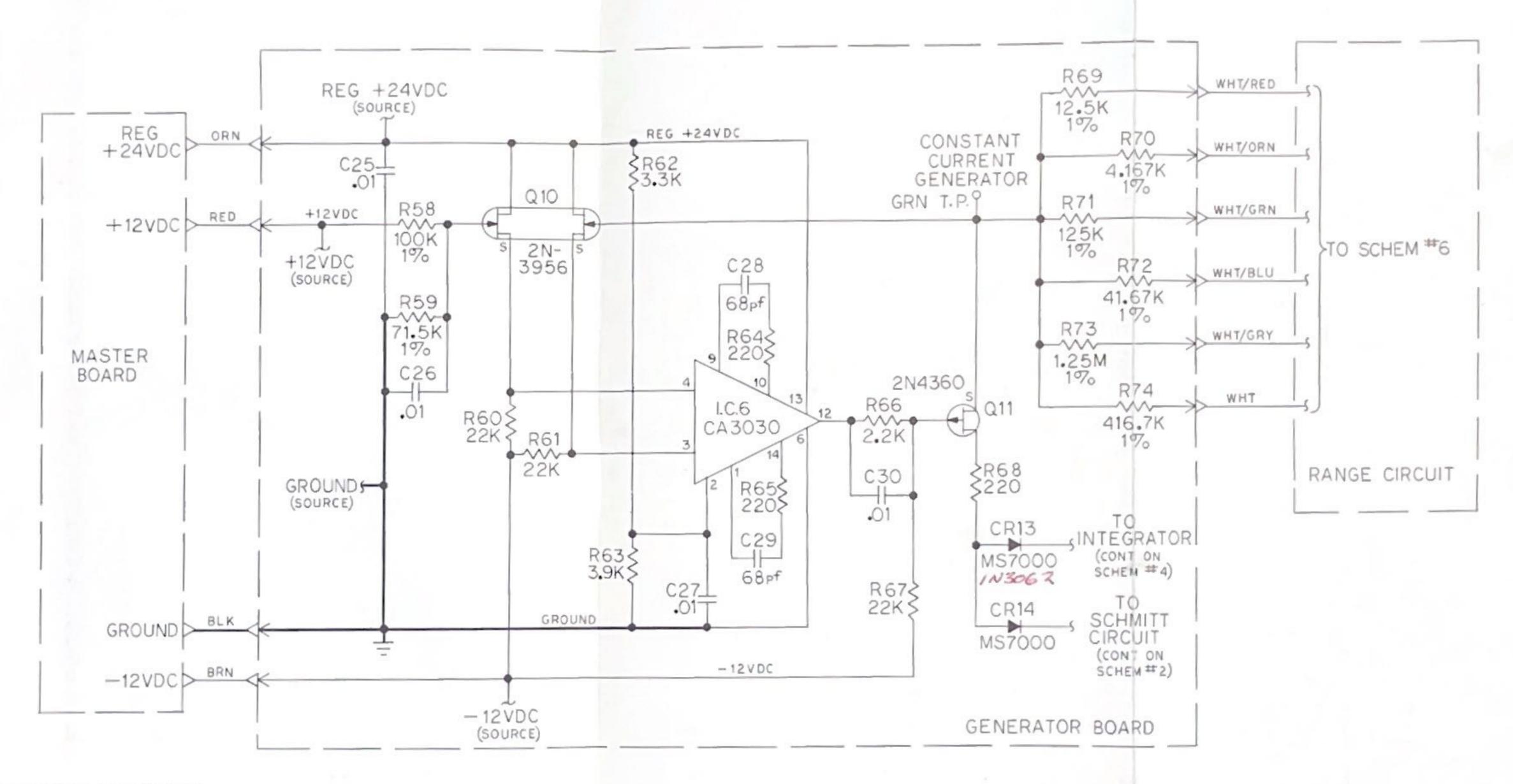
SCHEMATIC #1
Frequency Control Amplifiers



- 1. CAPACITANCE IN MICROFARADS, RESISTANCE IN OHMS.
- 2. RESISTORS ARE 1/4W, 5%.

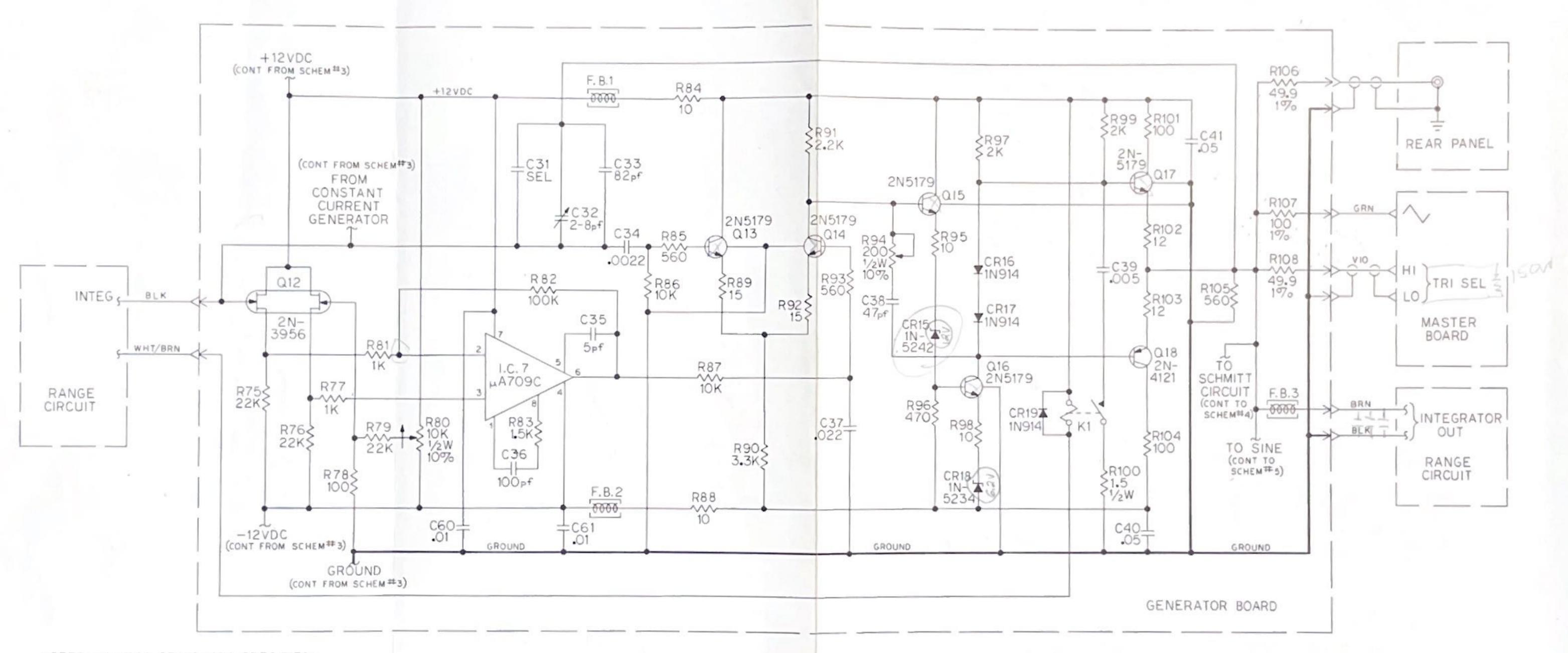
SCHEMATIC #2

Schmitt Trigger



- 1. CAPACITANCE IN MICROFARADS, RESISTANCE IN OHMS.
- 2. RESISTORS ARE 1/4W, 5%.

SCHEMATIC #3 Constant Current Generator

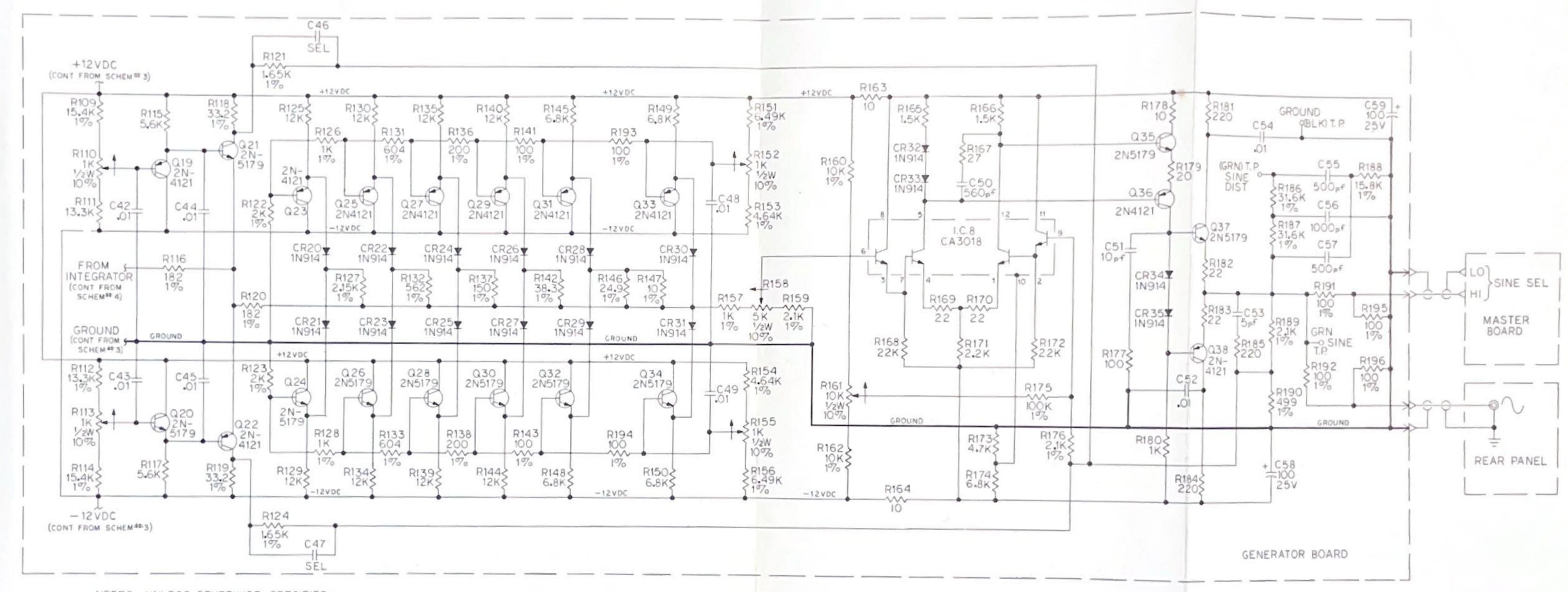


- 1. CAPACITANCE IN MICROFARADS, RESISTANCE IN OHMS.
- 2. RESISTORS ARE 1/4 W, 5%.

SCHEMATIC #4
Integrating Amplifier

10-1-68

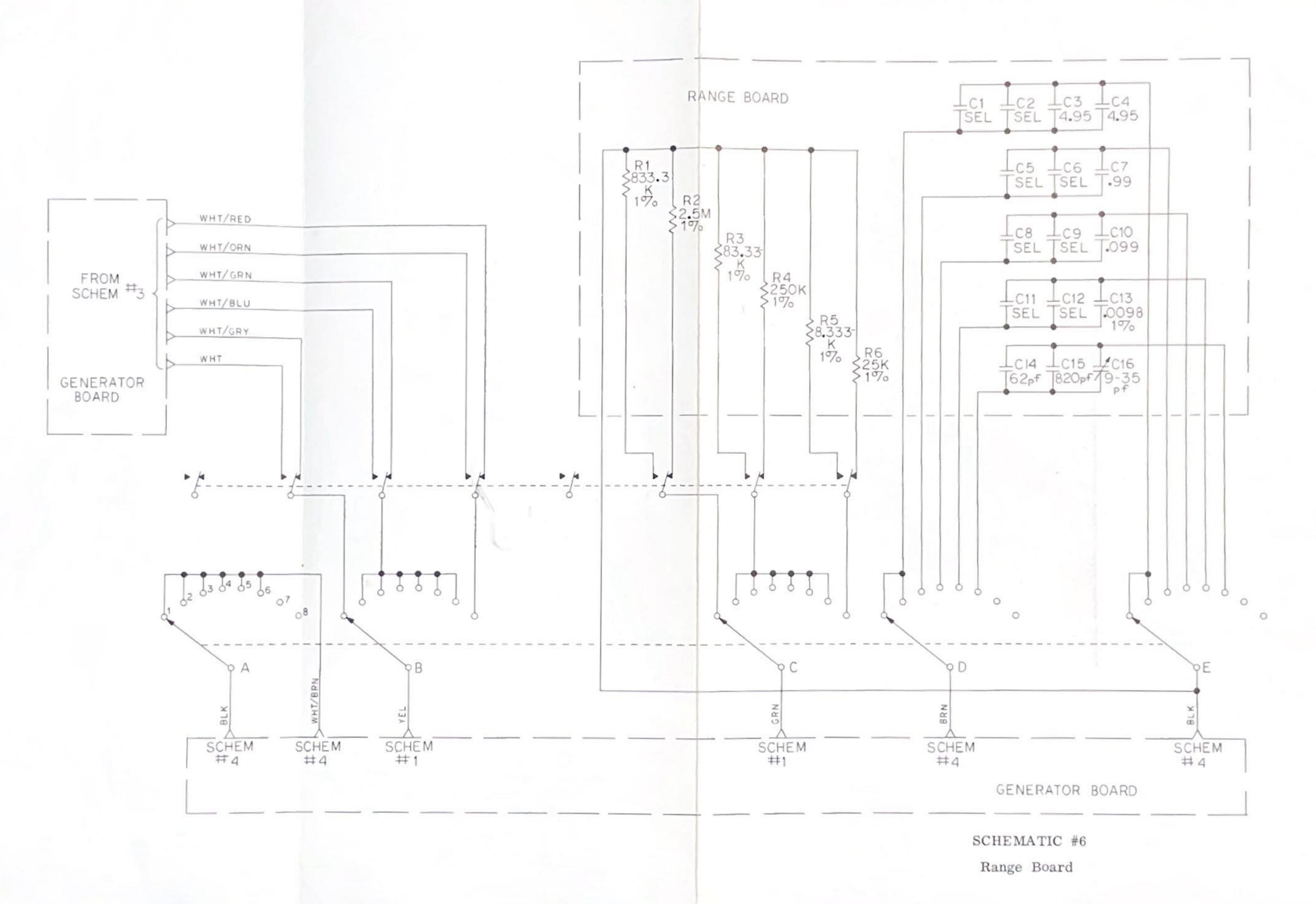
5-18



1. CAPACITANCE IN MICROFARADS, RESISTANCE IN OHMS.

2. RESISTORS ARE 1/4 W, 5%.

SCHEMATIC #5 Sine Generator



5-20

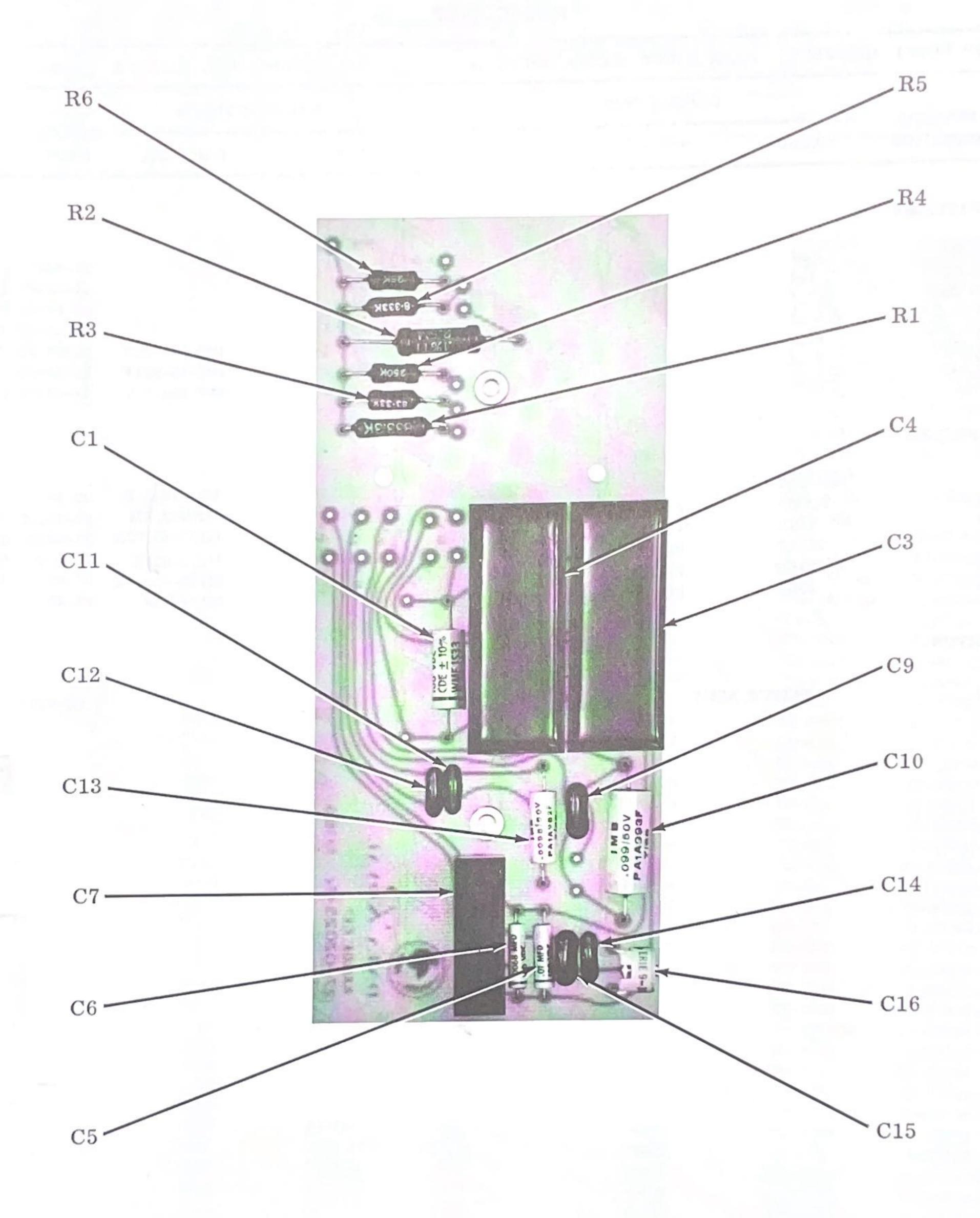


FIGURE 5-4
Range Board Assembly

# PARTS LIST

DATA ROYAL A	TA ROYAL ASSEMBLY: F210A RANGE BOARD ASSEMBLY				ROYAL PART NO	. 29-02025
SCHEMATIC		DESCRIPTION	1	MANU	DATEA DOTAT	
SCHEMATIC	VALUE	TYPE	RATING	CODE	PART NO.	PART NO.
CAPACITORS						
C1 - C4	$10\mu f$	KIT		29085		21-64000-1
C5 - C7	$1.0\mu f$	KIT		29085		21-64001-1
C8 - C10	$0.1\mu f$	KIT		29085		21-64002-1
C11 - 13	$0.01\mu f$	KIT		29085		21-64003-1
C14	62pf	MICA	500V	04062	DM-15-620F	21-57622-0
C15	82pf	MICA	300V	04062	DM-15-821F	21-75623-0
C16	9-35pf	VAR		72982	338-002-940	21-63204-0
RESISTORS						
rendro i orto						
R1	833.3ΚΩ	FILM	1/4W 1%	12126	M1/4-833.K	27-46510-0
R2	$2.5M\Omega$	FILM	1/4W 1%	12126	M1/4-2.5M	27-46512-0
R3	83.33ΚΩ	FILM	1/4W 1%	12126	M1/4-83.33K	27-46506-0
R4	$250 \mathrm{K}\Omega$	FILM	1/4W 1%	12126	M1/4-250K	27-46508-0
R5	$8.333$ K $\Omega$	FILM	1/4W 1%	12126	M1/4-8.333K	27-46501-0
R6	25ΚΩ	FILM	1/4W 1%	12126	M1/4-25K	27-46504-0
SWITCH						
S1	SWITCH A	ASS'Y		29085		28-64002-1

PARTS LIST

DATA ROYAL ASSEMBLY:		F210A MASTER BOARD ASSEMBLY		DATA ROYAL PART NO. 29-02001		
SCHEMATIC		DESCRIPTION		MANUFACTURER		
DESIGNATION	VALUE	TYPE	RATING	CODE	PART NO.	PART NO.
CAPACITOR						
C1	2700µf	ELECT	9537	F C D D D	FDT3 1104	01 55000 0
C2	2700µf	ELECT	25V	56289	TE-1164	21-57200-0
C3	.01µf		25V	56289	TE-1164	21-57200-0
C4		CER DISC	50V	56289	TG-S10	21-57001-0
C5	$01\mu f$	CER DISC	50V	56289	TG-S10	21-57001-0
C6	220pf	CER DISC	1000V	56289	DD-220	21-57014-0
C7	$01\mu f$	CER DISC	50V	56289	TG-S10	21-57001-0
C8	220pf	CER DISC	1000V	56289	DD-220	21-57014-0
C9	$.01\mu f$	CER DISC	50V	56289	TG-S10	21-57001-0
	$.05\mu f$	CER DISC	50V	56289	TG-S50	21-57003-0
C10	$100\mu f$	ELECT	25V	56289	TE-1211	21-57217-0
C11	$100\mu f$	ELECT	25V	56289	TE-1211	21-57217-0
C12	$1300 \mu f$	ELECT	50V	56289	36D132G	
					050AA6B	21-57213-0
C13	$1300 \mu f$	ELECT	50V	56289	36D132G	
					050AA6B	21-57213-0
C14	$.01\mu f$	CER DISC	50V	56289	TG-S10	21-57001-0
C15	$2500 \mu f$	ELECT	35V	00853	500-1954-01	21-57221-0
C16	2500µf	ELECT	35V	00853	500-1954-01	21-57221-0
C17	$.01\mu f$	CER DISC	50V	56289	TG-S10	
C18	$.01\mu f$	CER DISC	50V	56289		21-57001-0
C19	100µf	ELECT	25V		TG-S10	21-57001-0
C20	$.01\mu f$	CER DISC	50V	56289	TE-1211	21-57217-0
C21	$.01\mu f$	CER DISC	50V	56289	TG-S10	21-57001-0
C22	100μf	ELECT	25V	56289	TG-S10	21-57001-0
C23	47pf	CER DISC		56289	TE-1211	21-57217-0
C24	47pf	CER DISC	1000V	56289	DD-470	21-57016-0
C25	$.01\mu f$	CER DISC	1000V	56289	DD-470	21-57016-0
C26	$01\mu$ f	CER DISC	50V	56289	TG-S10	21-57001-0
C27	$100\mu f$		50V	56289	TG-S10	21-57001-0
C28	. 01µf	ELECT CER DISC	25V	56289	TE-1211	21-57217-0
C29	2000 and 200 to 100 and 100 an	CER DISC	50V	56289	TG-S10	21-57001-0
C30	$100\mu f$	ELECT	25V	56289	TE-1211	21-57217-0
C31	$01\mu f$	CER DISC	50V	56289	TG-S10	21-57001-0
	$01\mu f$	CER DISC	50V	56289	TG-S10	21-57001-0
C32	470pf	CER DISC	1000V	56289	DD-471	21-57006-0
C33	22pf	CER DISC	1000V	56289	DD-220	21-57012-0
C34	15pf	CER DISC	1000V	56289	DD-150	21-57017-0
C35	$100\mu f$	ELECT	25V	56289	TE-1211	21-57217-0
C36	$100\mu f$	ELECT	25V	56289	TE-1211	21-57217-0
237	2-8pf	VAR CER		72982	538-002-89	21-63201-0
238	$01\mu f$	CER DISC	50V	56289	TG-S10	21-57001-0
239	$01\mu f$	CER DISC	50V	56289	TG-S10	21-57001-0
240	5pf	CER DISC	1000V	56289	DD-050	21-57001-0
241	2pf	MICA	500V	04062	DM-15-020D	21-57600-0
242	$75\mu f$	ELECT	50V	56289	TE-1308	
243	100pf	CER DISC	1000V	56289	DD-101	21-57220-0
244	$75\mu f$	ELECT	50V	56289	TE-1308	21-57007-0
245	$75\mu f$	ELECT	50V	56289		21-57220-0
246	$75\mu s$	ELECT	50V	00200	TE-1308	21-57220-0

PARTS LIST

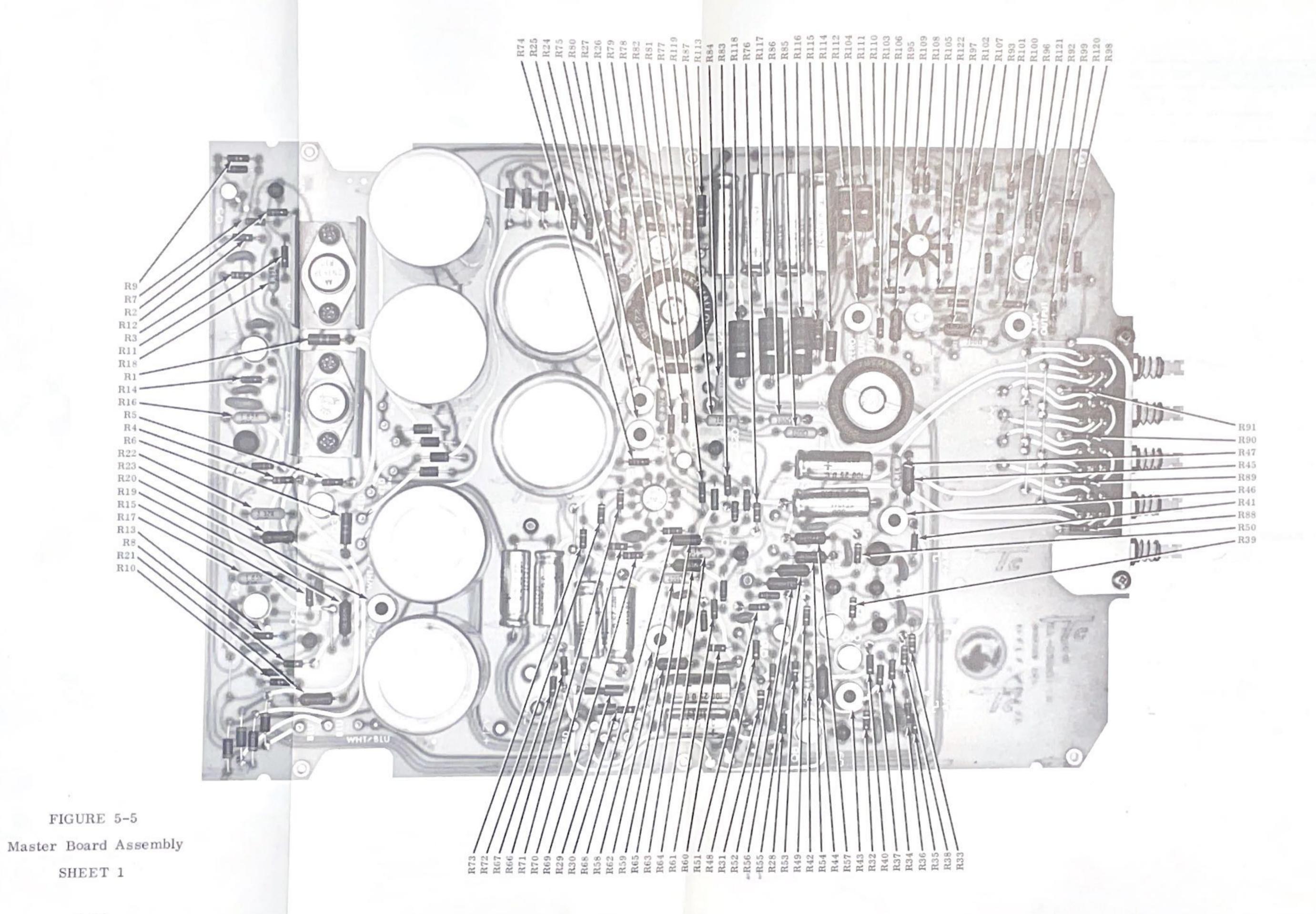
DATA ROYAL A	SSEMBLY: F21	OA MASTER BO	ARD ASSEMBLY	DATA	ROYAL PART NO	). 29-02001
COMPANIE	DESCRIPTION		MANUFACTURER		DATA ROYAI	
SCHEMATIC	VALUE	TYPE	RATING	CODE	PART NO.	PART NO.
RESISTORS (Con	ntinued)					
R54	$86.6\Omega$	FILM	1/4W 1%	12126	M1/4-86.6	27-42779-0
R55	$121\Omega$	FILM	1/4W 1%	12126	M1/4-121	27-32787-0
R56	$301\Omega$	FILM	1/4W 1%	12126	M1/4-301	27-42804-
R57	$60.4\Omega$	FILM	1/4W 1%	12126	M1/4-60.4	27-42771-0
R58	$200\Omega$	VAR	1/2W 10%	01121	SV2011	27-49511-
R59	$374\Omega$	FILM	1/4W 1%	12126	M1/4-374	27-42810-
R60	$390\Omega$	COMP	1/4W 5%	01121	CB3915	27-39268-
R61	1.5K $\Omega$	COMP	1/4W 5%	01121	CB1525	27-39275-
R62	$499\Omega$	FILM	1/4W 1%	12126	M1/4-499	27-42821-0
R63	12.1K $\Omega$	FILM	1/4W 1%	12126	M1/4-12.1K	27-42916-0
R64	$2.1 \text{K}\Omega$	FILM	1/4W 1%	12126	M1/4-2.1K	27-42861-
R65	$2.21 \mathrm{K}\Omega$	FILM	1/4W 1%	12126	M1/4-2.21K	27-42863-
R66	$10\Omega$	COMP	1/4W 5%	01121	CB1005	27-39250-0
R67	$10\Omega$	COMP	1/4W 5%	01121	CB1005	27-39250-0 27-39279-0
R68	$2.7 \mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB2725 CB2725	27-39279-0
R69	$2.7 \mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB2725 CB2715	27-39257-0
R70	$270\Omega$	COMP	1/4W 5%	01121	CB2715 CB4705	27-39257-0
R71	$47\Omega$	COMP	1/4W 5%	01121	CB4705	27-39257-0
R72	$47\Omega$	COMP	1/4W 5%	01121 01121	CB2725	27-39279-0
R73	2.7ΚΩ	COMP	1/4W 5% 1/4W 5%	01121	CB6835	27-39292-0
R74	68KΩ	COMP	1/4W 5% 1/2W 10%	01121	SV1031	27-49513-0
R75	10ΚΩ	VAR	1/4W 5%	01121	CB2725	27-39279-0
R76	2.7ΚΩ	COMP	1/4W 5%	01121	CB1015	27-39261-0
R77	$100\Omega$ $22\Omega$	COMP	1/4W 5%	01121	CB2205	27-39253-6
R78 R79	3. 32KΩ	FILM	1/4W 1%	12126	M1/4-3.32K	27-42872-0
R80	1ΚΩ	VAR	1/2W 10%	01121	SV1021	27-49500-0
R81	4. 12ΚΩ	FILM	1/4W 1%	12126	M1/4-4.12K	27-42880-
R82	22Ω	COMP	1/4W 5%	01121	CB2205	27-39253-6
R83	$100\Omega$	COMP	1/4W 5%	01121	CB1015	27-39261-0
R84	$100\Omega$	FILM	1/4W 1%	12126	M1/4-100	27-42784-0
R85	$100\Omega$	FILM	1/4W 1%	12126	M1/4-100	27-42784-
R86	$100\Omega$	FILM	1/4W 1%	12126	M1/4-100	27-42784-0
R87	$100\Omega$	FILM	1/4W 1%	12126	M1/4-100	27-42784-
R88	$150\Omega$	COMP	1/4W 5%	01121	CB1515	27-39263-
R89	$150\Omega$	COMP	1/4W 5%	01121	CB1515	27-39263-
R90	$150\Omega$	COMP	1/4W 5%	01121	CB1515	27-39263-
R91	$150\Omega$	COMP	1/4W 5%	01121	CB1515	27-39263-
R92	$100\Omega$	VAR	1/2W 10%	01121	SV1011	27-49510-
R93	$100\Omega$	FILM	1/4W 1%	12126	M1/4-100	27-42784-
R94	SELECTED	****	2 /4777 101	10100	M1 /4 9 01V	07 40000
R95	3. 01ΚΩ	FILM	1/4W 1%	12126	M1/4-3.01K	27-42869-
R96	1.5ΚΩ	COMP	1/4W 5%	01121	CB1525	27-39275-
R97	1.5ΚΩ	COMP	1/4W 5%	01121	CB1525	27-39275-
R98	1.5ΚΩ	COMP	1/4W 5%	01121	CB1525	27-39275-
R99	$15\Omega$	COMP	1/4W 5%	01121	CB1505	27-39252-
R100	$15\Omega$	COMP	1/4W 5%	01121	CB1505	27-39252-
R101	820Ω	COMP	1/4W 5%	01121	CB8215	27-39271-
R102	182Ω	FILM	1/4W 1% 1/4W 5%	12126	M1/4-182	27-42797-
R103	22ΚΩ	COMP	1/4W 5% 1/2W 10%	01121	CB2235	27-39288-
R104	10ΚΩ	VAR		01121	SV1031	27-49513-
R105	$10\Omega$	COMP	1/4W 5%	01121	CB1005	27-39250-

PARTS LIST

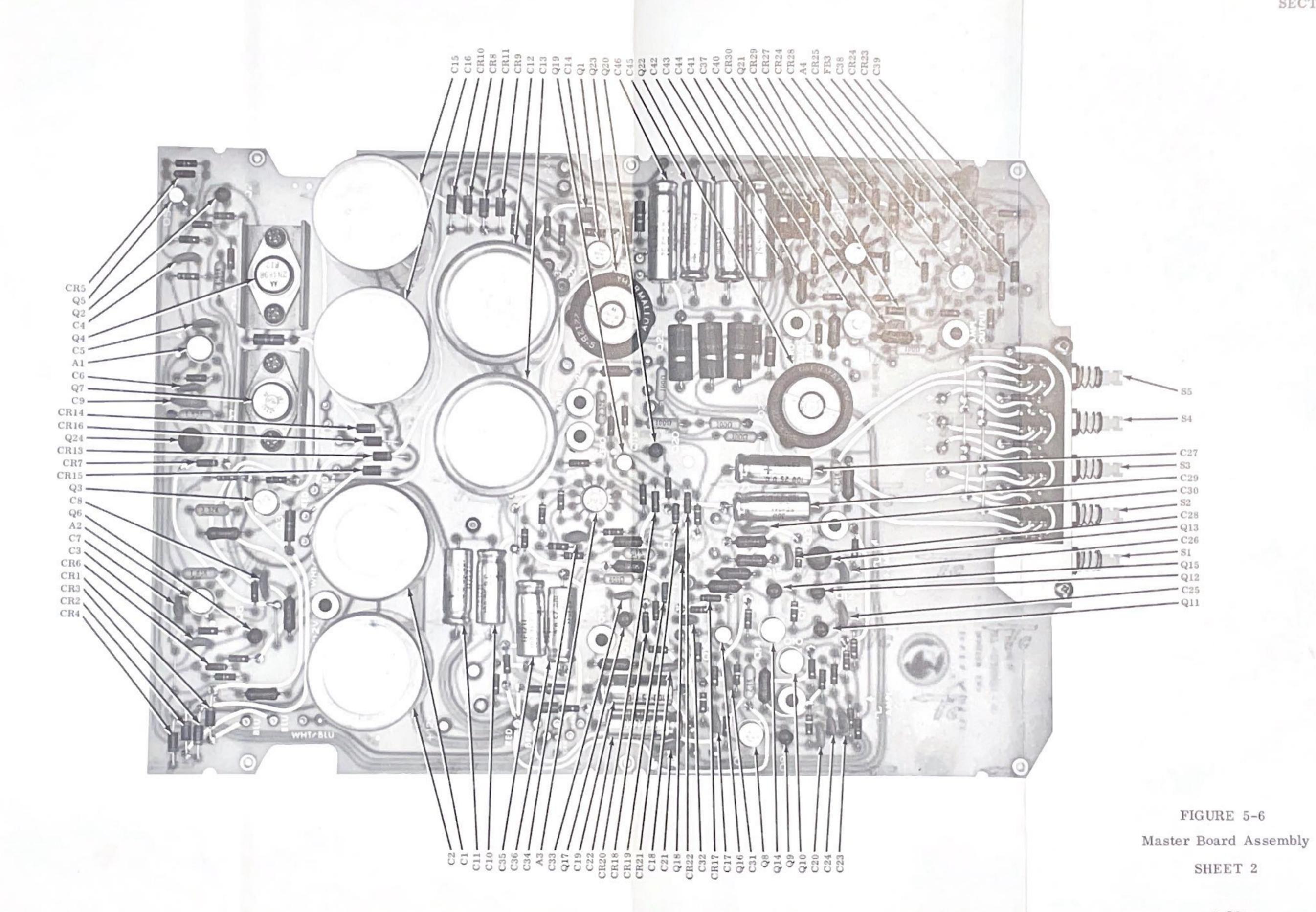
	SSEMBLY: F21	OA MASTER BO	ARD ASSEMBLY	DATA	ROYAL PART N	O. 29-02001
SCHEMATIC	DESCRIPTION		MANU	MANUFACTURER		
DESIGNATION	VALUE	TYPE	RATING	CODE	PART NO.	PART NO.
RESISTORS (Con	tinued)					
R106	180Ω	COMP	1/4W 5%	01121	CB1815	27-39264-0
R107	$1.5\Omega$	COMP	1/2W 5%	01121	EB15G5	27-39508-0
R108	$10\Omega$	COMP	1/4W 5%	01121	CB1005	27-39250-0
R109	$10\Omega$	COMP	1/4W 5%	01121	CB1005	27-39250-
R110	$150\Omega$	COMP	1/4W 5%	01121	CB1515	27-39263-
R111	$750\Omega$	COMP	1W 5%	01121	GB7515	27-40006-
R112	$750\Omega$	COMP	1W 5%	01121	GB7515	27-40006-
R113	$1.5\Omega$	COMP	1/2W 5%	01121	EB15G5	27-39508-
R114	$12\Omega$	COMP	1/2W 5%	01121	EB1205	27-39510-
R115	$12\Omega$	COMP	1/2W 5%	01121	EB1205	27-39510-
R116	$150\Omega$	COMP	2W 5%	01121	HB1515	27-40251-
R117	$150\Omega$	COMP	2W 5%	01121	HB1515	27-40251-
R118	$150\Omega$	COMP	2W 5%	01121	HB1515	27-40251-
R119	1.5 $\Omega$	COMP	1/2W 5%	01121	EB15G5	27-39508-
R120	$5.6 \mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB5625	27-39283-
R121	$10 \mathrm{K}\Omega$	COMP	1/4W 5%	01121	CB1035	27-39286-
R122	82Ω	COMP	1/4W 5%	01121	CB8205	27-39260-
SEMICONDUCTO	R					
CR1		DIODE		14099	SCE-2	27-95000-0
CR2		DIODE		14099	SCE-2	27-95000-0
CR3		DIODE		14099	SCE-2	27-95000-
CR4		DIODE		14099	SCE-2	27-95000-
CR5		DIODE		JEDEC	1N914	27-95001-
CR6		DIODE		JEDEC	1N914	27-95001-
CR7		DIODE		JEDEC	1N914	27-95001-
CR8		DIODE		14099	SCE-2	27-95000-
CR9		DIODE		14099	SCE-2	27-95000-
		DIODE		14099	SCE-2	
CR10						27-95000-
CR10 CR11		DIODE		14099	SCE-2	
CR11		DIODE		14099 JEDEC	SCE-2 1N5252	27-95000-
CR11 CR12		ZENER		JEDEC	1N5252	27-95000- 27-95261-
CR11 CR12 CR13		ZENER		JEDEC 14099	1N5252 SCE-2	27-95000- 27-95000- 27-95261- 27-95000- 27-95000-
CR11 CR12 CR13 CR14		ZENER DIODE DIODE		JEDEC 14099 14099	1N5252 SCE-2 SCE-2	27-95000- 27-95261- 27-95000- 27-95000-
CR11 CR12 CR13 CR14 CR15		ZENER DIODE DIODE DIODE		JEDEC 14099 14099	1N5252 SCE-2 SCE-2 SCE-2	27-95000- 27-95261- 27-95000- 27-95000- 27-95000-
CR11 CR12 CR13 CR14 CR15 CR16		ZENER DIODE DIODE DIODE DIODE		JEDEC 14099 14099 14099	1N5252 SCE-2 SCE-2 SCE-2	27-95000- 27-95261- 27-95000- 27-95000- 27-95000-
CR11 CR12 CR13 CR14 CR15 CR16 CR17		ZENER DIODE DIODE DIODE DIODE		JEDEC 14099 14099 14099 JEDEC	1N5252 SCE-2 SCE-2 SCE-2 1N914	27-95000- 27-95261- 27-95000- 27-95000- 27-95000- 27-95001-
CR11 CR12 CR13 CR14 CR15 CR16 CR17 CR18		DIODE DIODE DIODE DIODE DIODE DIODE		JEDEC 14099 14099 14099 JEDEC JEDEC	1N5252 SCE-2 SCE-2 SCE-2 1N914 1N914	27-95000- 27-95261- 27-95000- 27-95000- 27-95000- 27-95001- 27-95001-
CR11 CR12 CR13 CR14 CR15 CR16 CR17 CR18 CR19		ZENER DIODE DIODE DIODE DIODE DIODE DIODE DIODE		JEDEC 14099 14099 14099 JEDEC JEDEC JEDEC JEDEC	1N5252 SCE-2 SCE-2 SCE-2 1N914 1N914 1N914	27-95000- 27-95000- 27-95000- 27-95000- 27-95001- 27-95001- 27-95001-
CR11 CR12 CR13 CR14 CR15 CR16 CR17 CR18 CR19 CR20		ZENER DIODE DIODE DIODE DIODE DIODE DIODE ZENER		JEDEC 14099 14099 14099 JEDEC JEDEC JEDEC JEDEC JEDEC	1N5252 SCE-2 SCE-2 SCE-2 1N914 1N914 1N914 1N5232B	27-95000- 27-95000- 27-95000- 27-95000- 27-95001- 27-95001- 27-95255-
CR11 CR12 CR13 CR14 CR15 CR16 CR17 CR18 CR19 CR20 CR21		ZENER DIODE		JEDEC 14099 14099 14099 JEDEC JEDEC JEDEC JEDEC JEDEC JEDEC	1N5252 SCE-2 SCE-2 SCE-2 1N914 1N914 1N914 1N5232B 1N914	27-95000- 27-95000- 27-95000- 27-95000- 27-95001- 27-95001- 27-95001- 27-95001- 27-95001-
CR11 CR12 CR13 CR14 CR15 CR16 CR17 CR18 CR19 CR20 CR21 CR22		ZENER DIODE		JEDEC 14099 14099 14099 JEDEC	1N5252 SCE-2 SCE-2 SCE-2 SCE-2 1N914 1N914 1N914 1N5232B 1N914 1N914	27-95000- 27-95000- 27-95000- 27-95000- 27-95001- 27-95001- 27-95001- 27-95001- 27-95001- 27-95001-
CR11 CR12 CR13 CR14 CR15 CR16 CR17 CR18 CR19 CR20 CR21 CR22 CR23		ZENER DIODE DIODE DIODE DIODE DIODE DIODE ZENER DIODE DIODE ZENER DIODE ZENER		JEDEC 14099 14099 14099 JEDEC	1N5252 SCE-2 SCE-2 SCE-2 SCE-2 1N914 1N914 1N914 1N5232B 1N914 1N914 1N914	27-95000- 27-95000- 27-95000- 27-95000- 27-95001- 27-95001- 27-95255- 27-95001- 27-95001- 27-95001- 27-95001- 27-95001-
CR11 CR12 CR13 CR14 CR15 CR16 CR17 CR18 CR19 CR20 CR21 CR22 CR23 CR24		ZENER DIODE DIODE DIODE DIODE DIODE DIODE ZENER DIODE DIODE ZENER ZENER ZENER ZENER		JEDEC 14099 14099 14099 JEDEC	1N5252 SCE-2 SCE-2 SCE-2 1N914 1N914 1N9232B 1N914 1N914 1N914 1N914 1N9242 1N5252	27-95000- 27-95000- 27-95000- 27-95000- 27-95001- 27-95001- 27-95255- 27-95001- 27-95255- 27-95259- 27-95261-
CR11 CR12 CR13 CR14 CR15 CR16 CR17 CR18 CR19 CR20 CR21 CR22 CR23 CR24 CR25		ZENER DIODE DIODE DIODE DIODE DIODE DIODE ZENER DIODE ZENER ZENER ZENER ZENER ZENER DIODE		JEDEC 14099 14099 14099 JEDEC	1N5252 SCE-2 SCE-2 SCE-2 1N914 1N914 1N9232B 1N914 1N914 1N914 1N5242 1N5252 1N914	27-95000- 27-95000- 27-95000- 27-95000- 27-95001- 27-95001- 27-95255- 27-95001- 27-95259- 27-95261- 27-95201- 27-95261- 27-95001-
CR11 CR12 CR13 CR14 CR15 CR16 CR17 CR18 CR19 CR20 CR21 CR22 CR23 CR24 CR25 CR26		ZENER DIODE DIODE DIODE DIODE DIODE DIODE ZENER DIODE ZENER ZENER ZENER DIODE ZENER DIODE ZENER DIODE		JEDEC 14099 14099 14099 JEDEC	1N5252 SCE-2 SCE-2 SCE-2 1N914 1N914 1N9232B 1N914 1N914 1N5242 1N5242 1N5252 1N914 1N914	27-95000- 27-95000- 27-95000- 27-95000- 27-95001- 27-95001- 27-95001- 27-95001- 27-95255- 27-95259- 27-95261- 27-95001- 27-95001- 27-95001-
CR12 CR13 CR14 CR15 CR16 CR17 CR18 CR19 CR20 CR21 CR22 CR23 CR24 CR25 CR26 CR27		ZENER DIODE DIODE DIODE DIODE DIODE DIODE ZENER DIODE ZENER ZENER ZENER DIODE ZENER ZENER ZENER DIODE		JEDEC 14099 14099 14099 JEDEC	1N5252 SCE-2 SCE-2 SCE-2 1N914 1N914 1N914 1N5232B 1N914 1N5242 1N5242 1N5252 1N914 1N914 1N914 1N914 1N914 1N914 1N914	27-95000- 27-95000- 27-95000- 27-95000- 27-95001- 27-95001- 27-95255- 27-95001- 27-95261- 27-95261- 27-95261- 27-95001- 27-95261- 27-95264-
CR11 CR12 CR13 CR14 CR15 CR16 CR17 CR18 CR19 CR20 CR21 CR22 CR23 CR24 CR25 CR24 CR25 CR26 CR27 CR28		ZENER DIODE DIODE DIODE DIODE DIODE DIODE ZENER DIODE ZENER ZENER ZENER DIODE ZENER ZENER ZENER ZENER ZENER ZENER ZENER		JEDEC 14099 14099 14099 JEDEC	1N5252 SCE-2 SCE-2 SCE-2 1N914 1N914 1N914 1N5232B 1N914 1N914 1N5242 1N5252 1N914 1N914 1N914 1N914 1N914 1N914 1N914	27-95000- 27-95000- 27-95000- 27-95000- 27-95001- 27-95001- 27-95255- 27-95255- 27-95261- 27-95261- 27-95261- 27-95261- 27-95264- 27-95264- 27-95263-
CR11 CR12 CR13 CR14 CR15 CR16 CR17 CR18 CR19 CR20 CR21 CR22 CR23 CR24 CR25 CR26 CR27		ZENER DIODE DIODE DIODE DIODE DIODE DIODE ZENER DIODE ZENER ZENER ZENER DIODE ZENER ZENER ZENER DIODE		JEDEC 14099 14099 14099 JEDEC	1N5252 SCE-2 SCE-2 SCE-2 1N914 1N914 1N914 1N5232B 1N914 1N5242 1N5242 1N5252 1N914 1N914 1N914 1N914 1N914 1N914 1N914	27-95000- 27-95000- 27-95000- 27-95000- 27-95001- 27-95001- 27-95255- 27-95001- 27-95261- 27-95261- 27-95261- 27-95261- 27-95261- 27-95264-

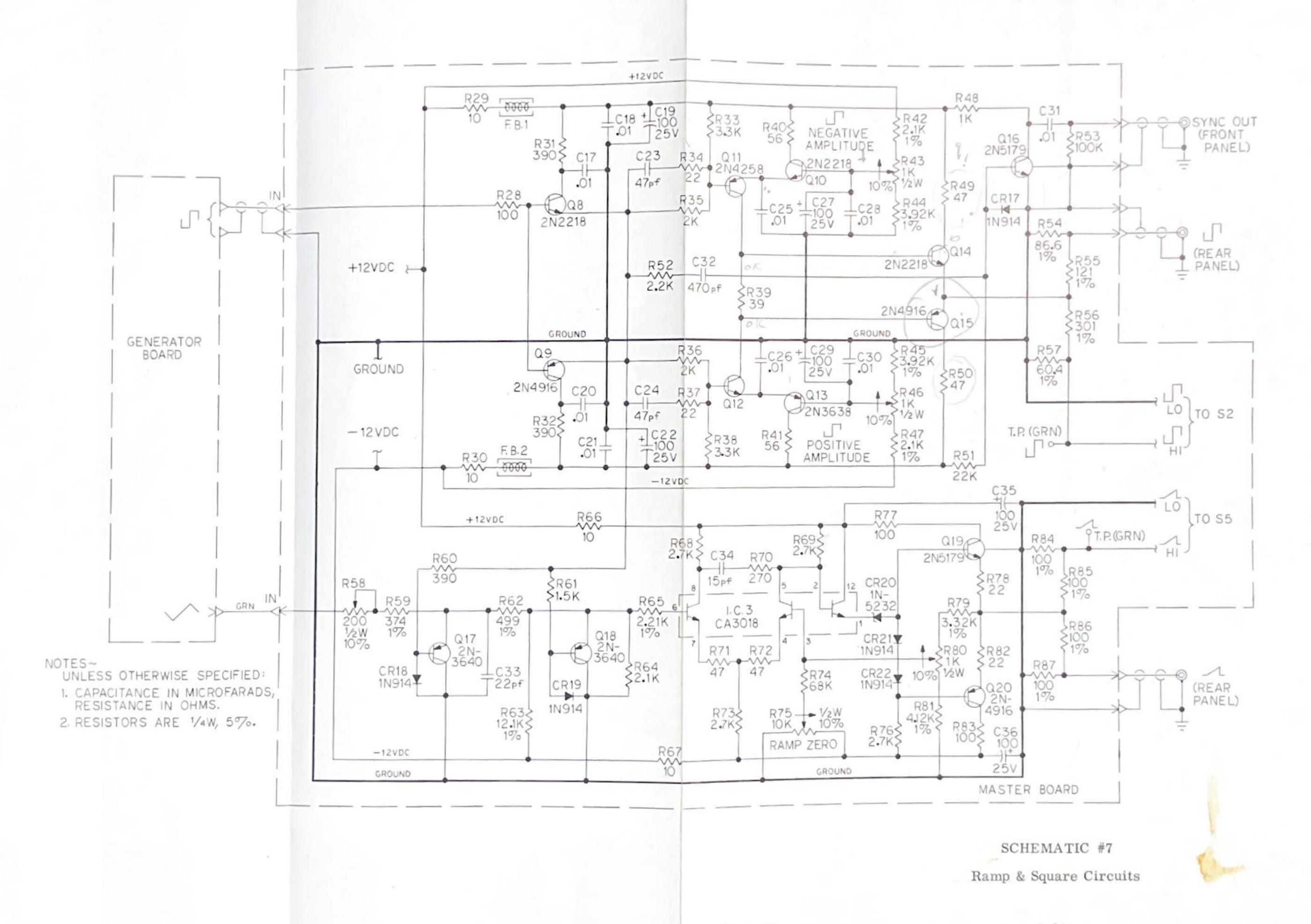
# PARTS LIST

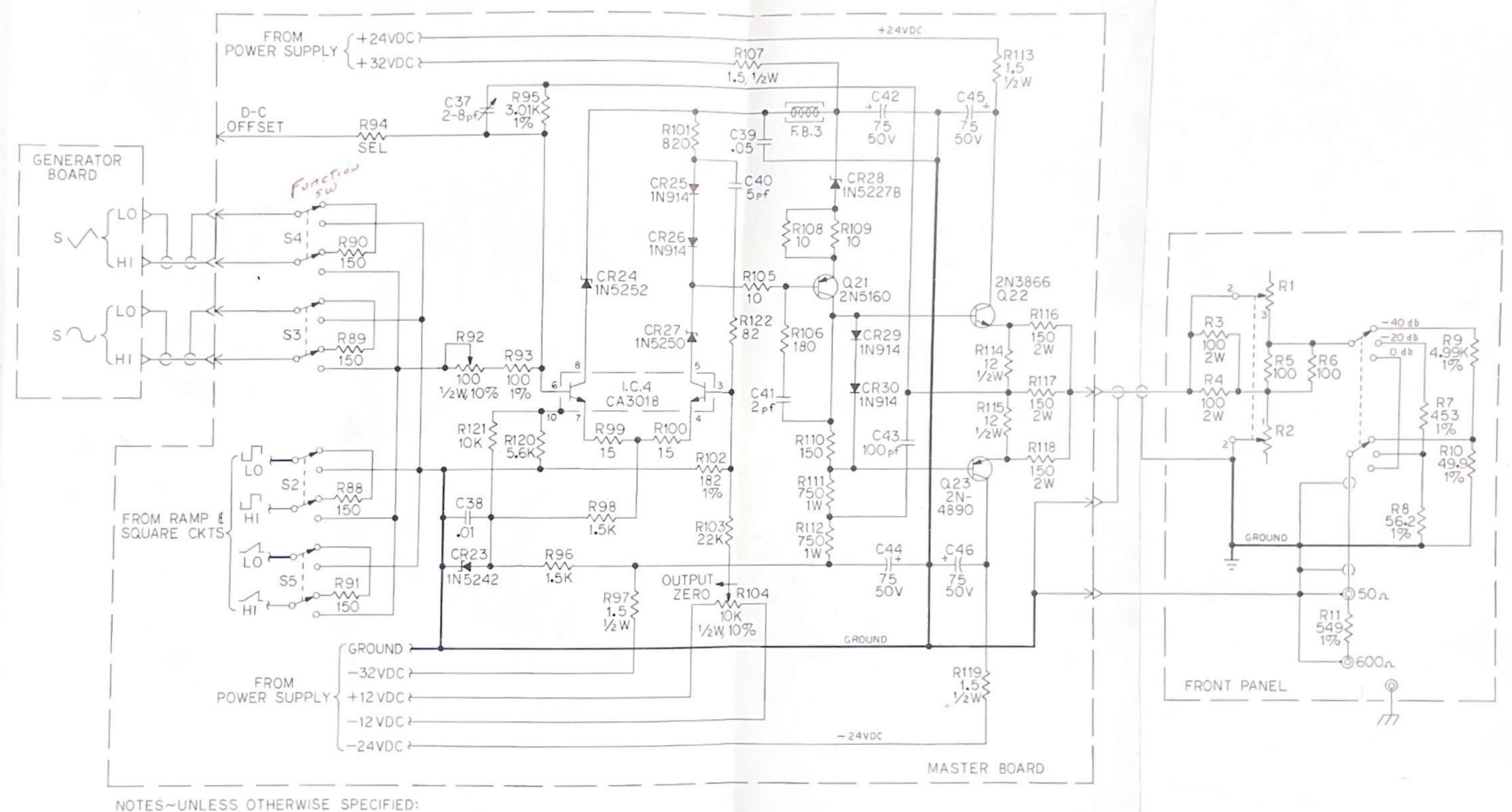
DATA ROYAL AS	SSEMBLY: FZI	JA WASTER BOA	ND ADDLINDLI		ROYAL PART N	
	DESCRIPTION			MANUI	MANUFACTURER	
SCHEMATIC DESIGNATION	VALUE	TYPE	RATING	CODE	PART NO.	PART NO.
TRANSISTOR						
Q1				JEDEC	2N2218	29-04500-0
Q2				JEDEC	2N4916	29-04530-0
Q3				JEDEC	2N2218	29-04500-0
Q4				JEDEC	2N4898	29-04510-0
Q5		RCA-40468		49671		29-04516-0
Q6		1021 10100		JEDEC	2N4360	29-04513-0
Q7		RCA-40250		49671		29-04515-0
Q8		1011 10200		JEDEC	2N2218	29-04500-0
Q9				JEDEC	2N4916	29-04530-0
Q10				JEDEC	2N2218	29-04500-0
Q11				JEDEC	2N4258	29-04507-0
Q12				JEDEC	2N4274	29-04508-0
				JEDEC	2N3638	29-04503-0
Q13				JEDEC	2N2218	29-04500-0
Q14				JEDEC	2N4916	29-04530-0
Q15				JEDEC	2N5179	29-04512-0
Q16				JEDEC	2N3640	29-04504-0
Q17				JEDEC	2N3640	29-04504-0
Q18				JEDEC	2N5179	29-04512-0
Q19				JEDEC	2N4916	29-04530-0
Q20				JEDEC	2N5160	29-04525-0
Q21				JEDEC	2N3866	29-04522-0
Q22				JEDEC	2N4890	29-04524-0
Q23				JEDEC	2N3638	29-04503-0
Q24						
INTEGRATED C	CIRCUIT					
A1 - 2		μΑ-709		17227		25-08700-0
A3 - 4		CA3018		49671		25-08705-0
SWITCH						
		PUSH BUTT				28-63003-



5-28



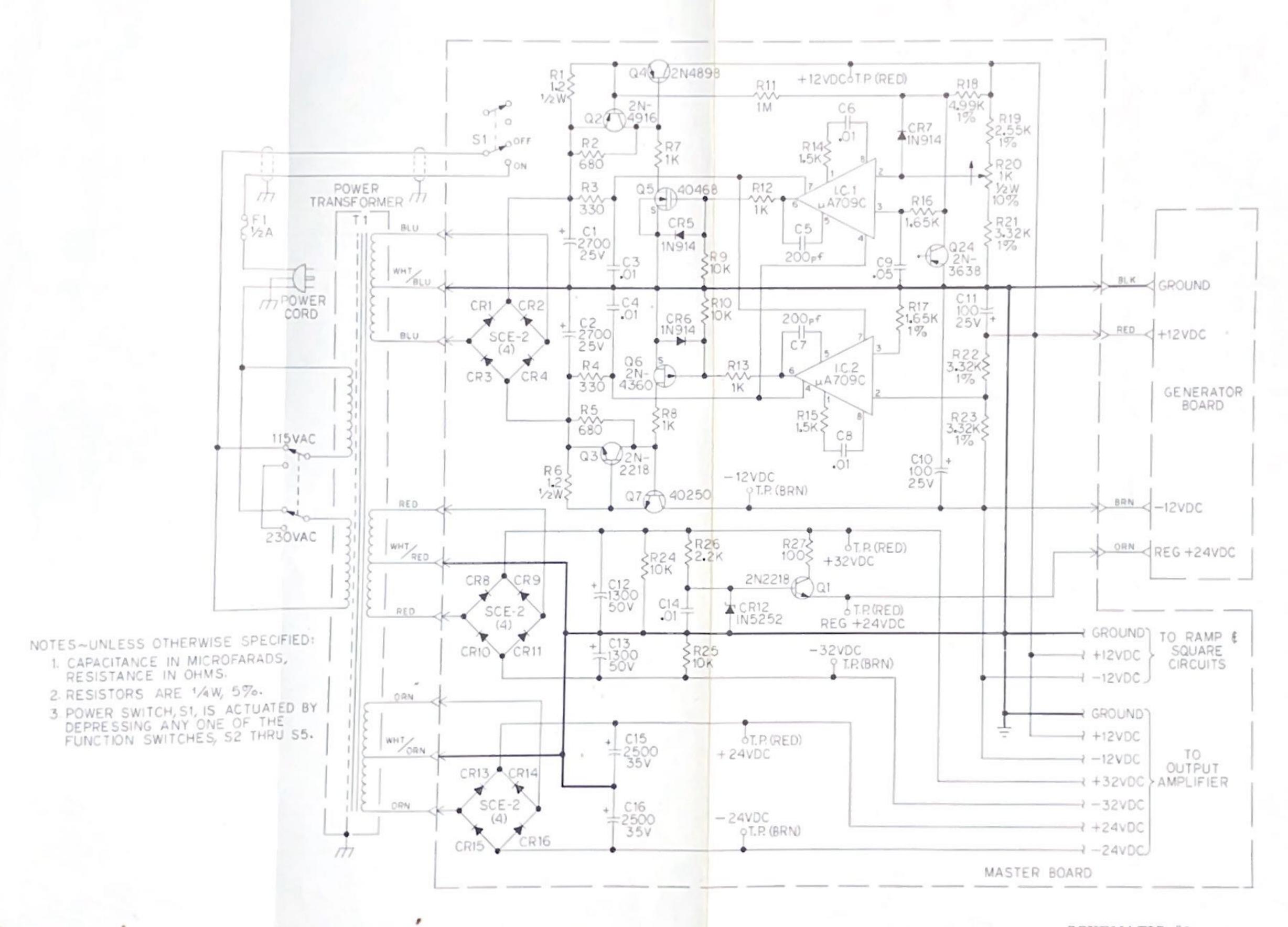




- 1. CAPACITANCE IN MICROFARADS, RESISTANCE IN OHMS.
- 2 RESISTOR ARE 1/4W, 5%

SCHEMATIC #8

Output Amplifier



SCHEMATIC #9

Power Supplies

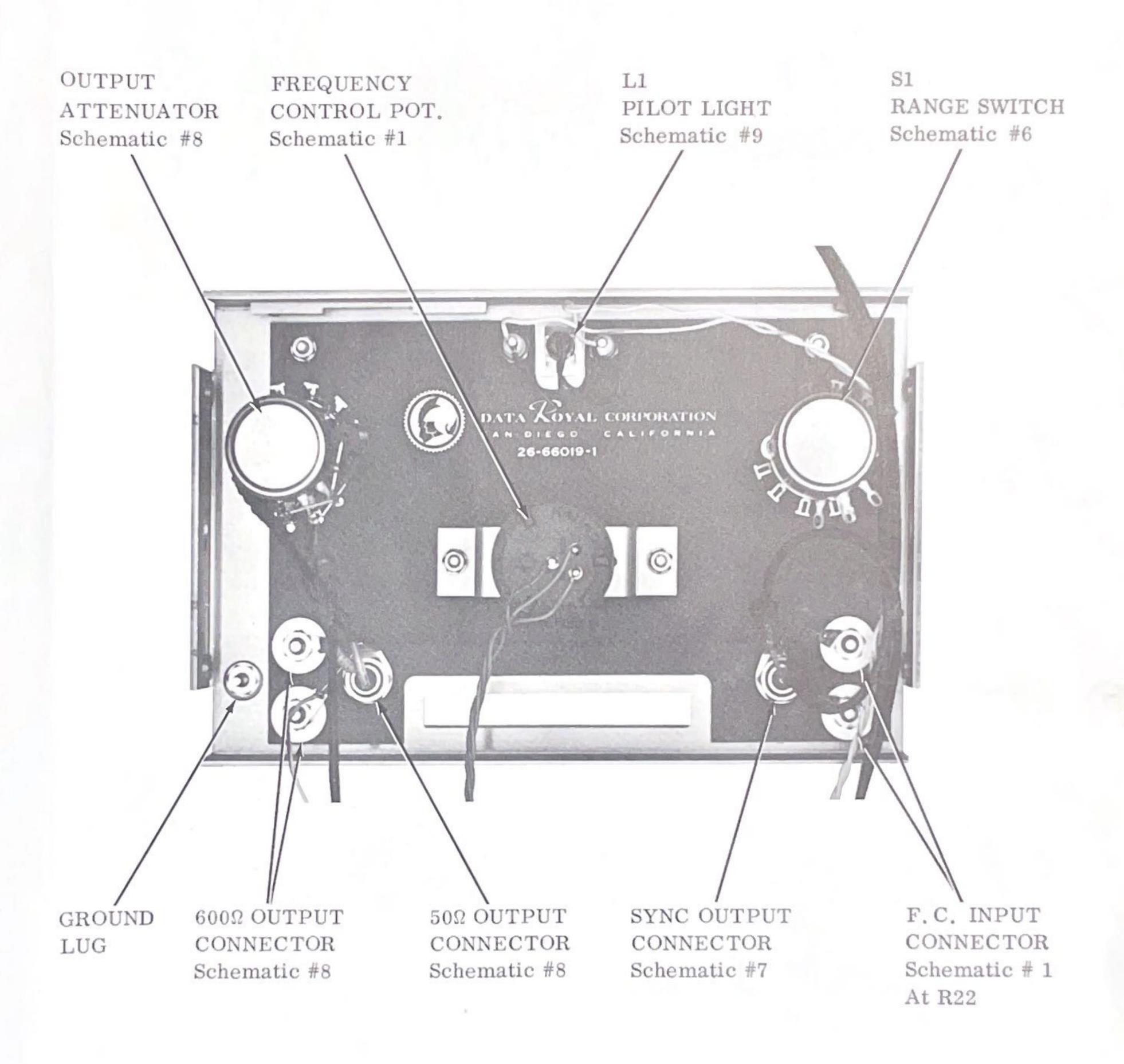


FIGURE 5-7
Front Sub-Panel Assembly

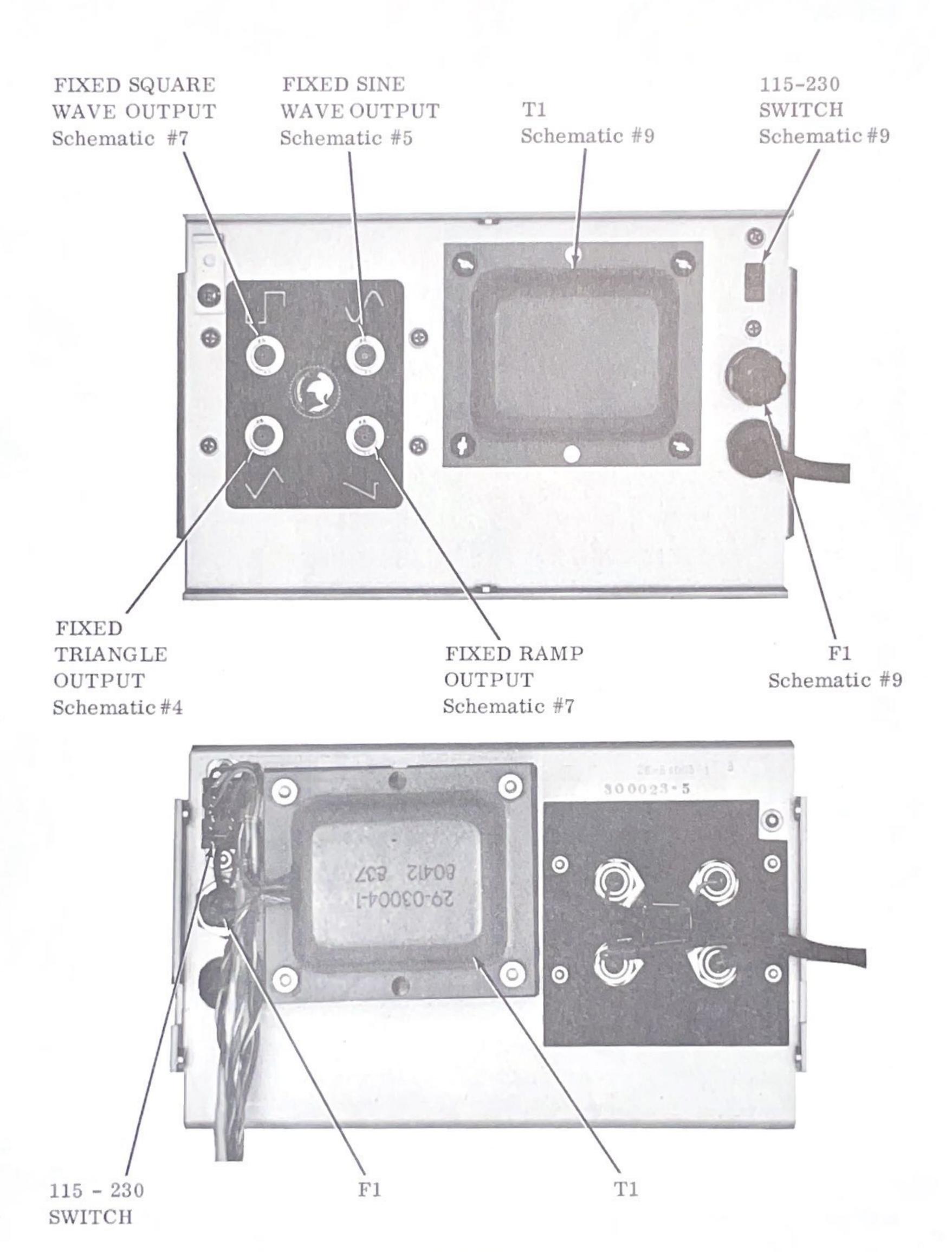


FIGURE 5-8 Rear Panel Assembly

#### SECTION VI

# RECOMMENDED SPARE PARTS

The following is a list of the recommended spare parts required to maintain a specific number of instruments at a satisfactory level of performance for one year in an isolated area.

PART DESCRIPTION	PART NUMBER	1 UNIT	5 UNITS	10 UNITS
Fuse, 1/2 Amp, Slo-Blo	24-08000-0	2	4	6
Capacitor, Elect. 2700µf 25V	21-57200-0	2	4	6
Capacitor, Elect. 1300µf 50V	21-57213-0	2	4	6
Capacitor, Elect. 100µf 25V	21-57217-0	2	4	6
Capacitor, Elect. 2500µf 35V	21-57221-0	2	4	6
Tunnel Diode, 1N3719	27-95003-0	2	4	6
Diode, Zener, 1N5234	27-95251-0	1	2	3
Diode, Zener, 1N5232B	27-95255-0	1	2	3
Diode, Zener, 1N5235B	27-95258-0	1	2	3
Diode, Zener, 1N5242B	27-95259-0	1	2	3
Diode, Zener, 1N5252	27-95261-0	1	2	3
Diode, Zener, 1N5227B	27-95263-0	1	2	3
Diode, Zener, 1N5250	27-95264-0	1	2	3
Diode, MS-7000	27-95254-0	2	4	6
Integrated Circuit, µA709	25-08700-0	2	4	6
Integrated Circuit, µA710	25-08701-0	1	2	3
Integrated Circuit, CA-3018	25-08705-0	2	4	6
Integrated Circuit, CA-3030	25-08706-0	1	2	3
Transistor, 2N2218	29-04500-0	1	2	3
Transistor, 2N3638	29-04503-0	1	2	3
Transistor, 2N3640	29-04504-0	1	2	3
Transistor, 2N4258	29-04507-0	1	2	3
Transistor, 2N4274	29-04508-0	1	2	3
Transistor, 2N4898	29-04510-0	1	2	3
Transistor, RCA 40235 or 2N5179	29-04512-0	3	6	9
Transistor, 2N4360	29-04513-0	1	2	3
Transistor, Dual FET, 2N3956	29-04514-0	1	2	9
Transistor, RCA 40250	29-04515-0	1	2	3
Transistor, RCA 40468	29-04516-0	1	2	9
Transistor, 2N 3866	29-04522-0	1	2	9
Transistor, 2N 4890	29-04524-0	1	2	9
Transistor, 2N 5160	29-04525-0	1	2	0
Transistor, 2N4121 or 2N4916	29-04530-0	3	6	9

TABLE 6-1

# LIST OF MANUFACTURERS

# FEDERAL SUPPLY CODE TO NAME

FEDERAL		
CODE	MANUFACTURER	ADDRESS
00853 01121 04062 04387 07115 12126 12406 14099 14655 17227 17856 21845 29085 44655 49671	Sangamo Electric Company Allen Bradley Company Elmenco Products Company Dale Electronics Inc. Corning Glass, Electronic Components Kidco, Inc. Elpac, Inc. Semtech Corporation Cornell-Dubilier Electric Corporation Raytheon Company Siliconix, Inc. Solitron Devices, Inc. Data Royal Corporation Ohmite Manufacturing Company Radio Corporation of America	Pickens, South Carolina Milwaukee, Wisconsin New York, New York Burbank, California Bradford, Pennsylvania Medford, New Jersey Fullerton, California Newbury Park, California Newark, New Jersey Mountain View, California Sunnyvale, California Riviera Beach, Florida San Diego, California Skokie, Illinois New York, New York
56289	Sprague Electric Company	North Adams, Massachusetts
72982 84171	Erie Technological Products Arco Electronics Company	Erie, Pennsylvania Great Neck, New York

#### ONE YEAR UNCONDITIONAL

# WARRANTY

DATA ROYAL CORPORATION hereby warrants to each original purchaser of all instruments of Data Royal Corporation manufacture as follows:

At the time of delivery of all instruments to the original purchaser thereof, Data Royal Corporation UNCONDITIONALLY WARRANTS that all of such instruments shall be free

from defects in parts, materials, and workmanship; and

II. Commencing with the date of delivery of all instruments to the original purchaser thereof, which delivery date for purposes of this warranty shall be deemed to be Data Royal Corporation's original shipment date, AND FOR A PERIOD EXPIRING ONE (1) YEAR FROM SAID DATE, Data Royal Corporation UNCONDITIONALLY WARRANTS that all such instruments shall remain free from defects in parts, materials and workmanship.

In the event any instrument shall fail to meet the terms of this warranty, Data Royal

Corporation agrees that if the original purchaser of any such instrument shall:

(1) Give to Data Royal Corporation's customer service department prompt notice in

writing of the nature of any suspected defects; and

(2) Upon receipt of written authorization and shipping instructions from Data Royal Corporation, return the instrument with suspected defects, transportation charges prepaid, to Data Royal Corporation's main plant located in San Diego, California; then Data Royal Corporation shall replace any and all defective parts or materials and shall repair any and all defective workmanship and shall return the instrument, TRANSPORTATION CHARGES COLLECT, in good working order and state of repair to the original purchaser thereof, or in the alternative, Data Royal Corporation shall have the option to replace any such defective instrument by substituting a new instrument of the same type therefor, ALL WITHOUT ANY CHARGE WHATSOEVER:

The warranties herein contained shall not obligate Data Royal Corporation in any manner whatsoever with respect to, and shall not be applicable to, any defects which after an inspection of the instrument by Data Royal Corporation are not to Data Royal Corporation's reasonable satisfaction demonstrably the result of defective parts, materials or workmanship.

Data Royal Corporation reserves the right to modify or change the design or appearance of any of its instruments as it deems desirable. Nothing herein contained shall preclude such right or create any obligation to effect such changes on units pre-

viously purchased. The remedies herein specified in the event of a breach of any of the warranties herein contained shall be the sole and exclusive remedies for such breach.

The warranties herein contained are intended to be and shall be construed as being in addition to and cumulative to all implied warranties contained in the Uniform Commercial Code, provided, however, that in the event of any breach by Data Royal Corporation of any of the implied warranties contained in the Uniform Commercial Code neither the purchaser of any Data Royal Corporation product, nor any other person, shall be entitled to recover

by reason of such breach any incidental damages or consequential damages as those terms are defined in subsection 2-715 of the Uniform Commercial Code.

All warranties herein contained shall run only in favor of the original purchaser of Data Royal Corporation's instruments and all such warranties shall immediately terminate and become null and void and of no further force or effect whatsoever upon the sale or other transfer of any such instrument by the original purchaser. The warranties herein contained constitute the sole and exclusive warranties made by Data Royal Corporation of its instruments and no other express warranties not herein contained are given and no affirmation of fact, promise or representation made by any agent, employee or representative of Data Royal Corporation shall constitute a warranty. No agent, employee or representative of Data Royal Corporation has any authority to bind Data Royal Corporation in any affirmation of fact, promise, representation or warranty not herein expressly contained.

The above statements and warranty constitute a part of Data Royal Corporation's Standard Terms and Conditions of Sale as published in our Order Acknowledgement which together is Data Royal

Corporation's warranty in its entirety.